# Project Study Report-Project Development Support (PSR-PDS) 

To

## Request Approval to Proceed to the Project Approval and Environmental Document Phase for a Locally Funded Project

On Route State Route 133

Between Canyon Acres Drive (PM 0.9)
And El Toro Road (PM 3.4)

## SUBMITTED BY:



Shohreh Dupuis, City Manager
City of Laguna Beach

## APPROVAL RECOMMENDED:

Barbara McGahey, Project Manager


APPROVED:


## Vicinity Map



On Route State Route 133
Between Canyon Acres Drive (PM 0.9)

And El Toro Road (PM 3.4)

This project study report-project development support has been prepared under the direction of the following registered civil engineer. The registered civil engineer attests to the technical information contained herein and the engineering data upon which recommendations, conclusions, and decisions are based.


GIRAIR A. KOTCHIAN - REGISTERED CIVIL E $\overline{\text { NGINEER }}$ DATE


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## 1. INTRODUCTION

The City of Laguna Beach (City), in cooperation with the California Department of Transportation (Caltrans) District 12, is proposing to construct improvements along the State Route 133 (SR-133) corridor extending approximately 2.5 miles from Canyon Acres Drive (Post Mile [PM] 0.9) to El Toro Road (PM 3.4) in the City of Laguna Beach, Orange County (the Project). Project location and vicinity maps are included in Attachment A.

SR-133, also known as Laguna Canyon Road (LCR) in this area, extends further south of Canyon Acres Drive, terminating at Pacific Coast Highway (SR-1) and transitions into unincorporated Orange County (County) north of the junction with El Toro Road. LCR is one of three gateways into the City and provides critical access to adjacent recreational spaces as well as key destinations and activities in the City. As such, ensuring that LCR provides efficient, safe access to the area is vital both to the region and to the City itself.

SR-133 within the Project limits consists of a two-lane conventional highway with a two-way left turn lane, limited shoulders, and sporadic off-street angled and parallel parking located along the northbound (NB) side of the roadway. The right-of-way (ROW) is constrained by residential and light commercial land uses, as well as various trails, park uses, institutional uses, and open space preservation areas. This portion of LCR is further constrained by Southern California Edison's (SCE) overhead transmission and distribution line poles near the travel way within the Clear Recovery Zone (CRZ). Furthermore, the existing roadway within the Project limits lacks pedestrian paths or sidewalks, or a designated bikeway, forcing pedestrians and bicyclists to use the limited shoulders to gain access to the various businesses, schools, recreational areas and trails, and transit stops along LCR.

The proposed improvements to LCR within the Project limits generally consist of bicycle lanes, pedestrian pathways/sidewalks, improved access to transit facilities, improved shoulders, and undergrounding of the SCE transmission and distribution lines outside the travel way.

Four Build Alternatives are under consideration, in addition to the No-Build Alternative, ranging in cost from approximately $\$ 130$ million to $\$ 136$ million (escalated to Year 2030), inclusive of construction, ROW, engineering, environmental, and construction management costs. The estimated cost for Project Approval/ Environmental Document (PA/ED) for the Project is approximately $\$ 4.4$ million. Preliminary layout plans and typical sections for the four proposed Build Alternatives and existing utility plans along the corridor are provided in Attachment B. Preliminary cost estimates for specific work items included in the Project are provided in Attachment C.

Potential funding for the Project is currently being sought from federal, state, and local sources including potential funding from the State Active Transportation Program (ATP), State Transportation Improvement Program (STIP).

The Project has been assigned Project Development Processing Category 4B in accordance with Chapter 8, Section 5 of the Caltrans Project Development Procedures Manual (PDPM), as it does not require substantial new ROW and does not substantially increase traffic capacity. The majority of the ROW costs are attributed to utility undergrounding.

Below is a summary of the Project information:

| Project Limits | 12-ORA-133-PM 0.9/3.4 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Number of Alternatives | 5 (including No-Build) |  |  |  |
| Alternative Recommended for Funding | Alternative 5 |  |  |  |
| Project Build Alternatives: | $\begin{gathered} \text { Alternative } \\ 2 \end{gathered}$ | Alternative 3 | Alternative 4 | Alternative 5 |
| Current Capital Outlay Support Estimate for PA/ED | $\begin{gathered} \$ 4.4 \\ \text { million } \end{gathered}$ | $\begin{gathered} \$ 4.4 \\ \text { million } \end{gathered}$ | $\begin{gathered} \$ 4.4 \\ \text { million } \end{gathered}$ | $\begin{gathered} \$ 4.4 \\ \text { million } \end{gathered}$ |
| Current Capital Outlay Construction Cost Range | $\begin{aligned} & \hline \$ 39.4 \\ & \text { million } \end{aligned}$ | $\begin{gathered} \$ 39.1 \\ \text { million } \end{gathered}$ | $\begin{aligned} & \text { \$39.6 } \\ & \text { million } \end{aligned}$ | $\begin{gathered} \hline \$ 40.2 \\ \text { million } \end{gathered}$ |
| Current Capital Outlay Right-of-Way Cost Range | $\begin{gathered} \$ 74.2 \\ \text { million } \end{gathered}$ | $\begin{gathered} \$ 74.7 \\ \text { million } \end{gathered}$ | $\begin{gathered} \$ 74.9 \\ \text { million } \end{gathered}$ | $\begin{aligned} & \$ 77.7 \\ & \text { million } \end{aligned}$ |
| Funding Source | TBD |  |  |  |
| Type of Facility | 2-lane conventional highway (one lane in each direction) |  |  |  |
| Number of Structures | 0 |  |  |  |
| Anticipated Environmental Determination or Document | Initial Study (IS)/Mitigated Negative Declaration (MND) and Environmental Assessment (EA)/Finding of No <br> Significant Impact (FONSI) |  |  |  |
| Legal Description | In Orange County in Laguna Beach from Canyon Acres Drive to El Toro Road |  |  |  |
| Project Development Category | 4B Project |  |  |  |

This Project Study Report/Project Development Support (PSR/PDS) will be used to estimate and program the capital outlay support costs necessary to complete the PA/ED phase and request approval of a locally funded project to proceed to the PA/ED phase. The remaining capital outlay support, ROW, and construction components of the Project are preliminary estimates and are not suitable for programming purposes. A Project Report (PR) will serve as the programming document for the remaining components of the Project and will serve as approval of the "selected" alternative.

It is recommended that the project development support component of the Project, as summarized in Table 15, be programmed in the STIP as discussed in the Funding Section (see Section 11). Based on the analysis contained in this PSR/PDS, it is recommended that Build Alternatives 2 through 5 be carried forward in the PA/ED phase for further detailed study. Build Alternative 5 should be used as the basis for programming support costs for this Project since it is the highest cost alternative. Final determination of the preferred alternative will be made during the PA/ED phase.

The following assumptions were made in developing the programming schedule and estimated project support costs for the PA/ED phase of the Project.

- The environmental document for this Project is assumed to be an IS/EA leading to a MND/FONSI.
- The environmental document is anticipated to take 18 to 24 months to complete.
- It is anticipated that the IS/EA will evaluate up to four Build Alternatives considered in this PSR/PDS. However, alternatives may be added, removed, or revised during the subsequent $\mathrm{PA} / E D$ phase.


## 2. BACKGROUND

The Transportation, Circulation and Growth Management Element of the City's General Plan identifies LCR as a Primary Arterial, serving as a regional access to and from the City, as well as a critical evacuation route. Due to the topographic constraints with the roadway located within an existing canyon and the proximity of the Pacific Ocean to the south, LCR serves as one of only three routes in and out of the City. Pacific Coast Highway (PCH or SR-1) accommodates travelers north and south along the coast, and LCR is oriented inland. As part of the State Highway System, LCR connects SR-1 and the coastal areas within the County to three of the key inland highways including Interstate 5 (I-5), I-405, and the SR-73 toll road.

## A. Existing Facility

LCR within the Project limits generally consists of a 34 -foot-wide roadway comprised of one 12 -foot travel lane in each direction and a 10 -foot center two-way left turn lane. Most of the route includes nonstandard paved shoulders that vary in width from a minimum of approximately 2 feet to a maximum width of 8 feet throughout the Project limits. The roadway alignment also includes tight radius reversing horizontal curves located just south of the Castle Rock Road intersection that are locally referred to as the 'Big Bend.' The roadway terrain gradually slopes downward in the southbound (SB) direction towards the Pacific Ocean. The design speed of the existing roadway is 40 mile per hour. The posted speed limit is 40 miles per hour.

Two signalized intersections at Canyon Acres Drive and El Toro Road are located within the Project limits. In addition, an existing midblock HAWK (High-Intensity Activated crossWalK) signal is located between the LCAD Main Campus and East Campus.

The existing ROW width varies from a minimum of about 53 feet in the vicinity of the 'Big Bend' area to a maximum of about 218 feet at the Canyon Acres Drive intersection. The median ROW width is approximately 73 feet but varies significantly along the route (see Attachment B, typical sections).

The roadway is bordered on both the NB and SB sides by SCE overhead utility lines that are comprised of overhead electric transmission, electric primary distribution, electric secondary distribution, telephone, and cable TV lines that run along the length of the SR-133 proposed improvements. The transmission, distribution, and telecommunications lines are for the most part supported on $66-\mathrm{kV}$ transmission poles with electrical services from the overhead distribution lines to the adjacent residences and businesses.

The Orange County Transportation Authority (OCTA) operates Bus Route 89 which provides transit service from inland areas to downtown Laguna Beach via El Toro Road and LCR - terminating at the downtown Laguna Beach Bus Station. Ten bus stops are located within the Project limits, as follows:

- Anneliese's School - NB direction
- Willow Canyon Staging Area/Laguna Coast Wilderness Park, located just south of El Toro Road - SB direction
- Vicinity of Stans Lane and Phillips Street, located just north of Sun Valley Drive - NB and SB directions
- Vicinity of Stan Oaks Drive - NB and SB directions
- LCAD Main Campus - NB and SB directions
- Vicinity of Canyon Acres Drive - NB and SB directions

The City also operates a trolley bus service during the summer months to help relieve the traffic demand associated with beachgoers and other visitors heading to Laguna Beach for special events. This trolley service provides a shuttle between the City Maintenance Yard/Municipal Parking Lot (ACT V Parking Lot), which is heavily used as a park-and-ride lot, and other points downtown. In addition, a weekend Summer Breeze service (OC Bus Route 689) operates during the peak summer months providing bus service from a parking lot near the intersection of SR-133/I-405 to the downtown Laguna Beach Bus Station with intermediate stops at key destinations along LCR.

## B. Community Interaction

In April 2013, the City initiated the Laguna Canyon Road Corridor Improvement Assessment (Assessment) in conjunction with Caltrans, Orange County Parks, and OCTA to generate and assess concepts for improving SR-133 and the LCR corridor between the intersection of Canyon Acres Drive and El Toro Road. The goal of the Assessment was to identify alternative ways to improve LCR and to create a multimodal corridor that addresses all modes of transportation, improves safety, retains the semi-rural characteristics of the area, and respects the environmental context within the project study area. Completed in August 2014, the Assessment Report presented five alternatives for improving SR-133/LCR - each alternative was comprised of different configurations of travel lanes, median treatments, complete street elements such as bike lanes and sidewalks, utility undergrounding, multi-use trails, intersection control, roadway widths, and ROW impacts.

Between 2014 and 2015, the City convened the SR-133/Laguna Canyon Road Task Force (Task Force) to review the Assessment Report, conduct additional public outreach, and conduct technical studies to consider the corridor's issues and needs, and evaluate alternative improvement concepts. Although this effort has not led to changes in adopted plans, the Task Force did reach a strong consensus on several issues, including undergrounding of utilities, minimizing impacts to open space, enhancing mobility and safety for multiple modes, making improvements to reduce potential vehicular conflicts, and not adding vehicular travel lanes. The efforts of the Task Force and associated outreach efforts culminated in the recommendation of the top two or three improvement options for further consideration by the City Council, who would prepare recommendations to Caltrans and initiate the Caltrans project development process.

The City, through the work of the Task Force, assessed several corridor improvement options to evaluate a multimodal corridor that considered operational and safety improvements, the incorporation of active transportation and complete street elements, character of the area, as well as environmental constraints along the LCR corridor. This effort culminated in the identification of nine alternatives (A through F and G.0, G. 1 and G.2) identified in the September 8, 2015 Task Force Final Report that was presented to the City Council. The Task Force also presented areas of consensus, both positive and negative, regarding the potential improvements, as well as possible next steps. Based on the presentation, the City Council approved the following recommendations:

- Review the Laguna Canyon Road Task Force's areas of specific consensus, recognizing their strong support or opposition to certain elements; and evaluation of alternative options to improve the State Highway 133/Laguna Canyon Road corridor to improve safety and mobility for motorists, pedestrians, and bicyclists.
- Direct the City Manager to transmit the information produced by and for the Laguna Canyon Road Task Force including the areas of specific consensus/concerns to Caltrans, OCTA, and SCAG; with a cover letter stating
that the City Council is interested in exploring Alternatives E, F, G.0, G.1, and G.2, and the possibility of adding a shared public transit/bicycle lane.
- Direct the City Manager to request a cost estimate from SCE to design the undergrounding of electrical transmission and distribution poles and wires along Laguna Canyon Road between the [Morro] substation and El Toro Road, and after its receipt, return to City Council with options to expedite undergrounding of utilities.

It should be noted that Task Force Alternatives F and G have been advanced with minor variations in this PSR/PDS as Build Alternatives 3 and 4, respectively.

## 3. PURPOSE AND NEED

## Purpose:

The purpose of the Project is to:

- Improve vehicular safety along the existing corridor;
- Improve pedestrian and bicycle mobility and safety; and
- Encourage the use of active transportation along the corridor.


## Need:

- Overhead Southern California Edison (SCE) transmission and distribution lines currently exist along both sides of the State Route 133 (SR-133) corridor within the Clear Recovery Zone (CRZ) and in close proximity to the edge of travel way. Coupled with high traffic demand, vehicle queuing during both peak and non-peak periods, the lack of traffic breaks or protected left-turn movements, and inadequate shoulders, there is a high concentration of accidents that occur at various locations within the Project limits.
- The corridor currently lacks adequate shoulders and pedestrian and bicycle facilities within the Project limits. Dedicated pedestrian and bicycle paths, sidewalks with Americans with Disabilities Act (ADA) access, and improved shoulders along the corridor would improve access, connectivity, and safety for pedestrians and bicyclists.
- Due to special events and the proximity to the Pacific Ocean as well as multiple adjacent recreational facilities and trails within the Project limits, traffic demand within this corridor already exceeds capacity during weekday AM and PM peak hours and during most summer weekends and holidays. Without the provision for alternative transportation modes such as public transit, walking, and biking to improve connectivity and access to adjacent residential and commercial land uses, recreational trails, and parks within the City of Laguna Beach (City) this multi-modal corridor will continue to degrade.


## 4. TRAFFIC ENGINEERING PERFORMANCE ASSESSMENT

The Traffic Engineering Performance Assessment (TEPA) prepared for this Project provides an assessment of the traffic information relevant to this Project, as well as the proposed traffic analysis methodology that will be performed in the PA/ED phase of project delivery. The TEPA serves as a reference document for this PSR/PDS (see Attachment D) and includes both vehicle traffic demand and operational analyses along the corridor as well as an assessment of complete street elements, such as bike and pedestrian facilities, and transit services.

For purposes of the traffic analysis, the corridor was separated into the following four highway/arterial segments along LCR:

1. Between El Toro Road \& Anneliese's School Driveway
2. Between Anneliese's School Driveway \& Stan Oaks Drive
3. Between Stan Oaks Drive \& LCAD Main Campus Driveway
4. Between LCAD Main Campus Driveway \& Canyon Acres Drive

In addition, the traffic study area (see TEPA Figure 1-3) consists of the following nine study intersections/locations along LCR:

1. El Toro Road
2. Anneliese's School Driveway
3. Sun Valley Drive
4. Laguna Beach Dog Park Driveway
5. Stan Oaks Drive
6. Castle Rock Road
7. LCAD Main Campus Driveway
8. City Maintenance Yard/ACT V Parking Lot Driveway
9. Canyon Acres Drive

For arterial segments, traffic counts were collected over a 24 -hour period on Thursday November 30, 2017. Weekday intersection AM and PM peak period counts were collected on December 2, 2017, and January 25, 2018. Traffic counts were collected while educational institutions in the vicinity of the Project were in session, thereby ensuring the validity of the data collection.

For the intersections that traffic counts were not directly collected, a methodology was used to develop the turning movement volumes. The methodology consisted of utilizing the arterial counts collected along SR-133 and the Institute of Transportation Engineers (ITE) Trip Generation Manual to estimate the diverging traffic into and out of the cross streets/driveways.

The TEPA provides existing and forecast traffic conditions in the Project area. Detailed methodologies and analyses can be found in the TEPA. Key findings and recommendations are summarized herein. The opening year established for the PSR/PDS is 2030 and the horizon year is 2050. Thus, the scenarios that are evaluated in the TEPA include:

- Existing Baseline (2017) Conditions
- Opening Year (2030) Conditions
- Horizon Year (2050) Conditions

The traffic analysis for the existing, No-Build and four Build Alternatives include complete street elements such as bike and pedestrian facilities and transit services. Since additional lanes are not being added for Build Alternatives 2 to 4, the traffic capacity enhancements provided by the proposed Project under Build Alternatives 2 to 4 are consistent from one alternative to another.

Traffic demand within this corridor already exceeds capacity during weekday AM and PM peak hours and during most summer weekends and holidays due to special events and the proximity to the Pacific Ocean as well as multiple adjacent recreational facilities and trails. A reversible lane alternative, Build Alternative 5, is being considered part of the overall corridor improvements evaluation in the PSR/PDS in order to handle the overcapacity traffic conditions. For Build Alternative 5, the peak direction is proposed to have two lanes. Left turn at the two-way stop-controlled intersections/locations are prohibited between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits. All driveways have right-in and right-out accesses. The reversible traffic lanes add peakdirection capacity to a two-way road and decrease congestion by borrowing available lane capacity from the other (off-peak) direction. Peak season daily and corresponding peak hour traffic volumes were used to evaluate the traffic conditions for Alternative 5. The peak season traffic volume increase rate was developed to be approximately $12 \%$ higher than the off-peak months. Therefore, the No-Build and Build traffic volumes under Alternative 1 through Alternative 4 remain the same. The Alternative 5 traffic volumes are generally 12\% higher than the Alternative 1 through 4 volumes.

Based on the 2014 Transportation Concept Report (TCR) for SR-133, the target concept level of service is LOS D for Year 2050. The concept LOS indicates the minimum LOS that would be allowed on a route prior to proposing an alternative to improve operating conditions. However, based on the forecast 2050 traffic volumes, concurrence from Caltrans staff, and the approved traffic methodology for this Project, the target LOS was determined to be LOS E.

## Highway Segment Analysis

Table 1 through Table 3 present the Existing, Opening Year, and Horizon Year AM and PM peak hour and daily volumes for the four highway segments along LCR. Traffic demand for LCR is at capacity during peak hours of the day/week and is expected to increase more than 50 percent from existing approximately 36,000 vehicles per day to approximately 55,000 vehicles per day by the year 2050 during non-peak season. Existing AM and PM peak hour intersection turning movement volumes for the nine study intersections/locations can be found in the TEPA.

Table 1: Existing Highway Segment Traffic Volumes

| ID | Description | Direction | AM Peak Hour | PM Peak <br> Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,006 | 1,348 | 36,337 |
|  |  | Southbound | 1,239 | 1,251 |  |
| 2 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 988 | 1,350 | 36,373 |
|  |  | Southbound | 1,267 | 1,264 |  |
| 3 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 989 | 1,306 | 35,690 |
|  |  | Southbound | 1,249 | 1,282 |  |
| 4 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,032 | 1,307 | 36,088 |
|  |  | Southbound | 1,235 | 1,301 |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Table 3-1

Table 2: Opening Year (2030) Highway Segment Traffic Volumes

| ID | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Alternatives 1 to 4 |  |  |  |  |  |
| 1 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,310 | 1,920 | 44,600 |
|  |  | Southbound | 1,720 | 1,730 |  |
| 2 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,300 | 1,960 | 45,100 |
|  |  | Southbound | 1,780 | 1,730 |  |
| 3 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 1,350 | 1,890 | 44,300 |
|  |  | Southbound | 1,770 | 1,790 |  |
| 4 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,370 | 1,890 | 44,800 |
|  |  | Southbound | 1,760 | 1,800 |  |
| Alternative 5 |  |  |  |  |  |
| 1 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,470 | 2,150 | 50,000 |
|  |  | Southbound | 1,930 | 1,940 |  |
| 2 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,460 | 2,200 | 50,500 |
|  |  | Southbound | 1,990 | 1,940 |  |
| 3 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 1,510 | 2,120 | 49,600 |
|  |  | Southbound | 1,980 | 2,000 |  |
| 4 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,530 | 2,120 | 50,200 |
|  |  | Southbound | 1,970 | 2,020 |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Table 4-1 and Table 4-2

Table 3: Horizon Year (2050) Highway Segment Traffic Volumes

| ID | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Alternatives 1 to 4 |  |  |  |  |  |
| 1 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,680 | 2,625 | 54,800 |
|  |  | Southbound | 2,310 | 2,310 |  |
| 2 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,680 | 2,730 | 55,900 |
|  |  | Southbound | 2,415 | 2,310 |  |
| 3 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 1,785 | 2,625 | 54,800 |
|  |  | Southbound | 2,415 | 2,415 |  |
| 4 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,785 | 2,625 | 55,400 |
|  |  | Southbound | 2,415 | 2,415 |  |
| Alternative 5 |  |  |  |  |  |
| 1 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,880 | 2,940 | 61,400 |
|  |  | Southbound | 2,590 | 2,590 |  |
| 2 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,880 | 3,060 | 62,600 |
|  |  | Southbound | 2,700 | 2,590 |  |
| 3 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 2,000 | 2,940 | 61,400 |
|  |  | Southbound | 2,700 | 2,700 |  |
| 4 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 2,000 | 2,940 | 62,000 |
|  |  | Southbound | 2,700 | 2,700 |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Table 4-7 and Table 4-8
Table 4 presents highway analysis LOS results for the four segments along LCR under Existing conditions, and under Opening Year and Horizon Year No-Build and Build conditions. As shown in the table, all the study area highway segments currently operate at LOS E or better under existing conditions. Under Opening Year (2030) conditions, all the study area highway segments are projected to operate at LOS F with No-Build and Build Alternatives, 1 to 4 . Similarly, all the study area highway segments are projected to operate at LOS F under Horizon Year (2050) conditions with No-Build and Build Alternatives, 1 to 4 . For Build Alternative 5 conditions, the peak direction, i.e., southbound during AM peak and northbound during PM peak, operate at LOS C and D with two-lane configuration utilizing the center reversible lane under Opening Year (2030) and Horizon Year (2050), respectively.

Table 4: Highway Analysis LOS Results along SR-133

| ID | From | To | Existing(2017) |  | Opening Year* <br> (2030) |  | Horizon Year* (2050) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM <br> Peak <br> Hour <br> LOS | $\overline{P M}$ <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | $\mathbf{P M}$ <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | $\overline{P M}$ <br> Peak <br> Hour <br> LOS |
| Alternatives 1 to 4 |  |  |  |  |  |  |  |  |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |  |
| 1 | El Toro Road | Sun Valley Drive | E | E | F | F | F | F |
| 2 | Sun Valley Drive | Stan Oaks Drive | E | E | F | F | F | F |
| 3 | Stan Oaks Drive | LCAD Driveway | E | E | F | F | F | F |
| 4 | LCAD Driveway | Canyon Acres Drive | E | E | F | F | F | F |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |  |  |  |
| 1 | El Toro Road | Sun Valley Drive | E | E | F | F | F | F |
| 2 | Sun Valley Drive | Stan Oaks Drive | E | E | F | F | F | F |
| 3 | Stan Oaks Drive | LCAD Driveway | E | E | F | F | F | F |
| 4 | LCAD Driveway | Canyon Acres Drive | E | E | F | F | F | F |
| Alternative 5 |  |  |  |  |  |  |  |  |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |  |
| 1 | El Toro Road | Sun Valley Drive | E | E | F | C | F | D |
| 2 | Sun Valley Drive | Stan Oaks Drive | E | E | F | C | F | D |
| 3 | Stan Oaks Drive | LCAD Driveway | E | E | F | C | F | D |
| 4 | LCAD Driveway | Canyon Acres Drive | E | E | F | C | F | D |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |  |  |  |
| 1 | El Toro Road | Sun Valley Drive | E | E | C | F | D | F |
| 2 | Sun Valley Drive | Stan Oaks Drive | E | E | C | F | D | F |
| 3 | Stan Oaks Drive | LCAD Driveway | E | E | C | F | D | F |
| 4 | LCAD Driveway | Canyon Acres Drive | E | E | C | F | D | F |
| LOS = Level of Service; Bold: LOS F; * No-Build and Build Conditions |  |  |  |  |  |  |  |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Tables 6-1, 6-3, 6-4, 6-13 \& 614

## Intersection Analysis

## No-Build Condition - Alternative 1

Table 5 presents intersection LOS results for the study intersections/locations under Existing, Opening Year and Horizon Year No-Build conditions. As shown in the table, all study area intersections currently operate at LOS E or better under existing conditions, except the following which operate at LOS F:

- Anneliese's School driveway, during AM Peak Hour
- LCAD Main Campus driveway, during AM Peak Hour
- City Maintenance Yard driveway, during AM and PM Peak Hours

Under Opening Year (2030) No-Build conditions, all study area intersections will operate at LOS E or better, except the following which operate at LOS F:

- Anneliese's School driveway, during AM and PM Peak Hours
- Stan Oaks Drive, during PM Peak Hour
- Castle Rock Road, during PM Peak Hour
- LCAD Main Campus driveway, during AM and PM Peak Hours
- City Maintenance Yard driveway, during AM and PM Peak Hours

Under Horizon Year (2050) No-Build conditions, all study area intersections will operate at LOS E or better, except the following which operate at LOS F:

- Anneliese's School driveway, during AM and PM Peak Hours
- Sun Valley Drive, during AM and PM Peak Hours
- Laguna Beach Dog Park driveway, during AM and PM Peak Hours
- Stan Oaks Drive, during AM and PM Peak Hours
- Castle Rock Road, during AM and PM Peak Hours
- LCAD Main Campus driveway, during AM and PM Peak Hours
- City Maintenance Yard driveway, during AM and PM Peak Hours

Table 5: Intersection Analysis LOS results along SR-133 (No-Build Condition)

|  |  |  |  |  | Openi | Year <br> 3) | Horizo (20 | Year <br> 50) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | Intersection/ Driveway | Traffic Control | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS |
| 1 | El Toro Road | Signalized | C | B | C | C | E | D |
| 2 | Anneliese's School Driveway | Stop-Controlled | F | E | F | F | F | F |
| 3 | Sun Valley Drive | Stop-Controlled | D | D | E | E | F | F |
| 4 | Laguna Beach Dog Park Driveway | Stop-Controlled | D | D | E | E | F | F |
| 5 | Stan Oaks Drive | Stop-Controlled | D | D | E | F | F | F |
| 6 | Castle Rock Road | Stop-Controlled | D | D | E | F | F | F |
| 7 | LCAD Main Campus Driveway | Stop-Controlled | F | D | F | F | F | F |
| 8 | City Maintenance Yard Driveway | Stop-Controlled | F | F | F | F | F | F |
| 9 | Canyon Acres Drive | Signalized | A | A | A | A | A | A |
| LOS = Level of Service; Bold: LOS F |  |  |  |  |  |  |  |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Tables 6-2, 6-5, \& 6-15

## Build Condition - Alternatives 2, 3, 4, and 5

The comparative evaluation of the Project alternatives provided in the TEPA is based on the latest Caltrans Intersection Control Evaluation (ICE) review process as well as a preliminary peak hour warrant analysis under the Horizon Year (2050) conditions.

The ICE review follows a two-step process that includes an initial screening assessment appropriate for this PSR/PDS followed by further design and analysis in the subsequent $\mathrm{PA} / \mathrm{ED}$ phase. The goal of this process is to allow for an informed decision to be made to implement the most efficient intersection control system or strategy at each location along the State ROW - with an increased emphasis on pedestrian and bike access and safety.

Based on the preliminary analysis included in the TEPA, the following three driveways, analyzed as stop-controlled intersections, met the peak hour traffic signal warrant thresholds during the AM peak hour under existing (2017) conditions:

- Anneliese's School Driveway
- LCAD Main Campus Driveway
- City Maintenance Yard Driveway

At the junction of SR-133 with Anneliese's School driveway, the peak hour typically occurs before the school starts and after the school dismisses. Traffic entering and exiting Anneliese's School is expected to be minimal for the rest of the time periods. To avoid the interruption of the traffic flow along LCR and due to the close proximity of the driveway to the SR-133/El Toro Road Intersection immediately to the north, the junction of SR-133 with Anneliese's School driveway remains stop-controlled under the future build conditions. To reflect the worst-case scenario with low left turn movement volumes at this driveway, the driveway is analyzed with left turn movement allowed under Build Alternatives 2 to 4 .

At the ingress/egress of SR-133 with the LCAD Main Campus Driveway, traffic entering and exiting the driveway is expected to spread throughout the day. To provide adequate gaps for left turning traffic and safe access in and out of the school, the driveway was analyzed as signalized intersection under the future year Build Alternatives 2 to 4 conditions. This driveway was analyzed as a stop-controlled rightin and right-out intersection under Build Alternative 5 with the worst-case peak season volumes. The existing signalized High-Intensity Activated Crosswalk Beacon (HAWK) is located 250 feet upstream of this driveway. Under Build Alternatives 2 to 4 conditions with the signalization at the junction of LCR and Laguna College of Arts \& Design Driveway, the HAWK signal is recommended to be removed and a pedestrian crossing walk at this signalized driveway is recommended to be added. Under Build Alternative 5, the HAWK signal is recommended to remain as is. Decisions on the signalization at the junction of LCR with Laguna College of Arts \& Design Driveway and removal of the HAWK signal is deferred to the PA/ED phase for further evaluation.

The ingress/egress at the City Maintenance Yard Driveway was also analyzed as a stopcontrolled intersection. Although the City Maintenance Yard Driveway is warranted for a traffic signal during the AM peak hour, a traffic signal is not recommended at this location due to right-of-way constraints and the close proximity to the Canyon Acres Drive intersection located immediately to the south. Therefore, this intersection is recommended to be maintained as a stop-controlled intersection under the future build conditions.

The intersections at El Toro Road and Canyon Acres Drive would remain as signalized intersections in all Build scenarios.

The above recommendations were applied in the analysis under the four Build Alternatives. Further warrant analysis is required to be performed in the PA/ED phase to determine the need for traffic signals at the above proposed locations.

As further discussed below in Section 6 - Corridor and System Coordination, two separate improvement projects are currently being advanced by Caltrans encompassing the El Toro Road/SR-133 and the Canyon Acres Drive/SR-133 signalized intersections. These proposed improvements are anticipated to be constructed in advance of this Project and are, therefore, assumed to be an existing condition. Thus, an ICE analysis to evaluate an alternative intersection control system at these locations, such as a
roundabout, has not been performed and is considered to be outside the scope of this ATP/utility undergrounding Project.

Although improvements to the El Toro Road/SR-133 intersection are currently considered outside the scope of this PSR/PDS, subsequent studies may be warranted to evaluate options to potentially improve the El Toro Road/SR-133 intersection and the portion of El Toro Road from the SR-133 intersection to SR-73. Among many options, a roundabout at the El Toro Road/SR-133 intersection is being considered.

Table 6 presents the projected intersection LOS results under Opening Year (2030) Build conditions. As shown, the study area intersections will operate at LOS E or better under Opening Year (2030) Build Alternatives 2 to 4 conditions, except the following which are expected to operate at LOS F.

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at LCAD Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

As shown, all study area intersections operate at LOS E or better under Opening Year (2030) Build Alternative 5 conditions, except the following which are expected to operate at LOS F.

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at LCAD Driveway, during PM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

Table 6: Intersection Analysis Year Opening Year (2030) Build Condition

| ID | Intersection/ Driveway | Traffic Control | Alternatives 1 to 4 |  | Alternative 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS |
| 1 | El Toro Road | Signalized | C | C | D | C |
| 2 | Anneliese's School Driveway | Stopcontrolled | F | F | F | D |
| 3 | Sun Valley Drive | Stopcontrolled | E | E | E | C |
| 4 | Laguna Beach Dog Park Driveway | Stopcontrolled | E | E | E | C |
| 5 | Stan Oaks Drive | Stopcontrolled | E | F | E | C |
| 6 | Castle Rock Road | Stopcontrolled | E | F | E | C |
| 7 | LCAD Main Campus Driveway | Signalized/ Stopcontrolled | F | D | D | F |
| 8 | City Maintenance Yard Driveway | Stopcontrolled | F | F | F | F |
| 9 | Canyon Acres Drive | Signalized | A | A | A | A |
| LOS = Level of Service; Bold: LOS F; * Signalized under Alternatives 1 to 4 and Minor Street Stop Controlled intersection under Alternative 5 |  |  |  |  |  |  |
| Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Tables 6-6 and 6-7 |  |  |  |  |  |  |

Table 7 presents the projected intersection LOS results under Horizon Year (2050) Build conditions. As shown, the study area intersections will operate at LOS F under Horizon Year Build Alternatives 2 to 4 conditions, except for the intersections at SR133/El Toro Road, which operates at LOS E and LOS D during the AM and PM peak hours, respectively, and SR-133/Canyon Acres Drive, which operates at LOS A during both the AM and the PM peak hours. As shown, all study area intersections operate at LOS E or better under Horizon Year (2050) Build Alternative 5 conditions, except the following intersections which are expected to operate at LOS F.

- SR-133 at El Toro Road, during AM Peak Hour
- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Sun Valley Drive, during AM Peak Hour
- SR-133 at Laguna Beach Dog Park Driveway, during AM Peak Hour
- SR-133 at Stan Oaks Drive, during AM Peak Hour
- SR-133 at Castle Rock Road, during AM Peak Hour
- SR-133 at LCAD Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

Table 7: Intersection Analysis Horizon Year (2050) Build Condition

| ID | Intersection/ Driveway | Traffic Control | Alternatives 1 to 4 |  | Alternative 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS | AM <br> Peak <br> Hour <br> LOS | PM <br> Peak <br> Hour <br> LOS |
| 1 | El Toro Road | Signalized | E | D | F | D |
| 2 | Anneliese's School Driveway | Stopcontrolled | F | F | F | F |
| 3 | Sun Valley Drive | Stopcontrolled | F | F | F | D |
| 4 | Laguna Beach Dog Park Driveway | Stopcontrolled | F | F | F | D |
| 5 | Stan Oaks Drive | Stopcontrolled | F | F | F | D |
| 6 | Castle Rock Road | Stopcontrolled | F | F | F | D |
| 7 | LCAD Main Campus Driveway | Signalized/ Stopcontrolled | F | F | F | F |
| 8 | City Maintenance <br> Yard Driveway | Stopcontrolled | F | F | F | F |
| 9 | Canyon Acres Drive | Signalized | A | A | A | A |

LOS = Level of Service; Bold: LOS F; * Signalized under Alternatives 1 to 4 and Minor Street Stop Controlled intersection under Alternative 5
Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Tables 6-16 and 6-17

## Multimodal Analysis

A multimodal analysis was performed to identify existing operational deficiencies and evaluate and compare the different alternatives. The methodologies put forth by Highway Capacity Manual (HCM) 6 were used to assess the LOS performance of bicycle, transit and pedestrian modes of transportation along LCR. The methodology and inputs used to assess the different modes can be found in the TEPA.

Table 8 presents the worst-case results of the multimodal analysis under the Opening Year (2030) and the Horizon Year (2050) conditions for Alternative 1 (No-Build) and Alternatives 2, 3, 4, and 5 (Build). As shown, under the No-Build condition, transit and pedestrian modes operate at LOS E or better, while vehicle and bicycle modes operate at LOS F. However, under the four Build conditions (Alternatives 2, 3, 4, and 5), transit, pedestrian, and bicycle modes operate at LOS E or better, while vehicle mode operates at LOS F.

Table 8: Opening Year (2030) and Horizon Year (2050) Multimodal LOS Comparison

| Mode | Alt 1 (No-Build) | Alt 2 | Alt 3 | Alt 4 | Alt 5 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |
| Vehicle | F | F | F | F | F/D* |
| Transit | E | B | A | A | B |
| Bicycle | F | A | B | A | A |
| Pedestrian | D | A | A | A | A |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |
| Vehicle | F | F | F | F | F/D* |
| Transit | E | B | C | A | B |
| Bicycle | F | A | A | A | A |
| Pedestrian | D | N/A | A | A | A |
| LOS $=$ Level of Service; Bold: LOS F; Alt $=$ Alternative; N/A $=$ Not Applicable; <br> * off-peak/peak direction results |  |  |  |  |  |

Source: LCR Traffic Engineering Performance Assessment (March 30, 2022)
Tables 6-8, 6-9, 6-10, 6-11, 6-12, 6-18, 6-19, 6-20, 6-21, and 6-22
The multimodal analysis results show improvement in pedestrian, transit and bicycle LOS for all Build Alternatives as compared to the No-Build Alternative due to the addition of bike, pedestrian and transit improvements along the corridor. The vehicular LOS remains F for the Build Alternatives 2 to 4 conditions since no additional capacity is proposed as part of the Project. Under Build Alternative 5 conditions, vehicle mode operates at LOS F and D for the off-peak and peak directions, respectively. The peak direction vehicular LOS would improve resulting from the two-lane configuration with the reversible lane conversion.

## Traffic Analysis Summary

The No-Build and three Build Alternatives 2 to 4 provide one vehicular travel lane in each direction along LCR, thereby adding no capacity compared to existing conditions. Therefore, vehicular traffic demand is forecasted to be the same for No-Build and Build, Alternatives 1 to 4 conditions.

The No-Build and Build, Alternatives 1 to 4, differ from one another in the number, classification, and configuration of pedestrian, bike, and transit facilities they provide.

Alternative 5 was proposed to focus on the peak season with the worst-case traffic volumes. As mentioned in previous section, the peak direction configurations are proposed to have two lanes during the peak hours using the reversible lane concept, i.e., Build Alternative 5.

For Alternatives 1 to 4, since none of the alternatives have proposed any addition in number of lanes, there was no significant improvement in vehicular operations along the corridor. As shown in Table 4, the corridor operations for the peak direction under Build Alternative 5 would improve significantly with the reversible lane conversion.

Table 6 and Table 7 compare years 2030 and 2050 intersection analysis, respectively. As shown in the tables, the intersections service levels would improve at several stopcontrolled intersections with the right-in and right-out configuration during the PM peak hour under Build Alternative 5.

Table 8 compares the results of the multimodal analysis for Alternatives 1 through 5 under the Opening Year (2030) and Horizon Year (2050) conditions. As shown, the LOS performance for transit, bike, and pedestrian modes improves for all four Build Alternatives compared to the No-Build Alternative. The peak direction LOS performance for vehicle modes improves with the two-lane configuration under Build Alternative 5 compared to the No-Build Alternative.

Due to heavy traffic experienced during weekdays, summer weekends and holidays, several operational constraints are observed along the corridor, including vehicular queuing, inadequate gaps for left-turning traffic from driveways and cross streets, and conflicts between vehicles, pedestrians and bicycles due to inadequate bike lanes and sidewalks. The proposed Build Alternatives accommodate safety improvements and improvements for alternative transportation modes; thus, enhancing the safety and circulation for all modes of transportation and addressing the constraints observed.

As a result of the Build Alternatives, the corridor is expected to be safer for pedestrians and bicyclists due to a reduction in conflicts with vehicles.

## Complete Streets

This Project is consistent with Deputy Directive 64-R2 and addresses the mobility and safety needs of bicyclists and pedestrians by implementing 'complete streets' elements such as dedicated pedestrian paths/sidewalks and bicycle lanes.

## Safety/Collision Data

The Traffic Accident Surveillance and Analysis System (TASAS) Tables B collision data provided by Caltrans District 12 were analyzed for collisions that occurred for the 60 -month period between January 1, 2016 and December 31, 2020 on SR-133 from PM 0.940 to PM 3.415. Table 9 provides a summary of Caltrans’ TASAS Table B Selective Accident Rate Calculation. Table B provides actual and average rates for similar highways and intersections. TASAS Selective Accident Retrieval (TSAR) provides a summary of the type of collision by location. TSAR data for the study area can be found in Table 10. A more detailed analysis can be found in the TEPA.

## Northbound SR-133

As shown in Tables 9 and 10, there were a total of 103 collisions in the NB direction recorded on SR-133 within the Project limits, with 50 injury collisions and no fatality collision. The majority of the collisions were rear ends and broadsides corresponding to approximately 51 percent and 14 percent of the total collisions, respectively. In addition, there were two auto-pedestrian collisions recorded from the LCAD Main Campus Driveway to Anneliese's School.

As shown in Table 9, the total actual collision rate for each of the four NB segments, measured in collisions per million vehicle-miles ( $a / \mathrm{mvm}$ ), are approximately double the statewide average collision rates for similar facilities.

Table 9: TASAS Table B Accident Rates for SR-133

| Post Mile (PM) | Location | Number of Accidents |  |  |  | Accident Rates ${ }^{1}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Actual |  |  | Average |  |  |
|  |  | Total <br> (T) | Fatal <br> (F) | Injury (I) | F + I | Fat | F+I | Total | Fat | F+I | Total |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |  |  |  |  |
| PM 0.94 <br> to 1.573 | From Canyon Acres Drive to Laguna Canyon of Arts and Design | 35 | 0 | 14 | 14 | 0.00 | 0.68 | 1.70 | 0.012 | 0.40 | 0.83 |
| $\begin{aligned} & \hline \text { PM } 1.573 \\ & \text { to } 2.446 \end{aligned}$ | From Laguna Canyon Arts and Design to Stan Oaks Drive | 30 | 0 | 16 | 16 | 0.00 | 0.55 | 1.03 | 0.013 | 0.40 | 0.82 |
| $\begin{aligned} & \text { PM } 2.446 \\ & \text { to } 3.330 \end{aligned}$ | From Stan Oaks Drive to Laguna Canyon Arts and Design | 36 | 0 | 20 | 20 | 0.00 | 0.66 | 1.19 | 0.013 | 0.40 | 0.82 |
| $\begin{gathered} \text { PM } 3.330 \\ \text { to } 3.415 \end{gathered}$ | From Anneliese's School to EI Toro Road | 2 | 0 | 0 | 0 | 0.00 | 0.00 | 0.74 | 0.013 | 0.40 | 0.82 |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \hline \text { PM } 1.573 \\ \text { to } 0.94 \end{gathered}$ | From Laguna Canyon Arts and Design to Canyon Acres Drive | 16 | 0 | 7 | 7 | 0.00 | 0.34 | 0.78 | 0.012 | 0.40 | 0.83 |
| $\begin{aligned} & \text { PM } 2.446 \\ & \text { to } 1.573 \end{aligned}$ | From Stan Oaks Drive to Laguna Canyon Arts and Design | 17 | 0 | 10 | 10 | 0.00 | 0.34 | 0.58 | 0.013 | 0.40 | 0.82 |
| $\begin{aligned} & \text { PM } 3.330 \\ & \text { to } 2.446 \end{aligned}$ | From Anneliese's School to Stan Oaks Drive | 24 | 0 | 17 | 17 | 0.00 | 0.56 | 0.79 | 0.013 | 0.40 | 0.82 |
| $\begin{aligned} & \text { PM } 3.415 \\ & \text { to } 3.330 \\ & \hline \end{aligned}$ | From El Toro Road to Anneliese's School | 6 | 0 | 2 | 2 | 0.00 | 0.74 | 2.23 | 0.013 | 0.40 | 0.82 |

[^0]Source: LCR Traffic Engineering Performance Assessment (March 30, 2022) Table 3-4

## Southbound SR-133

As shown in Tables 9 and 10, there were a total of 63 collisions in the SB direction recorded on SR-133 within the Project limits, with 36 injury collisions and no fatality collision. The majority of the collisions were rear ends and hit objects corresponding to approximately 41 percent and 24 percent of the total collisions, respectively. In addition, one auto-pedestrian collisions were recorded from LCAD Main Campus Driveway to Stan Oaks Drive.

Similar to the NB direction, as shown in Table 9, the total actual collision rate for each of the four SB segments are approximately double the statewide average collision rates for similar facilities.

## Table 10: Summary of Accident Types

| Post Mile <br> (PM) | Location | $\begin{aligned} & \text { Accid } \\ & \text { ent } \\ & \text { Type } \end{aligned}$ |  | $\begin{aligned} & \stackrel{0}{2} \\ & \frac{0}{3} \\ & \frac{0}{6} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{.}{0} \\ & \stackrel{\rightharpoonup}{0} \\ & 0 \\ & \dot{E} \end{aligned}$ | \% | 皆淢 | ¢ | ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} 0.94 \\ \text { to } \\ 1.573 \end{gathered}$ | From Canyon Acres Drive to Laguna Canyon Arts and Design | Total | 3 | 4 | 22 | 3 | 2 | 1 | 0 | 0 | 35 |
|  |  | \% | 8.6\% | 11.4\% | 62.9\% | 8.6\% | 5.7\% | 2.9\% | 0.0\% | 0.0\% | 100\% |
| $\begin{gathered} 1.573 \\ \text { to } \\ 2.446 \end{gathered}$ | From LCAD Main Campus Driveway to Stan Oaks Drive | Total | 3 | 5 | 11 | 6 | 3 | 1 | 1 | 0 | 30 |
|  |  | \% | 10.0\% | 16.7\% | 36.7\% | 20.0\% | 10.0\% | 3.3\% | 3.3\% | 0.0\% | 100\% |
| $\begin{aligned} & \hline 2.446 \\ & \text { to } \\ & 3.330 \\ & \hline \end{aligned}$ | From Stan Oaks Drive to Anneliese's School | Total | 2 | 3 | 20 | 4 | 4 | 1 | 1 | 1 | 36 |
|  |  | \% | 5.6\% | 8.3\% | 55.6\% | 11.1\% | 11.1\% | 2.8\% | 2.8\% | 2.8\% | 100\% |
| $\begin{gathered} 3.330 \\ \text { to } \\ 3.415 \end{gathered}$ | From Anneliese's <br> School to El Toro Road | Total | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
|  |  | \% | 0.0\% | 0.0\% | 0.0\% | 50.0\% | 50.0\% | 0.0\% | 0.0\% | 0.0\% | 100\% |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} 1.573 \\ \text { to } \\ 0.94 \end{gathered}$ | From LCAD Main Campus Driveway to Canyon Acres Drive | Total | 2 | 2 | 4 | 0 | 4 | 2 | 0 | 2 | 16 |
|  |  | \% | 12.5\% | 12.5\% | 25.0\% | 0.0\% | 25.0\% | $\begin{gathered} 12.5 \\ \% \end{gathered}$ | 0.0\% | $\begin{gathered} 12.5 \\ \% \end{gathered}$ | 100\% |
| $\begin{gathered} 2.446 \\ \text { to } \\ 1.573 \\ \hline \end{gathered}$ | From Stan Oaks Drive to LCAD Main Campus Driveway | Total | 3 | 0 | 7 | 0 | 6 | 0 | 1 | 0 | 17 |
|  |  | \% | 17.6\% | 0.0\% | 41.2\% | 0.0\% | 35.3\% | 0.0\% | 5.9\% | 0.0\% | 100\% |
| $\begin{gathered} 3.330 \\ \text { to } \\ 2.446 \\ \hline \end{gathered}$ | From Anneliese's School to Stan Oaks Drive | Total | 2 | 2 | 13 | 0 | 3 | 3 | 0 | 1 | 24 |
|  |  | \% | 8.3\% | 8.2\% | 54.2\% | 0.0\% | 12.5\% | $\begin{gathered} 12.5 \\ \% \end{gathered}$ | 0.0\% | 4.2\% | 100\% |
| $\begin{gathered} 3.415 \\ \text { to } \\ 3.330 \\ \hline \end{gathered}$ | From El Toro Road to Anneliese's School | Total | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 0 | 6 |
|  |  | \% | 0.0\% | 33.3\% | 33.3\% | 0.0\% | 33.3\% | 0.0\% | 0.0\% | 0.0\% | 100\% |

Source: Caltrans District 12 TASAS Selective Accident Retrieval (TSAR) (January 2016 to December 2020)
Bold indicates most occurring accident
Bold Red indicates second most occurring accident
Source: LCR Traffic Engineering Performance Assessment (March 30,2022) Table 3-5

Based on the analysis above, it is anticipated that the improvements proposed under Alternatives 2, 3, 4, and 5 including: (1) the removal of overhead utility poles and other obstacles located along the edge of the roadway; (2) improved shoulders; and (3) the introduction of separate bike and pedestrian facilities, would alleviate the identified deficiencies along the route and potentially decrease collision rates.

## Traffic Engineering Studies

The TEPA report provides a summary of the existing deficiencies along the SR-133 corridor and discusses and analyzes possible alternatives to determine the operational feasibility of each alternative. A detailed operational analysis and traffic report will be prepared during the PA/ED phase. The analysis will include capacity, delay, queuing, LOS, signal warrants, and safety analysis.

## 5. DEFICIENCIES

The SR-133 corridor within the Project limits experiences substantial congestion at two bottleneck locations during the period of high visitor travel to the City. These periods include most summer weekends and holidays. Additionally, congestion is observed during a typical weekday peak period without high visitor travel. The two bottlenecks occur along the SB travel lane just south of the Laguna Canyon Road (SR-133)/El Toro Road intersection, and along the NB travel lane just north of Canyon Acres Drive where SR-133 transitions from two northbound lanes to one. Improvements are currently proposed under separate projects for both locations as further discussed in Section 6, below.

This segment of LCR consists of one 12 -foot-wide travel lane in each direction, a 10-foot-wide nonstandard center two-way left turn lane, nonstandard shoulders, and limited on-street parking. Although no additional travel lanes are proposed with the Project under Build Alternatives 2 to 4, multimodal capacity of the corridor will improve significantly due to the addition of bike, pedestrian, and transit improvements.

Sidewalks or dedicated pedestrian paths do not exist along SR-133 within the Project limits, with the exception of a 0.2 -mile-long sidewalk on the east side of SR-133 near the Laguna Beach Dog Park. Pedestrian access is limited to the paved shoulder next to the traffic lanes or in dirt areas adjacent to nonstandard shoulders. A large number of bicyclists utilize SR-133 within the Project limits. These bicyclists have limited access on narrow, nonstandard paved shoulders that are separated from traffic lanes only by a travel way edge stripe.

The properties along NB SR-133 consist predominantly of residential and commercial land uses, many of which have direct driveway access to and from SR-133. SB SR-133 includes several satellite parking lots. Vehicular congestion and queuing, and inadequate gaps during peak traffic periods create difficulty for left-turning vehicles accessing these driveways and parking lots. This issue is compounded through the 'Big Bend' area, where restricted sight distance through the horizontal curves can create
difficulty for left-turning vehicles to find adequate gaps in traffic to make a safe leftturn movement through the oncoming traffic stream.

The availability of public parking is highly constrained throughout the City. City transit and trolley services make a critical contribution in improving traffic circulation by removing additional vehicles from utilizing the corridor, especially during the peak summer season. The City Maintenance Yard Parking Lot located at the southern end of the Project limits primarily serves as a park-and-ride location for the trolley service during summer months. Vehicular congestion and queuing, coupled with inadequate gaps during peak periods, makes ingress and egress difficult for vehicles and the trolley service accessing this lot.

Overhead utilities exist along both sides of LCR through most of the corridor within the Project limits. These overhead utility poles, and other fixed objects along the edge of the roadway in both directions, are located within the CRZ, increasing the risk of collisions with errant vehicles.

## 6. CORRIDOR AND SYSTEM COORDINATION

The proposed Project improvements are consistent with the state, regional and local mobility goals, and objectives, and are being coordinated with the responsible governmental, regulatory, and local agencies in the area to ensure consistency with their regional plans.

The following project is proposed by Caltrans within the Project limits:

| EA \# | Project Limits | Scope of Work | Status |
| :--- | :--- | :--- | :--- |
| 12-0P94U4 | El Toro Road to <br> SR-73 <br> (PM 3.1/R4.1) | Provide two lanes on NB SR-133 between El <br> Toro Road and SR-133/73 Interchange by <br> extending the second NB lane by 600 feet and <br> extending the SB merge lane by 900 feet south <br> of El Toro Road; and provide two left-turn lanes <br> on SB El Toro Road at SR-133; Construct 8 foot <br> shoulder in both directions (status: In <br> Construction) | Construction |

The proposed improvements for the above projects have been assumed to be an existing condition for this Project.

## Regional and System Planning

The State of California's TCR for SR-133 anticipates that "SR 133 will experience increased traffic from regional growth and recreational travel" and states that "improving safety and circulation for all modes of transportation is a key focus for the SR 133 corridor." Between Canyon Acres Drive and El Toro Road (which the TCR designates as Segment 4), the TCR indicates that potential opportunities for improvements "may include adding a lane in one or both directions, or a roundabout at
one or several locations." In addition, anticipated development within the City of Irvine at the northern end of LCR near I-405 "may necessitate system operations and management concepts such as implementation of complete streets, and strategies to respond to traffic impacts from new developments to maintain safe and efficient access for all users. These improvements may include safety spot improvements, limitation and separation of left turn movements, reduction of driveways and access points (typically done with re-development) reduction or combination, right turn pockets, bus turn-outs, signal synchronization and other Transportation Management System (TMS) improvements." In short, the State anticipates that the portion of LCR within the Project limits may need some combination of complete streets improvements, safety enhancements, traffic capacity enhancements, and property access management to serve the future multimodal user needs of the corridor.

OCTA's 2014 Long Range Transportation Plan includes multimodal corridor improvements between El Toro Road and Canyon Acres Drive. OCTA is currently updating this plan. The 2022 Long Range Transportation Plan is expected to be finalized in Fall of 2022.

SR-133 between El Toro Road and Canyon Acres Drive is listed for multimodal corridor improvements in the adopted 2020 Regional Transportation Plan/Sustainable Communities Strategy (RTP/SCS) Strategic Projects list developed by the Southern California Association of Governments (SCAG)(RTP ID S2160012). Future improvement projects must be in the adopted RTP/SCS financially constrained list of projects to be eligible for state and federal funding.

The build alternatives are also consistent with applicable City General Plan goals and policies to provide a safe circulation system for all users while protecting and encouraging bicycle and pedestrian travel.

## 7. ALTERNATIVES

Five alternatives were analyzed for the Project: one No-Build Alternative and four Build Alternatives, which include varying design configurations. No additional travel lanes are proposed for the Project. Each of the proposed Build Alternatives include a combination of the following elements:

- Undergrounding existing overhead utility lines outside travel lanes
- On-street and/or off-street bicycle facilities
- Emergency lanes
- ADA compliant pedestrian facilities (curb ramps, sidewalks/paths, and driveways)
- Removal of the existing High-Intensity Activated Crosswalk Beacon (HAWK)
- Improved shoulders
- Improved bus stops/turnouts
- Off-street parking
- New curb and gutter
- Cold Plane and place asphalt concrete overlay
- Drainage improvements
- Remove existing MBGR and install new MGS
- Install bike trail flexible posts
- Lighting and sign illumination
- Pavement delineations and signs

In addition to the project elements above, intersection improvements common to the four Build Alternatives are proposed at the following locations along SR-133:

- City Maintenance Yard Driveway - Southbound right-turn pocket and driveway entrance modifications

At the northern project limits, bike lanes would conform to the proposed improvements at the El Toro Road Intersection (see Section 6; Caltrans Project EA 12-0P94U4, El Toro Road to SR-73). At the southern project limit, Canyon Acres Drive, cyclists would continue southbound along SR-133 as they do today or cross at the Canyon Acres Drive signalized intersection to access downtown Laguna Beach.

Due to the ROW constraints and varying available width along the corridor as described in Section 3A (Existing Facility), the proposed improvements evaluated for all three Build Alternatives consist of a 64-foot-wide typical section for the majority of the Project's length with the exception of the constrained area in the vicinity of the 'Big Bend' where a 53 -foot to 58 -foot typical section is proposed depending on the alternative. Layouts and Typical Sections for the proposed three Build Alternatives are provided in Attachment B.

The proposed Build Alternatives are consistent with the recommendation identified in Caltrans' June 2014 TCR for this segment of SR-133, including widened shoulders, where feasible, to better accommodate bicyclists and pedestrians, and to promote the development of integrated multimodal projects in balance with community goals, plans and values.

## Project Alternatives

Additional details of each alternative are provided below:

## Alternative 1-No-Build Alternative

The No-Build Alternative would maintain LCR in its current condition. No improvements would be implemented at this time; therefore, no capital costs are associated with this alternative. Utility poles on both the NB and SB sides of the road would not be undergrounded to allow full use of the State ROW for complete street elements to be incorporated into the corridor that encourage increased use of active modes of transportation. As the traffic demand increases, traffic operation will further deteriorate, which may result in an increase in congestion, vehicle queuing, vehicle delay, and safety issues. This alternative would not satisfy the Purpose and Need of the Project.

The No-Build Alternative includes the improvements proposed by Caltrans for the Canyon Acres Drive Intersection and the El Toro Road Intersection improvements as further described in Section 7 of this PSR/PDS.

The No-Build Alternative is being considered because it serves as the baseline against which to evaluate the effectiveness of the proposed Build Alternatives. This alternative allows decision makers to make a comparison between the impacts of the Build Alternatives and the impacts of the No-Build scenario.

## Alternative 2

Alternative 2 generally consists of a typical width of 64 to 65 feet for the majority of the route including the vehicle, pedestrian and bicycle facilities. This alternative includes narrowed 11 -foot travel lanes, a 10 -foot center dual left-turn lane, 7 -foot shoulders in both the NB and SB directions, and a pedestrian path/sidewalk on the NB side. Alternative 2 also includes a 10 - to 12 -foot wide, two-way Class I bikeway on the SB side of the roadway. Flexible posts would be located within the buffer area between the bike lane and travel way. During emergencies, there is space for four outbound evacuation travel lanes on the roadway and one inbound emergency vehicle lane by utilizing the bike lane. The bikeway/pedestrian path on the SB side of the roadway would have openings, which would allow emergency vehicles to traverse the curb.

Within the constrained segment in the vicinity of the 'Big Bend,' the NB and SB shoulders are eliminated, and the adjacent bikeway becomes a Class I two-way, shareduse path with pedestrians and a narrower buffer. At the pinch point of 53 feet available ROW width, the NB shoulder would end within this short segment.

Alternative 3 (former September 8, 2015, Task Force Final Report Alt. F)
Alternative 3 generally consists of a typical width of 64 feet for most of the route, including the vehicle, pedestrian, and bicycle facilities. This alternative includes narrowed 11-foot travel lanes, a 10-foot center dual left-turn lane, a 7 -foot Class II bike lane, and a pedestrian path/sidewalk on the NB side of the roadway. Alternative 3 also includes a Class I bikeway on the SB side of the roadway. Portions of the SB side of the roadway have a 5 -foot pedestrian sidewalk. Flexible posts would be located within the buffer area between the bike lane and travel way. During emergencies, there is space for three outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lane. The bikeway/pedestrian path on the SB side of the roadway would have openings, which would allow emergency vehicles to traverse the curb.

Within the constrained segment in the vicinity of the 'Big Bend,' the dedicated pedestrian path on the SB side of the roadway would be eliminated and the buffer between the shared-use, two-way Class I bike path and the SB travel lane would be narrowed. At the pinch point of 53 feet available ROW width, the 7 -foot Class II bike lane on the NB side would be removed within this short segment.

## Alternative 4 (former September 8, 2015, Task Force Final Report Alt. G)

Alternative 4 generally consists of a typical width of 64 feet for most of the route including the vehicle, pedestrian, and bicycle facilities. This alternative includes 12foot travel lanes, and a 10 -foot center dual left-turn lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5- to 7-foot Class II buffered bike lane/shoulder on both sides of the roadway. During emergencies, there is space for four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes.

Within the constrained segment in the vicinity of the 'Big Bend,' the bike lane widths would be reduced to five feet and the travel lanes reduced to 11 feet. At the pinch point of 53 feet available ROW width, the pedestrian paths and bike lane buffers on either side of the roadway would be reduced within this short segment.

## Alternative 5 (Recommended for Programming)

Alternative 5 introduces a reversible lane that would provide a peak-direction capacity to a two-way road and decrease congestion by borrowing available lane capacity from the other (off-peak) direction. This alternative generally consists of a typical width of $64-\mathrm{ft}$. including the vehicle, pedestrian, and bicycle facilities. It would include 12 -foot travel lanes and a 12- to 14 - foot center reversible lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5 -foot Class II buffered bike lane on both sides of the roadway. During emergencies, there is space for four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes.

## Nonstandard Design Features

There are nonstandard features that have been identified in the No-Build and proposed Build Alternatives based on Caltrans Highway Design Manual (HDM) 6th Edition standards. Further analysis will be performed in the PA/ED phase and Design Standard Decision Documents (DSDD) will be prepared and further analyzed to document the nonstandard features prior to completion of the PA/ED phase for the Project. Tables $\mathbf{1 1 \&} \mathbf{1 2}$ include a listing of the identified nonstandard design features for the No-Build and Build Alternatives including the probability of approval and justification.

Table 11: Design Standards Risk Assessment

| Bold Design Standards Risk Assessment |  |  |  |
| :---: | :---: | :---: | :---: |
| Alternative | Design Standard from Highway Design Manual Tables 82.1A \& 82.1B | Probability of Nonstandard Design Feature Approval (None, Low, Medium, High, | Justification for Probability Rating |
| $2,3,4, \& 5$ | 201.1 - Stopping Sight Distance Table 201.1 shows the minimum standards for stopping sight distance related to design speed for motorists. <br> - Various Locations | Medium | Based on the existing alignment for this road, standard stopping sight distance may not be possible. Stopping sight distance will be improved from the existing condition when feasible, but the roadway centerline is not planned to be revised from its existing alignment due to utility and right of way impacts. |
| $2,3,4, \& 5$ | 202.2 - Standards for <br> Superelevation- <br> Table 202.2D Minimum Radii for <br> Design Superelevation Rates, <br> Design Speeds, and emax $=10 \%$ <br> - Sta. $102+06$ to $114+21$ | Medium | The roadway centerline is proposed to maintain its existing alignment and superelevation. As such the standard radii and standard superelevation rates would not be achieved. The feasibility of meeting this standard will be explored in the PA/ED phase of project. |
| $2,3,4, \& 5$ | 301.1 - Lane Width- <br> The minimum lane width on twolane and multilane highways, ramps, collector-distributor roads, and other appurtenant roadways shall be 12 feet <br> - Throughout Project | Medium | Lane widths are proposed to be reduced to 11 ft to provide traffic calming within the project area and to accommodate proposed bike and pedestrian facilities. Where feasible 12 ' lanes will be provided adjacent to bike lanes. Improved shoulders, bike and pedestrian facilities will be provided as part of this project. |
| $2 \& 3$ | 302.1 - Shoulder Width- <br> The table widths given in Table 302.1 shall be the minimum continuous usable width of paved shoulder on highways. <br> - Throughout Project | Medium | The existing shoulders vary from $0 \mathrm{ft}-6 \mathrm{ft}$. Project improvements include increasing the width of the existing non-standard shoulders and providing improved bike and pedestrian paths. |
| $2 \& 3$ | 309.1(3)(a)- Minimum Clearance- <br> The minimum horizontal clearance to all objects, such as bridge rails and safety shaped concrete barriers, as well as sand-filled barrels, guardrail, etc., on all freeway and expressway facilities, including auxiliary lanes, ramps, and collector-distributor roads, shall be equal to the standard shoulder width of the highway facility as stated in Table 302.1. <br> - Various Locations | Medium | Maximizing horizontal clearances between roadside objects and the edge of traveled way, will be provided when feasible. Project improvements include increasing the width of the existing nonstandard shoulders and providing improved bike and pedestrian paths. |


| Bold Design Standards Risk Assessment |  |  |  |
| :---: | :---: | :---: | :---: |
| Alternative | Design Standard from Highway Design Manual Tables 82.1A \& 82.1B | Probability of Nonstandard Design Feature Approval (None, Low, Medium, High,) | Justification for Probability Rating |
| $2 \& 3$ | 1003.1 Class I Bikeways (Bike Paths)(1)(b) - Widths and Cross Slopes - Shoulder <br> A minimum 2-foot wide shoulder, composed of the same pavement material as the bike path or all weather surface material that is free of vegetation, shall be provided adjacent to the traveled way of the bike path when not on a structure <br> - Throughout Project in various locations | Medium | 2-foot wide shoulders will be provided where feasible. Class I Bikeways are proposed where none exist today. Alternatives 2 \& 3 provides an option for an off-street bike path where the other Alternatives $4 \& 5$ provide a options for on-street Class II bike lanes. Overall safety improvement and other factors (conflict points, speed and volume) would be taken into consideration between these two options. |
| $2 \& 3$ | 1003.1 Class I Bikeways (Bike Paths)(7) - Bike Paths Parallel and Adjacent to Streets and Highways <br> The minimum separation between the edge of traveled way of a oneway or a two-way bicycle path and the edge of traveled way of a parallel road or street shall be 5 feet plus the standard shoulder width. Bike paths within the clear recovery zone of freeways shall include a physical barrier separation. <br> - Throughout Project in various locations | Medium | Class I Bikeways are proposed where none exist today. Design will take into consideration conflicts that may arise at intersections and public transit facilities. Alternatives $2 \& 3$ provides an option for an off-street bike path where the other Alternatives $4 \& 5$ provide options for on-street Class II bike lanes. The AASHTO Highway Safety Manual will be used to justify the best cross section of roadway, bicycle and pedestrian facilities. |

Table 12: Underline Design Standards Risk Assessment

| Underlined Design Standards Risk Assessment |  |  |  |
| :---: | :---: | :---: | :---: |
| Alternative | Design Standard from Highway Design Manual Tables 82.1A \& 82.1B | Probability of Nonstandard Design Feature Approval (None, Low, Medium, High, | Justification for Probability Rating |
| 2, 3, 4, \& 5 | 105.2 - Sidewalks and <br> Walkways- <br> The minimum width of a sidewalk should be 8 feet between a curb and a building when in urban and rural main street place types. For all other locations the minimum width of sidewalk should be 6 feet when contiguous to a curb or 5 feet when separated by a planting strip. <br> Throughout Project | Medium | Sidewalks or dedicated pedestrian paths do not exist along SR-133 within the Project limits, with the exception of a 0.2 -mile long sidewalk on the east side of SR-133 near the Laguna Beach Dog Park. The proposed 5 ft sidewalk meets the City standard for sidewalk width and also complies with the ADA minimum standard width of 4 ft . |
| 2, 3, 4, \& 5 | 202.5(1) - Superelevation <br> Transition- <br> A superelevation transition should be designed in accordance with the diagram and tabular data shown in Figure 202.5A to satisfy the requirements of safety, comfort and pleasing appearance <br> - Various Locations | Medium | Based on the existing alignment for this road, standard superelevation transitions may not be possible due to existing small radius reversing curves. |
| 2, 3, 4, \& 5 | 202.5(2) - Superelevation runoff-Two-thirds of the superelevation runoff should be on the tangent and one-third within the curve. <br> - Various Locations | Medium | Based on the existing alignment for this road, standard superelevation runoff may not be possible due to existing small radius reversing curves. |
| 2, 3, 4, \& 5 | 203.6 - Reversing curves- <br> When horizontal curves reverse direction the connecting tangents should be long enough to accommodate the standard superelevation runoffs given on Figure 202.5A. If this is not possible, the 6 percent per 100 feet rate of change should govern (see Index 202.5(3)). <br> - Sta $100+43$ to $102+06$ | Medium | The existing roadway alignment includes tight radius reversing horizontal curves located just south of the Castle Rock Road intersection. Roadway widening conforms to the existing roadway centerline. |

## Transportation Management Plan

Due to the topography constraints of the canyon, lack of adequate detour routes in and out of the City, and required access to the commercial, residential, and recreational land uses along the corridor, a minimum of one lane of through traffic in each direction would need to be maintained throughout the construction duration. It may be necessary to temporarily close driveways at night during Project construction.

The closest parallel detour routes to access PCH north and south of the City from inland locations are via Newport Coast Drive to the north and Crown Valley Parkway to the south.

Proposed Transportation Management Plan (TMP) elements that would mitigate traffic impacts during construction and their associated costs are listed in the attached Preliminary TMP Data Sheet (Attachment E). Due to the similarity of the proposed improvements, the TMP Data Sheet is considered common to all four Build Alternatives for this phase. The TMP Data Sheet will be further developed during the PA/ED phase to recommend specific methods of reducing construction and circulation impacts. The Plans, Specifications, and Estimates (PS\&E) package will include detailed detour, staging, and traffic handling plans.

## Construction Staging

It is anticipated that the Project will be constructed in three general stages. For Stage 1, traffic lanes would be shifted to the SB side of the roadway. Construction of the underground distribution lines and NB side of the roadway would be constructed a portion at a time in order to maintain access to all properties.


Figure 1 - LCR Construction Stage 1

For Stage 2, traffic would be shifted to the NB side of the roadway that was constructed in the previous stage. K-rail barrier would be placed for most of the length of the Project to construct the underground transmission lines and bike path.


Figure 2 - LCR Construction Stage 2
For Stage 3, construction of the overlay within the existing pavement area would be completed in sections during non-peak hours. Temporary traffic control would be used for this construction to cold plane and place the asphalt overlay.


Figure 3 - LCR Construction Stage 3
A minimum of one 11-foot lane of through traffic in each direction and access to local business, schools and residential properties would be maintained throughout the construction duration.

## Stormwater BMPs

A Storm Water Data Report (SWDR) has been prepared to accompany this PSR/PDS (Attachment F). The anticipated stormwater project risk level is Level 2. The SWDR recommends the implementation of treatment best management practices (BMPs) to treat the project targeted design pollutants. It is anticipated that post-Project State ROW
will provide adequate area for BMPs. This will be confirmed during the PA/ED and PS\&E phases. The SWDR will be updated during both the PA/ED and PS\&E phases to confirm the risk level, disturbed soil area, change in amount of impervious area, and specific BMPs to be implemented for design pollution prevention and treatment, if needed. The construction contractor will prepare and implement a Storm Water Pollution Prevention Plan (SWPPP) to address construction site BMPs. For this phase, permanent BMPs have been evaluated from a corridor scoping level.

The limits of the proposed project are within the jurisdiction of the San Diego Regional Water Quality Control Board (RWQCB). The receiving water body for the proposed project is Laguna Canyon Channel, which is not 2020/2021 CWA section 303(d) listed as being impaired. However, the project is located within the Twenty Beaches and Creeks Total Maximum Daily Load (TMDL) as identified in Attachment IV of the Caltrans Statewide NPDES Permit. Since this project discharges to an area with an established TMDL, any runoff treated in excess of the new impervious area created by the project may be claimed as a Compliance Unit (CU) to meet Caltrans NPDES permit requirements for achieving the TMDL compliance strategy. The project is located within and is contiguous to the Coastal Zone.

This project must conform to all applicable water quality regulations and/or permit requirements of the State Water Resources Control Board (SWRCB) and the local Santa Ana Regional Water Quality Control Board (RWQCB), including, but not limited to, the Caltrans Statewide NPDES Permit (Order No. 2014-0077-DWQ) amending (Order No. 2012-0011-DWQ, NPDES No. CAS000003), the Statewide General NPDES Permit for Construction Activities (Order No. 2012-0006-DWQ) amending (Order No. 2009-0009-DWQ, NPDES No. CAS000002), the Caltrans Storm Water Management Plan (December 2015 revision), and any subsequent revision and/or additional requirements at the time of construction. Should dewatering be required, dewatering must comply with the San Diego Regional Water Quality Control Board's Order R9-2015-0013, NPDES Permit No. CAG919003 for general water discharge requirements for groundwater extraction discharges to surface waters within the San Diego Region.

## Project Costs

Project costs for the four Build Alternatives are summarized in Table 13. Preliminary cost estimates are included as Attachment C. Estimated project support costs are summarized in Section 12.

Table 13: Project Cost Summary*

|  | Alternative 2 | Alternative 3 | Alternative 4 | Alternative 5 |
| :---: | :---: | :---: | :---: | :---: |
| Roadway Items | \$39,356,214 | \$38,104,247 | \$39,679,059 | \$40,265,628 |
| Structures Items | \$0 | \$0 | \$0 | \$0 |
| SUBTOTAL CONSTRUCTION | \$39,356,214 | \$38,104,247 | \$39,679,059 | \$40,265,628 |
| Right-of-way Acquisition | \$5,817,985 | \$6,347,159 | \$6,501,125 | \$9,319,186 |
| Electrical Undergrounding | \$56,486,000 | \$56,486,000 | \$56,486,000 | \$56,486,000 |
| Other Utilities | \$11,895,000 | \$11,895,000 | \$11,895,000 | \$11,895,000 |
| SUBTOTAL ROW | \$74,198,985 | \$74,728,159 | \$74,882,125 | \$77,700,186 |
| PA/ED Support | \$4,375,000 | \$4,375,000 | \$4,375,000 | \$4,375,000 |
| PS\&E Support | \$5,000,000 | \$5,000,000 | \$5,000,000 | \$5,000,000 |
| ROW Support | \$2,721,875 | \$2,860,625 | \$3,178,750 | \$3,846,875 |
| Const. Management | \$5,000,000 | \$5,000,000 | \$5,000,000 | \$5,000,000 |
| SUBTOTAL SUPPORT COSTS | \$17,096,875 | \$17,235,625 | \$17,553,750 | \$18,221,875 |
| TOTAL PROJECT COST | \$130,652,074 | \$130,068,031 | \$132,114,934 | \$136,187,689 |

*Escalated values 4\% per year to mid-point of construction (Year 2029)

## Alternatives Considered and Withdrawn

A total of nine preliminary alternatives were developed during the PSR/PDS process for consideration by the Project Development Team (PDT) including SR-133/Laguna Canyon Road Task Force Alternatives F and G (see Section 2B - Community Interaction). The nine preliminary alternatives in addition to the No-Build were evaluated based on the following general criteria, which encompass operational and safety improvements as well as active transportation elements along the corridor:

- Undergrounding Outside Travel Lanes/Safety
- Off-Street Bicycle Facilities
- Pedestrian Sidewalk or Path
- Bus Stop Compatibility
- Emergency Access
- Breakdown Shoulder
- On-Street Bicycle Facilities
- On-Street Parking

Each preliminary alternative was evaluated by applying a weighted score to each of the above criteria. The top three scoring alternatives were carried on and further refined into Build Alternatives 2, 3 and 4. The six lowest scoring alternatives were dropped from further consideration (see Attachment G-Alternatives Screening Process and Evaluation Matrix).

## 8. RIGHT-OF-WAY

ROW Data Sheets for the four Project Build Alternatives and one No Build Alternative are included in Attachment H. Attachment C provides the Conceptual Cost Estimate - Right-of-Way Component.

The acquisition of permanent easements and temporary easements are proposed for all Build Alternatives. All permanent easements are proposed to be partial acquisitions and include both private parcels and public parcels controlled by the County of Orange. Temporary easement would be required for all Build Alternatives. These temporary easements are needed mostly for construction of proposed adjacent sidewalks along the entire roadway. For estimating purposes, it is assumed that the temporary easement will need a width of 10 ' of each parcel's frontage adjacent to proposed sidewalk. It is also assumed that the easements will be needed for a three-year period. The government owned properties needed for construction purposes are proposed to be procured through each government entities' permitting process. Costs for these properties include only the services needed to obtain the permits. There are no railroad facilities or right of way affected. There are no proposed displacements that would require relocations. There are no expected dedications.

For the build alternatives (Alternatives 2-5) right of way impacts vary. Table 14 provides a summary of the highway easement and TCEs proposed for each build alternative.

## Table 14: Proposed Permanent and Temporary Easements for Build Alternatives

| Alternative | Permanent <br> Easements |  | Temporary <br> Easements |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\#$ | Total sf | $\#$ | Total sf |
| 2 | 2 | 5,100 | 83 | 188,898 |
| 3 | 2 | 6,760 | 85 | 195,708 |
| 4 | 18 | 7,605 | 78 | 186,954 |
| 5 | 29 | 24,672 | 86 | 192,669 |

## Utilities (Build Alternatives 2, 3, 4 and 5)

Impacted utilities are similar for each of the alternatives. A preliminary utility investigation was performed as part of the PSR/PDS. Potential utility owners with known facilities within the corridor were contacted to attain information about their existing facilities. Based on the gathering of that information, the following types of facilities and owners are present within the Project limits:

| Utility | Owner |
| :--- | :--- |
| Water | Laguna Beach County Water District |
| Sewer | City of Laguna Beach |
| Telephone/Communications | Cox Communications <br> Extenet Systems, Inc. <br> Crown Castle <br>  <br> Sprint <br> T Mobile USA <br> Frontier |
| Electrical | Southern California Edison (SCE) |
| Storm Drain | City of Laguna Beach <br> OC Flood Control Division |
| Gas | Southern California Gas/Sempra Utilities |

Coordination with the identified utility companies will be carried out during the subsequent phases. Preliminary utility sheets are provided in Attachment B. For programming purposes, it is assumed that all proposed Build Alternatives will impact the existing facilities. The specific facilities and owners in conflict with the proposed Build Alternatives, and their subsequent need for relocation and proposed location is further discussed below. Final utility dispositions will be confirmed and coordinated during the PA/ED phase.

SR-133 between El Toro Road and Canyon Acres Drive is included on the Statewide Construction Evaluation Map for the Middle-Mile Broadband Initiative. Further investigation will be completed during the PA/ED to determine locations of ducts that can be included in the statewide Broadband Middle-Mile Network.

## Utility Undergrounding

## Transmission and Distribution Lines (SCE)

The Project limits contain approximately 2.5 pole-miles of SCE transmission, distribution, and joint-use poles that would require undergrounding. The $66-\mathrm{kV}$ transmission lines are primarily on wood poles, and for the most part, located on the NB side of SR-133 with sections also located on the SB side. Overhead distribution lines are installed as 'underbuilds' on the same poles as the $66-\mathrm{kV}$ transmission lines. At some locations, the distribution lines are on separate poles. The distribution lines consist of primary lines with the voltage ranging from 12 to 25 kV and secondary lines with the voltage being 120 to 240 V normally for residences and 208 V or 480 V services for businesses. A portion of the distribution lines in the vicinity of the 'Big Bend' area were undergrounded by SCE in 2016. The locations of the existing power lines along the Project alignment are shown in the Existing Utility Plans included in Attachment B.

The $66-\mathrm{kV}$ transmission lines are proposed to be placed underground in a utility trench along the SB side of the roadway. This arrangement would allow for distribution lines to be placed within a utility trench on the NB side of the roadway since the existing residences and businesses are mostly located on the NB side. The design for both underground transmission and distribution lines will be coordinated with SCE and Caltrans and will depend on the proposed improvements. The standard underground duct banks used by SCE consists of PVC conduits encased in concrete with a 3-foot depth of cover over the bank. The proposed trench locations are shown in the Typical Cross Sections included in Attachment B.

Conversion of overhead electric facilities to underground will require the use of manholes or vaults used for splicing cables. Standard underground transmission vaults used by SCE are precast concrete spaced approximately every 2,000 feet along the alignment with approximate dimensions of $20^{\prime} \times 10^{\prime} \times 10^{\prime}$ in length, width, and height. Underground vaults for splicing distribution cables are precast concrete and normally spaced approximately 1,000 feet apart. The vaults would vary in size depending on the number and size of cables. Transformers and switching equipment will be required to convert the distribution voltage for residential and businesses use and can be placed either above ground or in underground vaults.

Due to the constrained existing corridor ROW width, manholes or vaults are proposed to be located within the bike lanes, sidewalks, and pedestrian paths, or in landscaped areas within the existing ROW outside the travel lanes and would be traffic loading rated.

Other considerations for converting the existing overhead electrical facilities to underground include, but are not limited to:

- Installation of transition poles on either end of the Project and along lateral roads to convert from underground back to overhead
- Undergrounding of electrical transmission and distribution line taps or connections to other overhead lines to the next available existing poles or to a new pole set at certain distances from the edge of the improvement
- Conversion of overhead services to residents and businesses to underground
- Conversion or replacement of the customer panel boxes to accept the underground service
- Improvements at the SCE Morro Substation located approximately 1,200 feet south of the Canyon Acres Drive intersection

The placement of the underground electrical lines will depend upon the number and location of existing underground substructures such as storm drains, sewer lines, water lines, gas lines, and others such as pipelines. These existing underground substructures will most likely dictate the alignment and placement of the duct banks and vaults required to underground the overhead electrical facilities. Consequently, the configuration, design, and ROW/easement requirements of the underground lines will
need to be determined during the subsequent PA/ED phase and will need to be further coordinated with Caltrans, SCE and the other utility owners.

## Telecommunication Facilities (Cox, Extenet, Crown Castle, Sprint, T-Mobile, Frontier)

There are approximately 2.5 pole-miles of overhead communication lines that run from the start to the end of the proposed improvements, for the most part on the SB side with sections also running on the NB side. The underground telecommunication lines will most likely be installed in duct banks and manholes will also be required. The telecommunication facilities are proposed to be placed in a joint trench with the electrical distribution lines. It would be preferable to place the joint trench on the NB side of the roadway since most of the businesses and/or residences are located on the NB side. This placement would minimize service conduit runs to the adjacent properties and reduce overall costs. Specific impacts to each of the communication line owners will be determined during the PA/ED phase of the project.
Streetlights (City of Laguna Beach)
The existing streetlights installed on SCE power poles are owned by SCE and will need to be relocated because of the project. The streetlights are currently fed from the overhead power lines and will be modified because of the undergrounding (see above). New underground circuits, controls, foundations, poles, and luminaires will be required, and would be installed along the proposed sidewalks and pedestrian paths. Decorative roadway lighting is an option, as well as decorative pathway lighting, based on the City's preference and available funding. The City will take ownership of the streetlights within the project limits.
Sewer (City of Laguna Beach)
The City of Laguna Beach has a sewer line along northbound side of the roadway for the length of the project. It is unknown if the sewer line can remain in place. For programming purposes, it is assumed that the sewer line will be relocated.

## Water (Laguna Beach County Water District)

The Laguna Beach County Water District has water lines on both sides of the project. It is assumed that the waterline located on the southbound side of the roadway will not require relocation because there are no apparent conflicts; however, further investigation will be required. For the northbound side of the roadway, it uncertain if the water lines can remain in place. As such, it is assumed that the waterline on the northbound side of the roadway will be relocated.

Gas (Southern California Gas)
The Southern California Gas Company (SCG) has a gas line that exists along northbound side of the roadway for the length of the project. It is uncertain if these gas lines will be impacted. It is assumed that the existing gas lines will be relocated outside of the proposed roadway for the length of the project.

## Railroad

There is no railroad involvement within the Project limits.

## 9. STAKEHOLDER INVOLVEMENT

City of Laguna Beach staff (the Project sponsor) and various functional units from Caltrans District 12 have attended the monthly PDT meetings and technical workshops to develop the purpose and need, assist in screening the proposed alternatives under consideration, and review the four proposed Build Alternatives and design options. Comments received to-date from the various stakeholder agencies with facilities along LCR, including SCE, the County of Orange Public Works, Laguna Beach County Water District, and LCAD, have been incorporated.

External stakeholder input, as well as prior assessments/studies of the corridor, have been reviewed and incorporated, as applicable. In addition, the City has continued to solicit community input and involvement with local stakeholder groups throughout the development of this PSR/PDS to balance the transportation needs of the corridor with community values. Furthermore, as described in Section 2B - Community Interaction, two of the four proposed Build Alternatives were developed in conjunction with the prior work of the SR-133/Laguna Canyon Road Task Force.

Community input will continue to be solicited during the subsequent PA/ED phase. A series of public workshops/informational meetings, as well as meetings with stakeholders and property owners, are anticipated to gain input prior to completion of the environmental document for the Project.

## 10. ENVIRONMENTAL COMPLIANCE

The preliminary environmental investigation focused on the proposed Project impacts from the four proposed Build Alternatives. Since a funding source has not been identified, environmental documentation pursuant to both CEQA and NEPA would be completed.

A Preliminary Environmental Analysis Report (PEAR) has been prepared for the Project and is included as Attachment I. A summary of environmental considerations for the Project is provided in the PEAR.

It is anticipated that the proposed Project will require the following permits and approvals:

- State Water Resources Board: National Pollutant Discharge Elimination System (NPDES) Construction General Permit for Storm Water Discharges Associated with Construction and Land Disturbance Activities
- San Diego Regional Water Quality Control Board: Section 401 Water Quality Certification
- U.S. Army Corps of Engineers: Section 404 Nationwide Permit
- California Department of Fish and Wildlife 1602 Streambed Alteration Agreement
- California Coastal Commission/City of Laguna Beach: Coastal Development Permit (State and Local Jurisdiction)
- Section 4(f) concurrence from Orange County Parks for de minimis impact determination
- California Department of Fish and Wildlife (CDFW): 1602 Streambed Alteration Agreement
- State Historic Preservation Office Consultation


## Initial Site Assessment (ISA)

The ISA Checklist for hazardous waste was completed in June 2018 and is included as Attachment J. Potential hazardous waste/materials issues associated with the proposed Project include aerially-deposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans ROW along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and pad-mounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles.

A full ISA for all ROW acquisition properties and Preliminary Site Investigations (PSI) will be conducted during the PA/ED phase.

## 11. FUNDING

Potential funding for the Project is currently being sought from federal, state, and local sources and is to be determined. Additional funding from the State ATP and State STIP may also become available at a later stage. A summary of potential funding sources and amounts identified to-date are included in Table 15. It has been determined that this project is eligible for Federal-aid funding.

Table 15: Current Capital Outlay Project Estimate

| Alternative | Range of Estimate |  | Other Funds/To Be <br> Determined |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Const. | ROW* | Const. | ROW |
| 2 | $\$ 39.4 \mathrm{M}$ | $\$ 74.7 \mathrm{M}$ | $\$ 39.4 \mathrm{M}$ | $\$ 74.7 \mathrm{M}$ |
| 3 | $\$ 38.1 \mathrm{M}$ | $\$ 74.4 \mathrm{M}$ | $\$ 38.1 \mathrm{M}$ | $\$ 74.4 \mathrm{M}$ |
| 4 | $\$ 39.7 \mathrm{M}$ | $\$ 74.9 \mathrm{M}$ | $\$ 39.7 \mathrm{M}$ | $\$ 74.9 \mathrm{M}$ |
| 5 | $\$ 40.2 \mathrm{M}$ | $\$ 77.7 \mathrm{M}$ | $\$ 40.2 \mathrm{M}$ | $\$ 77.7 \mathrm{M}$ |
| * Includes ROW acquisition and utility relocation costs |  |  |  |  |

The level of detail available to develop these capital outlay project estimates is only accurate to within the above ranges and is useful for long-range planning purposes only. The capital outlay project estimates should not be used to program or commit Stateprogrammed capital outlay funds.

## Capital Outlay Support Estimate

Capital outlay support estimate for programming for this Project is shown in Table 16, below:

Table 16: Capital Outlay Support Estimate

| Phase | Cost | Percentage |
| :---: | :---: | :---: |
| PA/ED | $\$ 4.375 \mathrm{M}$ | $3.9 \%$ |
| PS\&E | $\$ 5.0 \mathrm{M}$ | $4.4 \%$ |
| ROW | $\$ 2.72-\$ 3.85 \mathrm{M}$ | $2.4 \%-3.3 \%$ |
| Construction | $\$ 5 \mathrm{M}$ | $4.4 \%$ |
| Total | $\mathbf{\$ 1 7 . 1 - 1 8 . 2 M}$ | $\mathbf{1 5 . 1 \%} \mathbf{- 1 5 . 4 \%}$ |

## 12. DELIVERY SCHEDULE

Tentative Project schedule milestones (common to all four Build Alternatives) are as follows:

| Project Milestones |  | Scheduled Delivery Date <br> (Month/Year) |
| :--- | :---: | :---: |
| PSR/PDS Approval | M010 | October 2022 |
| Program Project | M015 | July 2023 |
| Project Report/Env. Document Approval | M200 | July 2025 |
| Complete PS\&E | M380 | January 2027 |
| Right-of-way Certification | M410 | April 2027 |
| Obtain Coastal Development Permit | --- | July 2027 |
| Ready-to-list | M460 | October 2027 |
| Advertise/Bid/Award Contract | M495 | February 2028 |
| Construction Contract Complete | M800 | February 2030 |

The anticipated funding fiscal year for construction is 2028/2029.
Project milestones listed above are used to indicate relative timeframes for planning purposes and are dependent on the identification and/or availability of funding.

The City is the lead agency for development of the Project. Caltrans will provide oversight for the duration of the Project. A Cooperative Agreement between the City and the Caltrans should be developed to define the responsibilities of each agency for the PA/ED, PS\&E, and Construction phases.

## 13. RISKS

Fourteen potential risks have been identified during the Project Initiation Document (PID) phase. While probability and impact vary with each one, these risks require close attention throughout the Project. These risks should be monitored, updated, and expanded during the PA/ED, PS\&E and construction phases. See Attachment K for the Risk Register and Table $\mathbf{1 1}$ for the nonstandard design feature risk evaluation.

## 14. EXTERNAL AGENCY COORDINATION

## Federal Highway Administration (FHWA)

The Project is not located on the interstate system, coordination with the FHWA for review and approval of project actions is not required.

The project requires the following coordination/consultation:

- State Historic Preservation Office Consultation
- Section 106 Consultation
- AB 52 Native Americans Tribal Consultation
- Section 4(f) Coordination
- Coastal Orange County NCCP/HCP or USFWS Endangered Species Act Section 7 Consultation
- Cooperative Agreements with Caltrans
- Maintenance Agreement with Caltrans
- County of Orange
- Agreements with utility companies/agencies


## 15. PROJECT REVIEWS

| NPDES | Date | 6/7/2022 |
| :---: | :---: | :---: |
| System Planning | Date | 6/6/2022 |
| Traffic Operations | Date | 6/6/2022 |
| Project Manager | Date | 5/31/2022 |
| District Safety Review | Date | 5/12/2022 |

## 16. PROJECT PERSONNEL

Principal contacts for the Project are as follows:

# City of Laguna Beach: 

Shohreh Dupuis, City Manager
(949) 497-0351

Tom Perez, Capital Programs Manager
(949) 464-6688

## Caltrans:

Lori Subida, Project Manager
(657) 328-6265

Raouf Fam, Project Engineer
(657) 328-6269

Grace Tell, Branch Chief - Advance Planning
(657) 328-6068

HDR Engineering, Inc.:
Girair Kotchian, Project Manager (714) 730-2493
Steve Crouch, Project Engineer
(714) 833-2743

Douglas Smith, Traffic
(714) 368-5635

Angie Kung, Environmental
(714) 730-2395

## 17. ATTACHMENTS

A. Location and Vicinity Maps
B. Preliminary Engineering Studies
C. Preliminary Project Cost Estimates
D. Traffic Engineering Performance Assessment (TEPA)
E. Transportation Management Plan (TMP) Data Sheets
F. Storm Water Data Report (SWDR
G. Alternatives Screening Process and Evaluation Matrix
H. Right-of-way Data Sheets
I. Preliminary Environmental Analysis Report (PEAR)
J. Initial Site Assessment (ISA) Checklist
K. Risk Register

ATTACHMENT A

## LOCATION AND VICINITY MAPS



FIGURE 1


## ATTACHMENT B

## PRELIMINARY ENGINEERING STUDIES



TYPICAL CROSS SECTIONS
TRANSMISSION
LINES DUCT BANK $\begin{aligned} & \text { Sta } \overline{96+40} \begin{array}{l}\text { TO Sta } \\ \text { Sta } \\ 107+00\end{array} \text { TO Sta } 113+50\end{aligned}$
No scale


















Sta $\overline{53+00 ~ T O ~ S t a ~} 81+50$ Sta $118+00$ TO Sta $164+60$
$\underset{\text { TRANSMISSION LINES }}{\stackrel{-}{+}}$
















EXist undergound uthlities location shown are approximate.
CIEARANCE TO EXIST UNDERGOUND UTILITIES TO BE DETERMINED.


$1 \quad \begin{aligned} & 0.10^{\prime} \mathrm{RHM} \\ & 0.75 \mathrm{AC} \\ & 0.50\end{aligned}$
$20.10^{\prime} \mathrm{OGFC}$
2. 0.50 AS (CLASS 4)

3 O.10 RHMA COLD PLANE EXISTING
AC PAVEMENT $\left(0.10^{\prime}\right)$

4


1ATTER



















Sta $\frac{\text { SR-133 }}{53+00 \text { TO Sta } 65+55}$


|  |
| :--- | :--- | :--- |

$0.10^{\prime}$ RHMA 0.75 AC
0.50 AB
$2 \begin{aligned} & 0.10^{\prime} \mathrm{OGFC} \\ & 0.40 \mathrm{ATPB}\end{aligned}$
5 AS (CLASS
$3 \begin{aligned} & 0.10^{\prime} \text { RHMA } \\ & \text { COLD P PLAN }\end{aligned}$
COLD RALANE EXISTING
AC PAVEMENT ( $\left.0.10^{\prime}\right)$

Sta 115+50 TO Sta 119+00


Sta $\frac{\text { SR-133 }}{84+50 \text { TO Sta 115 }} 5$
TYPICAL CROSS SECTIONS
ALTERNATIVE 5
no scale















## ALTERNATIVE 5

SCALE: $1^{\prime \prime}=40^{\prime} \quad$ L-13







LAGUNA CANYON ROAD




LAGUNA CANYON ROAD





## ATTACHMENT C

## PRELIMINARY PROJECT COST ESTIMATES

Type of Estimate: PSR/PDS
Project Limits: Canyon Acres Drive to El Toro Road
Project Description: SR-133 (Laguna Canyon Road) Improvements
Scope: Underground utilities, construct bike lane, construct ped path/sidewalks \& improve shoulders
Alternative : 2
SUMMARY OF PROJECT COST ESTIMATE

|  | Current Year Cost |  | Escalated Cost |  |
| :---: | :---: | :---: | :---: | :---: |
| TOTAL ROADWAY COST | \$ | 28,757,200 | \$ | 39,356,214 |
| TOTAL STRUCTURES COST | \$ | - | \$ | - |
| SUBTOTAL CONSTRUCTION COST | \$ | 28,757,200 | \$ | 39,356,214 |
| total right of way cost | \$ | 60,818,840 | \$ | 74,198,985 |
| TOTAL CAPITAL OUTLAY COSTS | \$ | 89,576,040 | \$ | 113,556,000 |
| PR/ED SUPPORT | \$ | 4,375,000 | \$ | 5,468,750 |
| PS\&E SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| RIGHT OF WAY SUPPORT | \$ | 2,721,875 | \$ | 3,402,344 |
| CONSTRUCTION SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| TOTAL SUPPORT COST | \$ | 17,096,875 | \$ | 21,371,094 |

TOTAL PROJECT COST $\quad \$ \quad 106,672,915 \quad \$ \quad 134,927,094$

If Project has been programmed enter Programmed Amount


Estimated Project Schedule

| PID Approval | October-18 |
| ---: | :---: |
| PA/ED Approval | December-20 |
| PS\&E | December-22 |
| $R T L$ | May-23 |
| Begin Construction | July-23 |


| Cost Estimate Certifier | ar H. Kotchion | 6/17/2022 | (714) 730-2493 |
| :---: | :---: | :---: | :---: |
| Approved by Program Manager | Girair Kotchian, PE - Consultant PM | Date | Phone |
|  |  | 6/17/2022 | (949) 464-6688 |
|  | Tom Perez, City Program M mager | Date | Phone |

## I. ROADWAY ITEMS SUMMARY

| Section |  | Cost |  |
| :---: | :---: | :---: | :---: |
| 1 | Earthwork | \$ | 653,300 |
| 2 | Pavement Structural Section | \$ | 3,955,100 |
| 3 | Drainage | \$ | 2,104,600 |
| 4 | Specialty Items | \$ | 54,500 |
| 5 | Environmental | \$ | 1,530,600 |
| 6 | Traffic Items | \$ | 4,509,800 |
| 7 | Detours | \$ | - |
| 8 | Minor Items | \$ | 1,921,200 |
| 9 | Roadway Mobilization | \$ | 1,473,000 |
| 10 | Supplemental Work | \$ | 828,200 |
| 11 | State Furnished | \$ | 1,329,200 |
| 12 | Time-Related Overhead | \$ | 1,473,000 |
| 13 | Roadway Contingency | \$ | 8,924,700 |

## TOTAL ROADWAY ITEMS $\$ 28,757,200$

Estimate Prepared By :
Seepler N.G. Wancf. 6/17/2022 (714)833-2743

Estimate Reviewed By :

| Qirar ff. Notchicer |
| :--- |
| 6/17/2022 |

By signing this estimate you are attesting that you have discussed your project with all functional units and have incorporated all their comments or have discussed with them why they will not be incorporated.

| Item code |  | Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190101 | Roadway Excavation | CY | 10,305 | X | 60.00 | = | \$ | 618,300 |
| 19010X | Roadway Excavation (Type X) ADL | CY |  | X |  | = | \$ | - |
| 194001 | Ditch Excavation | CY |  | x |  | = | \$ |  |
| 19801X | Imported Borrow | CY/TON |  | X |  | $=$ | \$ |  |
| 192037 | Structure Excavation (Retaining Wall) | CY |  | X |  | $=$ | \$ |  |
| 193013 | Structure Backfill (Retaining Wall) | CY |  | X |  | = | \$ |  |
| 193031 | Pervious Backfill Material (Retaining Wall) | CY |  | X |  | $=$ | \$ | - |
| 16010X | Clearing \& Grubbing | LS | 1 | x | 20,000.00 | = | \$ | 20,000 |
| 170101 | Develop Water Supply | LS | 1 | X | 15,000.00 | $=$ | \$ | 15,000 |
| 19801X | Imported Borrow | CY/TON |  | X |  | = | \$ |  |
| 210130 | Duff | ACRE |  | x |  | = | \$ | - |
| XXXXXX | Some Item | Unit |  |  |  |  |  |  |

## SECTION 2: PAVEMENT STRUCTURAL SECTION

| Item code |  | Unit | Quantity |  | Unit Price |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 401050 | Jointed Plain Concrete Pavement | CY | 157 | X | 900.00 | $=$ | \$ | 141,300 |
| 400050 | Continuously Reinforced Concrete Pavement | CY |  | X |  | = | \$ |  |
| 404092 | Seal Pavement Joint | LF |  | X |  | = | \$ |  |
| 404093 | Seal Isolation Joint | LF |  | x |  | = | \$ | - |
| 413117 | Seal Concrete Pavement Joint (Silicone) | LF |  | X |  | = | \$ |  |
| 413118 | Seal Pavement Joint (Asphalt Rubber) | LF |  | X |  | = | \$ |  |
| 280010 | Rapid Strength Concrete Base | CY |  | X |  | = | \$ |  |
| 410095 | Dowel Bar (Drill and Bond) | EA |  | X |  | = | \$ | - |
| 390132 | Hot Mix Asphalt (Type A) | TON | 6,390 | x | 160.00 | = | \$ | 1,022,400 |
| 390137 | Rubberized Hot Mix Asphalt (Gap Graded) | TON | 3,725 | X | 135.00 | = | \$ | 502,875 |
| 39300X | Geosynthetic Pavement Interlayer (Type X) | SQYD |  | X |  | = | \$ | - |
| 26020X | Class 2 Aggregate Base | CY | 2,385 | X | 85.00 | = | \$ | 202,725 |
| 390401 | HMA - Open Graded (Open Graded Friction Course) | TON | 1,165 | x | 160.00 | = | \$ | 186,400 |
| 290201 | Asphalt Treated Permeable Base | CY | 2,381 | x | 170.00 | = | \$ | 404,770 |
| 250401 | Class 4 Aggregate Subbase | CY | 2,976 | X | 95.00 | = | \$ | 282,720 |
| 374002 | Asphaltic Emulsion (Fog Seal Coat) | TON |  | X |  | = | \$ |  |
| 397005 | Tack Coat | TON |  | x |  | = | \$ |  |
| 377501 | Slurry Seal | TON |  | x |  | = | \$ |  |
| 3750XX | Screenings (Type XX) | TON |  | X |  | = | \$ |  |
| 374492 | Asphaltic Emulsion (Polymer Modified) | TON |  | X |  | = | \$ |  |
| 370001 | Sand Cover (Seal) | TON |  | x |  | = | \$ | - |
| 731504 | Minor Concrete (Curb and Gutter) | CY | 1,485 | X | 440.00 | = | \$ | 653,400 |
| 731521 | Minor Concrete (Sidewalk) | CY | 784 | x | 600.00 | = | \$ | 470,400 |
| 39407X | Place Hot Mix Asphalt Dike (Type X) | LF |  | X |  | = | \$ |  |
| 150771 | Remove Asphalt Concrete Dike | LF |  | X |  | = | \$ |  |
| 420201 | Grind Existing Concrete Pavement | SQYD |  | X |  | = | \$ |  |
| 150860 | Remove Base and Surfacing | CY |  | X |  | = | \$ |  |
| 390095 | Replace Asphalt Concrete Surfacing | CY |  | x |  | = | \$ |  |
| 15312X | Remove Concrete | LF/CY/LS |  | X |  | = | \$ |  |
| 394090 | Place Hot Mix Asphalt (Miscellaneous Area) | SQYD |  | X |  | = | \$ | - |
| 153103 | Cold Plane Asphalt Concrete Pavement | SQYD | 4,401 | X | 20.00 | = | \$ | 88,020 |
| 39405X | Shoulder Rumble Strip (HMA, X-In Indentations) | STA |  | X |  | = | \$ |  |
| 413113 | Repair Spalled Joints, Polyester Grout | SQYD |  | X |  | = | \$ |  |
| 420102 | Groove Existing Concrete Pavement | SQYD |  | X |  | = | \$ |  |
| 390136 | Minor Hot Mix Asphalt | TON |  | X |  | = | \$ |  |
| 394095 | Roadside Paving (Miscellaneous Areas) | SQYD |  | x |  | = | \$ |  |
| XXXXXX | Open Grade Finishing Course (OGFC) | CY |  | x |  | = | \$ | - |

SECTION 3: DRAINAGE

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15080X | Remove Culvert | EA/LF |  | x |  | $=$ | \$ | - |
| 150820 | Modify Inlet | EA |  | X |  | = | \$ | - |
| 155232 | Sand Backfill | CY |  | X |  | = | \$ | - |
| 15020X | Abandon Culvert | EA/LF |  | X |  | $=$ | \$ | - |
| 152430 | Adjust Inlet | LF |  | X |  | = | \$ | - |
| 155003 | Cap Inlet | EA |  | x |  | = | \$ | - |
| 510501 | Minor Concrete | CY |  | x |  | $=$ | \$ | - |
| 510502 | Minor Concrete (Minor Structure) | CY | 62 | x | 2,000.00 | $=$ | \$ | 124,000 |
| 5105XX | Minor Concrete (Type XX) | CY |  | X |  | = | \$ | - |
| 620XXX | XX" Alternative Pipe Culvert (Type X) | LF |  | X |  | $=$ | \$ | - |
| 6411XX | XX" Plastic Pipe | LF |  | x |  | = | \$ | - |
| 65XXXX | 24" Reinforced Concrete Pipe (Type X) | LF | 2,023 | X | 200.00 | = | \$ | 404,600 |
| 6650XX | 36" Reinforced Concrete Pipe (Type X) | LF | 1,200 | x | 260.00 | = | \$ | 312,000 |
| 68XXXX | XX" Plastic Pipe (Edge Drain) | LF |  | x |  | = | \$ | - |
| 69011X | XX" Corrugated Steel Pipe Downdrain (0.XXX" Thic | LF |  | x |  | $=$ | \$ | - |
| 70321X | XX" Corrugated Steel Pipe Inlet (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 70XXXX | XX" Corrugated Steel Pipe Riser (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 7050XX | XX" Steel Flared End Section | EA |  | X |  | $=$ | \$ | - |
| 703233 | Grated Line Drain | LF |  | X |  | $=$ | \$ | - |
| 72XXXX | Rock Slope Protection (Type and Method) | CY/TON |  | X |  | = | \$ | - |
| 72901X | Rock Slope Protection Fabric (Class X) | SQYD |  | X |  | = | \$ | - |
| 721420 | Concrete (Ditch Lining) | CY |  | X |  | = | \$ | - |
| 721430 | Concrete (Channel Lining) | CY |  | X |  | = | \$ | - |
| 750001 | Miscellaneous Iron and Steel | LB |  | x |  | = | \$ | - |
| 750029 | Inlet Frame and Grate | EA | 15 | x | 927.00 | $=$ | \$ | 13,905 |
| 7500xx | Other Drainage Items (7\% of Roadway) | LS | 1 | x | 1,250,000.00 | $=$ | \$ | 1,250,000 |

TOTAL DRAINAGE ITEMS
\$
2,104,600
SECTION 4: SPECIALTY ITEMS

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 080050 | Progress Schedule (Critical Path Method) | LS | 1 | x | 40,000.00 | = | \$ | 40,000 |
| 582001 | Sound Wall (Masonry Block) | SQFT |  | x |  | = | \$ | - |
| 510530 | Minor Concrete (Wall) | CY |  | X |  |  | \$ | - |
| 15325X | Remove Sound Wall | LF/LS |  | X |  | = | \$ | - |
| 070030 | Lead Compliance Plan | LS |  | X |  | = | \$ | - |
| 141120 | Treated Wood Waste | LB |  | X |  | = | \$ | - |
| 153221 | Remove Concrete Barrier | LF |  | X |  | = | \$ | - |
| 150661 | Remove Metal Beam Guard Railing | LF | 200 | X | 10.00 | = | \$ | 2,000 |
| 150668 | Remove Flared End Section | EA | 3 | X | 500.00 | = | \$ | 1,500 |
| 8000XX | Chain Link Fence (Type XX) | LF |  | X |  | = | \$ | - |
| 80XXXX | XX" Chain Link Gate (Type CL-6) | EA |  | X |  | = | \$ | - |
| 832005 | Midwest Guardrail System | LF | 200 | x | 40.00 | $=$ | \$ | 8,000 |
| 839301 | Single Thrie Beam Barrier | LF |  | X |  | $=$ | \$ | - |
| 839310 | Double Thrie Beam Barrier | LF |  | X |  | $=$ | \$ | - |
| 839521 | Cable Railing | LF |  | X |  |  | \$ | - |
| 839539 | Terminal System (Type SKT) | EA | 3 | X | 1,000.00 | = | \$ | 3,000 |
| 839585 | Alternative Flared Terminal System | EA |  | X |  | $=$ | \$ | - |
| 839584 | Alternative In-line Terminal System | EA |  | X |  | $=$ | \$ | - |
| 4906XX | CIDH Concrete Piling (Insert Diameter) | LF |  | x |  | $=$ | \$ | - |
| 839XXX | Crash Cushion (Insert Type) | EA |  | X |  | $=$ | \$ | - |
| 839701 | Bike Trail Barrier (Type TBD) | LF |  | X |  | = | \$ |  |
| 520103 | Bar Reinforced Steel (Retaining Wall) | LB |  | x |  | $=$ | \$ | - |
| 510060 | Structural Concrete, Retaining Wall | CY |  | X |  | = | \$ | - |
| 513553 | Retaining Wall (Masonry Wall) | SQFT | 1,500 | X |  | $=$ | \$ | - |
| 511035 | Architectural Treatment | SQFT |  | X |  | $=$ | \$ | - |
| 598001 | Anti-Graffiti Coating | SQFT |  | X |  | $=$ | \$ | - |
| 203070 | Rock Stain | SQFT |  | X |  | $=$ | \$ | - |
| 5136XX | Reinforced Concrete Crib Wall (Type X) | SQFT |  | X |  | $=$ | \$ | - |
| 83954X | Transition Railing (Type X) | EA |  | x |  | $=$ | \$ | - |
| 597601 | Prepare and Stain Concrete | SQFT |  | x |  | $=$ | \$ | - |
| 839561 | Rail Tensioning Assembly | EA |  | X |  | = | \$ | - |
| 83958X | Some Item | EA |  | X |  | $=$ | \$ | - |
| 839701 | Some Item | Unit |  | X |  | $=$ | \$ | - |

## SECTION 5: ENVIRONMENTAL



[^1]| 6A - Traffic Electrical |  |
| :--- | :---: |
| Item code | Unit |
| 860460 | Lighting and Sign Illumination |
| 860201 | Signal and Lighting |
| 860990 | Closed Circuit Television System |
| 86110X | Ramp Metering System (Location X) |
| 86070X | Interconnection Conduit and Cable |
| 5602XX | Furnish Sign Structure (Type X) |
| 5602XX | Install Sign Structure (Type X) |
| 498040 | XX" CIDHC Pile (Sign Foundation) |
| 860806 | Inductive Loop Detectors |
| 8609XX | Traffic Monitoring Station (Type X) |
| 15075X | Remove Sign Structure |
| 151581 | Reconstruct Sign Structure |
| 152641 | Modify Sign Structure |
| 860090 | Maintain Existing Traffic Management System EleI |
| 86XXXX | Fiber Optic Conduit System |
| XXXXX | Some Item |

6B - Traffic Signing and Striping

| Item code |  |
| :--- | :--- |
| 566011 | Roadside Sign - One Post |
| 566012 | Roadside Sign - Two Post |
| 5602 XX | Furnish Sign |
| 568016 | Install Sign Panel on Existing Frame |
| 150711 | Remove Painted Traffic Stripe |
| 141101 | Remove Yellow Painted Stripe (Haz Waste) |
| 150712 | Remove Painted Pavement Marking |
| 150742 | Remove Roadside Sign |
| 152320 | Reset Roadside Sign |
| 152390 | Relocate Roadside Sign |
| 82010X | Delineator (Class X) |
| 840502 | Thermo Stripe (Enhanced Wet Night Visibility) |
| 846012 | Thermo Crosswalk \& Pav. Marking |
| 120090 | Construction Area Signs |
| 84XXXX | Permanent Pavement Delineation |


| Unit | Quantity |  |
| :---: | :---: | :---: |
| EA | 50 | $x$ |
| EA | 10 | $x$ |
| SQFT |  | $x$ |
| SQFT |  | $x$ |
| LF | 51,744 | $x$ |
| LF |  | $x$ |
| SQFT |  | $x$ |
| EA | 60 | $x$ |
| EA |  | $x$ |
| EA |  | $x$ |
| EA |  | $x$ |
| LF | 51,744 | $x$ |
| SQFT |  | $x$ |
| LS | 1 | $x$ |
| LF | 38,808 | $x$ |

## 6C - Traffic Management Plan

| Unit Price (\$) |  | Cost |  |
| :---: | :---: | :---: | :---: |
| 500.00 | $=$ | \$ | 25,000 |
| 600.00 | = | \$ | 6,000 |
|  | = | \$ | - |
|  | = | \$ | - |
| 1.00 | = | \$ | 51,744 |
|  | = | \$ | - |
|  | = | \$ | - |
| 150.00 | = | \$ | 9,000 |
|  | = | \$ | - |
|  | = | \$ | - |
|  | = | \$ | - |
| 0.55 | $=$ | \$ | 28,459 |
|  | $=$ | \$ | - |
| 5,000.00 | $=$ | \$ | 5,000 |
| 0.55 | $=$ | \$ | 21,344 |

$$
\text { Subtotal Traffic Signing and Striping } \$
$$

| Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | x | 2,000,000.00 | $=$ | \$ | 2,000,000 |
| 2 | x | 400,000.00 | = | \$ | 800,000 |
|  | X |  | = | \$ | - |
|  | X |  | $=$ | \$ | - |
|  | X |  | = | \$ | - |
|  | x |  | = | \$ | - |
|  | X |  | $=$ | \$ | - |
|  | x |  | = | \$ | - |
|  | X |  | $=$ | \$ | - |
|  | X |  | = | \$ | - |
|  | X |  | = | \$ | - |
|  | x |  | = | \$ | - |
|  | x |  | = | \$ | - |
|  | x |  | = | \$ | - |
|  | X |  | $=$ | \$ | - |
|  | X |  | $=$ | \$ | - |

$$
\text { Subtotal Traffic Electrical } \$ \quad 2,800,000
$$

| Subtotal Traffic Electrical | $\$ 2,800,000$ |
| :---: | :---: | :---: |

Item code
12865X Portable Changeable Message Signs

| Quantity |  |  | Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | $\times$ | \$ | 10,000 | = | \$ | 100,000 |

Subtotal Traffic Management Plan $\$ 100,000$
6C - Stage Construction and Traffic Handling

| Item code |  |
| :---: | :--- |
| 120199 | Traffic Plastic Drum |
| $12016 X$ | Channelizer (Type X) |
| 120120 | Type III Barricade |
| 129100 | Temporary Crash Cushion Module |
| 120100 | Traffic Control System |
| 129110 | Temporary Crash Cushion |
| 129000 | Temporary Railing (Type K) |
| 120149 | Temporary Pavement Marking (Paint) |
| 120151 | Temporary Pavement Striping (Paint) |
| 82010X | Delineator (Class X) |
| XXXXXX | Temporary Ground Mounted Signs |
| XXXXXX | Other Street Improvements |


| Unit | Quantity |  | Unit Price (\$) |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EA |  | x |  | $=\$$ | - |
| EA |  | x |  | = \$ | - |
| EA |  | x |  | = \$ | - |
| EA | 420 | x | 250.00 | \$ | 105,000 |
| LS | 1 | x | 40,000.00 | = \$ | 40,000 |
| EA |  | x |  | = \$ | - |
| LF | 38,808 | x | 17.00 | = \$ | 659,736 |
| SQFT |  | x |  | = \$ | - |
| LF | 155,232 | x | 2.00 | = \$ | 310,464 |
| EA |  | x |  | = \$ | - |
| LS | 1 | x | 48,000.00 | = \$ | 48,000 |
| LS | 1 | x | 300,000.00 | = \$ | 300,000 |

[^2]SECTION 7: DETOURS
Includes constructing, maintaining, and removal

| Item code | Unit |  |
| :---: | :--- | :---: |
| 190101 | Roadway Excavation | CY |
| 19801X | Imported Borrow | CY/TON |
| 390132 | Hot Mix Asphalt (Type A) | TON |
| $26020 X$ | Class 2 Aggregate Base | TON/CY |
| 250401 | Class 4 Aggregate Subbase | CY |
| 130620 | Temporary Drainage Inlet Protection | EA |
| 129000 | Temporary Railing (Type K) | LF |
| 128601 | Temporary Signal System | LS |
| 120149 | Temporary Pavement Marking (Paint) | SQFT |
| 80010X | Temporary Fence (Type X) | LF |
| XXXXXX Some Item | Unit |  |



## SECTION 8: MINOR ITEMS

| 8A - Americans with Disabilities Act Items |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ADA Items |  |  | 5.0\% | \$ | 640,395 |
| 8B - Bike Path Items |  |  |  |  |  |
| Bike Path Items |  |  | 0.0\% | \$ | - |
| 8C - Other Minor Items |  |  |  |  |  |
| Other Minor Items |  |  | 10.0\% | \$ | 1,280,790 |
| Total of Section 1-7 | \$ | 12,807,900 | 15.0\% | \$ | 1,921,185 |

## SECTIONS 9: MOBILIZATION

## Item code

999990 Total Section 1-8
$\$ 14,729,100$
10\%
$=\$$
$1,472,910$

TOTAL MOBILIZATION \$
1,473,000

## SECTION 10: SUPPLEMENTAL WORK

| Item code |  | U |
| :---: | :--- | :---: |
| 066670 | Payment Adjustments For Price Index | L |
| 066094 | Vluctuations | L |
| 066070 | Maintain Traffic | L |
| 066919 | Dispute Resolution Board | L |
| 066921 | Dispute Resolution Advisor | L |
| 066015 | Federal Trainee Program | L |
| 066610 | Partnering | L |
| 066204 | Remove Rock and Debris | L |
| 066222 | Locate Existing Crossover | UXXX |

Uni
LS
LS
LS
LS
LS
LS
LS
LS
LS
Unit

Quantity Unit Price (\$)

## Quantity

(

1 x $=\$$
$=$
$=$
$x \quad=$
$x \quad=$

| $x$ | $=$ |
| :--- | :--- |
| $x$ | $=$ |

$x=\$$ $=\$$
$1 \begin{array}{llrr} & x & = & - \\ x \quad 200,000.00 & = & \$ & 200,000\end{array}$

Cost
$\$$
$\$$
\$
$\$$
$\$$
$\$$ -
\$ -
Cost of NPDES Supplemental Work specified in Section 5D $=\underline{\$}$

## PROJECT COST ESTIMATE

SECTION 11: STATE FURNISHED MATERIALS AND EXPENSES

| Item code |  | Unit |  | Quantity |  | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 066105 | Resident Engineers Office | LS |  | 1 | X | 200,000.00 | = |  | \$200,000 |  |
| 066063 | Traffic Management Plan - Public Information | LS |  | 1 | X | 120,000.00 | = |  | \$120,000 |  |
| 066901 | Water Expenses | LS |  |  | X |  | = |  | \$0 |  |
| 8609XX | Traffic Monitoring Station (X) | LS |  |  | X |  | = |  | \$0 |  |
| 066841 | Traffic Controller Assembly | LS |  |  | X |  | = |  | \$0 |  |
| 066840 | Traffic Signal Controller Assembly | LS |  |  | x |  | = |  | \$0 |  |
| 066062 | COZEEP Contract | LS |  | 1 | X | 170,000.00 | = |  | \$170,000 |  |
| 066838 | Reflective Numbers and Edge Sealer | LS |  |  | X |  | = |  | \$0 |  |
| 066065 | Tow Truck Service Patrol | LS |  | 1 | X | 250,000.00 | = |  | \$250,000 |  |
| 066916 | Annual Construction General Permit Fee | LS |  |  | X |  | = |  | \$0 |  |
| XXXXXX | Some Item | Unit |  |  | X |  | = |  | \$0 |  |
|  | Total Section 1-8 |  | \$ | 14,729,100 |  | 4\% | $=$ | \$ | 589,164 |  |
|  |  |  |  |  | TOTAL STATE FURNISHED |  |  |  |  | \$1,329,200 |

## SECTION 12: TIME-RELATED OVERHEAD

| Total of Roadway and Structures Contract Items excluding Mobilization | $\$ 14,729,100$ |
| ---: | :--- |
| Total Construction Cost (excluding TRO and Contingency) | $\$ 18,359,500$ |
|  |  |
| (used to calculate TRO) |  |
| Estimated Time-Related Overhead (TRO) Percentage $(0 \%$ to $10 \%)$ | $=$ |


| Item code |  | Unit | Quantity |  | Unit Price (\$) |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 070018 | Time-Related Overhead | WD | 650 | X | \$2,266 | = | \$1,473,000 |

ote: If the building portion of the project is greater than $50 \%$ of the total project cost, then TRO is not included.

## SECTION 13: ROADWAY CONTINGENCY

Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)
Total Section 1-12 $\$ \quad 19,832,500 \quad x \quad 45 \% \quad=\quad \$ 8,924,625$

## II. STRUCTURE ITEMS

Bridge 1

| DATE OF ESTIMATE | 00/00/00 | 00/00/00 | 00/00/00 |
| :---: | :---: | :---: | :---: |
| Bridge Name | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Bridge Number | 57-XXX | 57-XXX | 57-XXX |
| Structure Type | Pedestrian OC | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Width (Feet) [out to out] | 0 LF | 0 LF | 0 LF |
| Total Bridge Length (Feet) | 0 LF | 0 LF | 0 LF |
| Total Area (Square Feet) | 0 SQFT | 0 SQFT | 0 SQFT |
| Structure Depth (Feet) | 0 LF | 0 LF | 0 LF |
| Footing Type (pile or spread) | TBD | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Cost Per Square Foot | \$1,750 | \$0 | \$0 |
| COST OF EACH | \$0 | \$0 | \$0 |

DATE OF ESTIMATE<br>Name<br>Bridge Number<br>Structure Type<br>Width (Feet) [out to out] Total Length (Feet)<br>Total Area (Square Feet)<br>Structure Depth (Feet)<br>Footing Type (pile or spread)<br>Cost Per Square Foot

00/00/00 xxxxxxxxxxxxxxxxxxx 57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF xxxxxxxxxxxxxxxxxxx $\$ 100$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx
$\$ 0$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx $\$ 0$

| COST OF EACH | \$0 |  | $\$ 0$ |  | $\$ 0$ |
| :---: | :---: | :---: | :---: | :---: | :---: |



Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

Structures Contingency Percentage $10 \% \quad$| \$0 |
| :--- |

## TOTAL COST OF STRUCTURES

Estimate Prepared By:

## III. RIGHT OF WAY

Fill in all of the available information from the Right of Way data sheet.

L)

TOTAL RIGHT OF WAY ESTIMATE
$\$ 60,818,840$
M)

TOTAL R/W ESTIMATE: Escalated
\$74,198,985
N)

RIGHT OF WAY SUPPORT
\$2,721,875


[^3]${ }^{1}$ When estimate has Support Costs only

[^4]
## IV. SUPPORT COST ESTIMATE SUMMARY

| Note: Use PRSM project data. |  | Escalated Support Cost for Estimate To Completion (ETC) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total by FY |  | PA\&ED | PS\&E | RW | CON | Total \$ |
| <2014 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2015 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2016 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2017 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2018 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2019 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2020 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2021 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2022 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2023 | Expended | \$2,000,000 |  |  |  | \$2,000,000 |
|  | ETC |  |  |  |  | \$2,000,000 |
| 2024 | Expended | \$2,375,000 |  |  |  |  |
|  | ETC |  |  |  |  | \$2,375,000 |
| 2025 | Expended |  | \$2,500,000 | \$907,291 |  | \$3,407,291 |
|  | ETC |  |  |  |  | \$3,407,291 |
| 2026 | Expended |  | \$2,500,000 | \$1,814,584 |  |  |
|  | ETC |  |  |  |  | \$4,314,584 |
| 2027 | Expended |  |  |  | \$5,000,000 | \$5,000,000 |
|  | ETC |  |  |  |  |  |
| 2028 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2029> | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| EAC (Expended + ETC) |  | \$4,375,000 | \$5,000,000 | \$2,721,875 | \$5,000,000 | \$17,096,875 |
| Approved Budget (PRSM) |  |  |  |  |  |  |
| Difference (Budget - EAC) |  | -\$4,375,000 | -\$5,000,000 | -\$2,721,875 | -\$5,000,000 | -\$17,096,875 |
| Support Ratio (EAC / Cap Cost) |  | 3.9\% | 4.4\% | 2.4\% | 4.4\% | 15.1\% |


| Total Capital Cost: | $\$ 113,556,000$ |
| :---: | :---: |
| Total Capital Outlay Support Cost: | $\$ 17,096,875$ |
| Overall Percent Support Cost: | $15.06 \%$ |

Type of Estimate : PSR/PDS
Project Limits: Canyon Acres Drive to El Toro Road
Project Description: SR-133 (Laguna Canyon Road) Improvements
Scope : Underground utilities, construct bike lane, construct ped path/sidewalks \& improve shoulders
Alternative: 3
SUMMARY OF PROJECT COST ESTIMATE

| TOTAL ROADWAY COST | Current Year Cost |  | Escalated Cost |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \$ | 27,842,400 | \$ | 38,104,247 |
| TOTAL STRUCTURES COST | \$ | - | \$ | - |
| SUBTOTAL CONSTRUCTION COST | \$ | 27,842,400 | \$ | 38,104,247 |
| TOTAL RIGHT OF WAY COST | \$ | 61,252,589 | \$ | 74,728,159 |
| TOTAL CAPITAL OUTLAY COSTS | \$ | 89,094,989 | \$ | 112,832,406 |
| PR/ED SUPPORT | \$ | 4,375,000 | \$ | 5,468,750 |
| PS\&E SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| RIGHT OF WAY SUPPORT | \$ | 2,860,625 | \$ | 3,575,781 |
| CONSTRUCTION SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| TOTAL SUPPORT COST | \$ | 17,235,625 | \$ | 21,544,531 |


| TOTAL PROJECT COST | $\$ 106,330,614$ | $\$$ | $134,376,937$ |
| :---: | :---: | :---: | :---: | :---: |

If Project has been programmed enter Programmed Amount

|  | Month | Year |
| :---: | :---: | :---: |
| Date of Estimate (Month/Year) | 6 | 2022 |
| Estimated Construction Start (Month/Year) | 6 | 2028 |
|  | Number of Working Days $=$ | 650 |
| Estimated Mid-Point of Construction (Month/Year) | 9 | 2029 |
| Estimated Construction End (Month/Year) | 9 | 2030 |
| Number of Plant Establishment Days 261 |  |  |

Estimated Project Schedule

| PID Approval | October-18 |
| ---: | :---: |
| PA/ED Approval | December-20 |
| PS\&E | December-22 |
| $R T L$ | May-23 |
| Begin Construction | July-23 |


| Cost Estimate Certifier | an | 6/17/2022 | (714) 730-2493 |
| :---: | :---: | :---: | :---: |
| Approved by Program Manager | Girair Kotchian, PE - Consultant PM | Date | Phone |
|  |  | 6/17/2022 | (949) 464-6688 |
|  | Tom Perez, City Program M mager | Date | Phone |

## I. ROADWAY ITEMS SUMMARY

Section
Cost

| 1 | Earthwork | \$ | 542,300 |
| :---: | :---: | :---: | :---: |
| 2 | Pavement Structural Section | \$ | 3,636,600 |
| 3 | Drainage | \$ | 2,105,500 |
| 4 | Specialty Items | \$ | 54,500 |
| 5 | Environmental | \$ | 1,530,600 |
| 6 | Traffic Items | \$ | 4,509,800 |
| 7 | Detours | \$ | - |
| 8 | Minor Items | \$ | 1,856,900 |
| 9 | Roadway Mobilization | \$ | 1,423,700 |
| 10 | Supplemental Work | \$ | 808,500 |
| 11 | State Furnished | \$ | 1,309,500 |
| 12 | Time-Related Overhead | \$ | 1,423,700 |
| 13 | Roadway Contingency | \$ | 8,640,800 |

## TOTAL ROADWAY ITEMS $\quad \$ \quad 27,842,400$

Estimate Prepared By :
Seepler N.G. Wanef. 6/17/2022 (714)833-2743

Estimate Reviewed By :

| Qirar ff. Notchicer |
| :--- |
| 6/17/2022 |

By signing this estimate you are attesting that you have discussed your project with all functional units and have incorporated all their comments or have discussed with them why they will not be incorporated.

SECTION 1: EARTHWORK

| Item code |  | Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190101 | Roadway Excavation | CY | 12,682 | X | 40.00 | = | \$ | 507,280 |
| 19010X | Roadway Excavation (Type X) ADL | CY |  | X |  | = | \$ | - |
| 194001 | Ditch Excavation | CY |  | x |  | = | \$ |  |
| 19801X | Imported Borrow | CY/TON |  | X |  | = | \$ |  |
| 192037 | Structure Excavation (Retaining Wall) | CY |  | X |  | $=$ | \$ |  |
| 193013 | Structure Backfill (Retaining Wall) | CY |  | X |  | = | \$ |  |
| 193031 | Pervious Backfill Material (Retaining Wall) | CY |  | X |  | $=$ | \$ | - |
| 16010X | Clearing \& Grubbing | LS | 1 | x | 20,000.00 | = | \$ | 20,000 |
| 170101 | Develop Water Supply | LS | 1 | X | 15,000.00 | $=$ | \$ | 15,000 |
| 19801X | Imported Borrow | CY/TON |  | X |  | = | \$ |  |
| 210130 | Duff | ACRE |  | x |  | = | \$ | - |
| XXXXXX | Some Item | Unit |  |  |  |  |  |  |

## SECTION 2: PAVEMENT STRUCTURAL SECTION

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 401050 | Jointed Plain Concrete Pavement | CY | 153 | x |  | $=$ | \$ |  |
| 400050 | Continuously Reinforced Concrete Pavement | CY |  | X |  | = | \$ |  |
| 404092 | Seal Pavement Joint | LF |  | X |  | = | \$ |  |
| 404093 | Seal Isolation Joint | LF |  | x |  | = | \$ |  |
| 413117 | Seal Concrete Pavement Joint (Silicone) | LF |  | x |  | = | \$ | - |
| 413118 | Seal Pavement Joint (Asphalt Rubber) | LF |  | X |  | = | \$ |  |
| 280010 | Rapid Strength Concrete Base | CY |  | X |  | = | \$ |  |
| 410095 | Dowel Bar (Drill and Bond) | EA |  | X |  | = | \$ | - |
| 390132 | Hot Mix Asphalt (Type A) | TON | 7,032 | x | 160.00 | = | \$ | 1,125,120 |
| 390137 | Rubberized Hot Mix Asphalt (Gap Graded) | TON | 3,686 | x | 135.00 | = | \$ | 497,610 |
| 39300X | Geosynthetic Pavement Interlayer (Type X) | SQYD |  | X |  | = | \$ | - |
| 26020X | Class 2 Aggregate Base | CY | 2,468 | x | 85.00 | = | \$ | 209,780 |
| 390401 | HMA - Open Graded (Open Graded Friction Course) | TON | 1,063 | x | 160.00 | $=$ | \$ | 170,080 |
| 290201 | Asphalt Treated Permeable Base | CY | 2,100 | x | 170.00 | = | \$ | 357,000 |
| 250401 | Class 4 Aggregate Subbase | CY | 2,625 | X | 95.00 | $=$ | \$ | 249,375 |
| 374002 | Asphaltic Emulsion (Fog Seal Coat) | TON |  | X |  | = | \$ |  |
| 397005 | Tack Coat | TON |  | x |  | $=$ | \$ |  |
| 377501 | Slurry Seal | TON |  | X |  | = | \$ |  |
| 3750XX | Screenings (Type XX) | TON |  | x |  | $=$ | \$ |  |
| 374492 | Asphaltic Emulsion (Polymer Modified) | TON |  | X |  | = | \$ |  |
| 370001 | Sand Cover (Seal) | TON |  | X |  | = | \$ | - |
| 731504 | Minor Concrete (Curb and Gutter) | CY | 662 | x | 440.00 | $=$ | \$ | 291,280 |
| 731521 | Minor Concrete (Sidewalk) | CY | 1,182 | X | 600.00 | = | \$ | 709,200 |
| 39407X | Place Hot Mix Asphalt Dike (Type X) | LF |  | X |  | = | \$ |  |
| 150771 | Remove Asphalt Concrete Dike | LF |  | X |  | = | \$ |  |
| 420201 | Grind Existing Concrete Pavement | SQYD |  | X |  | $=$ | \$ |  |
| 150860 | Remove Base and Surfacing | CY |  | x |  | $=$ | \$ | - |
| 390095 | Replace Asphalt Concrete Surfacing | CY |  | x |  | $=$ | \$ |  |
| 15312X | Remove Concrete | LF/CY/LS |  | X |  | $=$ | \$ |  |
| 394090 | Place Hot Mix Asphalt (Miscellaneous Area) | SQYD |  | X |  | $=$ | \$ | - |
| 153103 | Cold Plane Asphalt Concrete Pavement | SQYD | 1,357 | x | 20.00 | = | \$ | 27,140 |
| 39405X | Shoulder Rumble Strip (HMA, X-In Indentations) | STA |  | x |  | $=$ | \$ | - |
| 413113 | Repair Spalled Joints, Polyester Grout | SQYD |  | x |  | $=$ | \$ |  |
| 420102 | Groove Existing Concrete Pavement | SQYD |  | X |  | $=$ | \$ |  |
| 390136 | Minor Hot Mix Asphalt | TON |  | X |  |  | \$ | - |
| 394095 | Roadside Paving (Miscellaneous Areas) | SQYD |  | X |  |  | \$ | - |
| XXXXXX | Open Grade Finishing Course (OGFC) | CY |  | x |  |  | \$ | - |

TOTAL PAVEMENT STRUCTURAL SECTION ITEMS \$

SECTION 3: DRAINAGE

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15080X | Remove Culvert | EA/LF |  | x |  | $=$ | \$ | - |
| 150820 | Modify Inlet | EA |  | X |  | = | \$ | - |
| 155232 | Sand Backfill | CY |  | X |  | = | \$ | - |
| 15020X | Abandon Culvert | EA/LF |  | X |  | $=$ | \$ | - |
| 152430 | Adjust Inlet | LF |  | X |  | = | \$ | - |
| 155003 | Cap Inlet | EA |  | x |  | = | \$ | - |
| 510501 | Minor Concrete | CY |  | x |  | $=$ | \$ | - |
| 510502 | Minor Concrete (Minor Structure) | CY | 62 | x | 2,000.00 | $=$ | \$ | 124,000 |
| 5105XX | Minor Concrete (Type XX) | CY |  | X |  | = | \$ | - |
| 620XXX | XX" Alternative Pipe Culvert (Type X) | LF |  | X |  | $=$ | \$ | - |
| 6411XX | XX" Plastic Pipe | LF |  | X |  | = | \$ | - |
| 65XXXX | 24" Reinforced Concrete Pipe (Type X) | LF | 2,023 | X | 200.00 | = | \$ | 404,600 |
| 6650XX | 36" Reinforced Concrete Pipe (Type X) | LF | 1,200 | x | 260.00 | = | \$ | 312,000 |
| 68XXXX | XX" Plastic Pipe (Edge Drain) | LF |  | x |  | = | \$ | - |
| 69011X | XX" Corrugated Steel Pipe Downdrain (0.XXX" Thic | LF |  | x |  | $=$ | \$ | - |
| 70321X | XX" Corrugated Steel Pipe Inlet (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 70XXXX | XX" Corrugated Steel Pipe Riser (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 7050XX | XX" Steel Flared End Section | EA |  | X |  | $=$ | \$ | - |
| 703233 | Grated Line Drain | LF |  | X |  | $=$ | \$ | - |
| 72XXXX | Rock Slope Protection (Type and Method) | CY/TON |  | X |  | = | \$ | - |
| 72901X | Rock Slope Protection Fabric (Class X) | SQYD |  | X |  | = | \$ | - |
| 721420 | Concrete (Ditch Lining) | CY |  | X |  | = | \$ | - |
| 721430 | Concrete (Channel Lining) | CY |  | X |  | = | \$ | - |
| 750001 | Miscellaneous Iron and Steel | LB |  | x |  | = | \$ | - |
| 750029 | Inlet Frame and Grate | EA | 16 | x | 927.00 | $=$ | \$ | 14,832 |
| 7500xx | Other Drainage Items (7\% of Roadway) | LS | 1 | x | 1,250,000.00 | $=$ | \$ | 1,250,000 |

TOTAL DRAINAGE ITEMS

## SECTION 4: SPECIALTY ITEMS

| Item code |  |
| ---: | :--- |
| 080050 | Progress Schedule (Critical Path Method) |
| 582001 | Sound Wall (Masonry Block) |
| 510530 | Minor Concrete (Wall) |
| $15325 X$ | Remove Sound Wall |
| 070030 | Lead Compliance Plan |
| 141120 | Treated Wood Waste |
| 153221 | Remove Concrete Barrier |
| 150661 | Remove Metal Beam Guard Railing |
| 150668 | Remove Flared End Section |
| 8000 XX | Chain Link Fence (Type XX) |
| 80 XXXX | XX" Chain Link Gate (Type CL-6) |
| 832005 | Midwest Guardrail System |
| 839301 | Single Thrie Beam Barrier |
| 839310 | Double Thrie Beam Barrier |
| 839521 | Cable Railing |
| 839539 | Terminal System (Type SKT) |
| 839585 | Alternative Flared Terminal System |
| 839584 | Alternative In-line Terminal System |
| 4906 XX | CIDH Concrete Piling (Insert Diameter) |
| $839 X X X$ | Crash Cushion (Insert Type) |
| 839701 | Bike Trail Mountable Curb (Type E-6) |
| 520103 | Bar Reinforced Steel (Retaining Wall) |
| 510060 | Structural Concrete, Retaining Wall |
| 513553 | Retaining Wall (Masonry Wall) |
| 511035 | Architectural Treatment |
| 598001 | Anti-Graffiti Coating |
| 203070 | Rock Stain |
| 5136 XX | Reinforced Concrete Crib Wall (Type X) |
| $83954 X$ | Transition Railing (Type X) |
| 597601 | Prepare and Stain Concrete |
| 839561 | Rail Tensioning Assembly |
| $83958 X$ | Some Item |
| 839701 | Some Item |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | X | 40,000.00 | $=$ | \$ | 40,000 |
| SQFT |  | X |  | = | \$ | - |
| CY |  | X |  | = | \$ | - |
| LF/LS |  | X |  | $=$ | \$ | - |
| LS |  | X |  | = | \$ | - |
| LB |  | X |  | = | \$ | - |
| LF |  | X |  | = | \$ | - |
| LF | 200 | x | 10.00 | = | \$ | 2,000 |
| EA | 3 | x | 500.00 | = | \$ | 1,500 |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF | 200 | X | 40.00 | = | \$ | 8,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA | 3 | x | 1,000.00 | = | \$ | 3,000 |
| EA |  | X |  | = | \$ | - |
| EA |  | X |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| CY |  | x |  | = | \$ | - |
| LB |  | x |  | = | \$ | - |
| CY |  | X |  | = | \$ | - |
| SQFT | 1,500 | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| SQFT |  | X |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| Unit |  | x |  | = | \$ | - |

## SECTION 5: ENVIRONMENTAL

5A - ENVIRONMENTAL MITIGATION

| Item code |  |
| :--- | :--- |
| 14XXXX | Biological Mitigation |
| 14XXXX | Archaeological Commitments |
| 14XXXX | Historical Commitments |
| 130670 | Temporary Reinforced Silt Fence |
| 141000 | Temporary Fence (Type ESA) |
| 14XXXX | Other Environmental Mitigation |
|  |  |
| 5B - LANDSCAPE AND IRRIGATION |  |
| Item code |  |
| 20XXXX | Highway Planting |
| 20XXXX | Irrigation System |
| 204099 | Plant Establishment Work |
| 204101 | Extend Plant Establishment Work |
| 20XXXX | Follow-up Landscape Project |
| 150685 | Remove Irrigation Facility |
| 20XXXX | Maintain Existing (Irrigation or Planted Areas) |
| 206400 | Check and Test Existing Irrigation Facilities |
| 21011X | Imported Topsoil (X) |
| 20XXXX | Rock Blanket, Rock Mulch, DG, Gravel Mulch |
| 200122 | Weed Germination |
| 208304 | Water Meter |
| 2087XX | XX" Conduit (Use for Irrigation x-overs) |
| 20890X | Extend X" Conduit |

## 5C - EROSION CONTROL

| Item code |  |
| :--- | :--- |
| 210010 | Move In/Move Out (Erosion Control) |
| 210350 | Fiber Rolls |
| 210360 | Compost Sock |
| 2102 XX | Rolled Erosion Control Product (X) |
| $21025 X$ | Bonded Fiber Matrix |
| 210300 | Hydromulch |
| 210420 | Straw |
| 210430 | Hydroseed |
| 210600 | Compost |
| 210630 | Incorporate Materials |
| 2106 XX | Other Erosion Control |
|  |  |
| 5D - NPDES |  |
| Item code |  |
| 130300 | Prepare SWPPP |
| 130200 | Prepare WPCP |
| 130100 | Job Site Management |
| 130330 | Storm Water Annual Report |
| 130310 | Rain Event Action Plan (REAP) |
| 130320 | Storm Water Sampling and Analysis Day |
| 130520 | Temporary Hydraulic Mulch |
| 130550 | Temporary Hydroseed |
| 130505 | Move-In/Move-Out (Temp Erosion Control) |
| 130640 | Temporary Fiber Roll |
| 130900 | Temporary Concrete Washout |
| 130710 | Temporary Construction Entrance |
| 130610 | Temporary Check Dam |
| 130620 | Temporary Drainage Inlet Protection |
| 130730 | Street Sweeping |
| XXXXXX | Permenant BMPs |


| Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 20,000.00 | $=$ | \$ | 20,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | $=$ | \$ | - |
| LS | 1 | x | 250,000.00 | $=$ | \$ | 250,000 |


| Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |
| LS | 1 | x | 100,000.00 | $=$ | \$ | 100,000 |
| LS | 1 | x | 50,000.00 | $=$ | \$ | 50,000 |
| LS |  | x |  | = | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| CY/TON |  | x |  | = | \$ | - |
| SF/SY |  | x |  | $=$ | \$ | - |
| SQYD |  | x |  | $=$ | \$ | - |
| EA |  | x |  | $=$ | \$ | - |
| LF |  | x |  | $=$ | \$ | - |
| LF |  | x |  | $=$ | \$ | - |


| Unit | Quantity |
| :---: | :---: |
| EA |  |
| LF |  |
| LF |  |
| SQFT |  |
| FT/ACRE |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| LS | 1 |


Unit
LS

## 6A - Traffic Electrical

| Item code | Unit |  |
| ---: | :--- | ---: |
| 860460 | Lighting and Sign Illumination | LS |
| 860201 | Signal and Lighting | EA |
| 860990 | Closed Circuit Television System | LS |
| 86110X | Ramp Metering System (Location X) | LS |
| 86070X | Interconnection Conduit and Cable | LS |
| $5602 X X$ | Furnish Sign Structure (Type X) | LB |
| $5602 X X$ | Install Sign Structure (Type X) | LF |
| 498040 | XX" CIDHC Pile (Sign Foundation) | LS |
| 860806 | Inductive Loop Detectors | LS |
| 8609XX | Traffic Monitoring Station (Type X) | EA/LS |
| $15075 X$ | Remove Sign Structure | EA |
| 151581 | Reconstruct Sign Structure | EA |
| 152641 | Modify Sign Structure | LS |
| 860090 | Maintain Existing Traffic Mgt.System | LS |
| 86XXXX | Fiber Optic Conduit System | LS |

6B - Traffic Signing and Striping

| Item code |  |
| :--- | :--- |
| 566011 | Roadside Sign - One Post |
| 566012 | Roadside Sign - Two Post |
| 5602 XX | Furnish Sign |
| 568016 | Install Sign Panel on Existing Frame |
| 150711 | Remove Painted Traffic Stripe |
| 141101 | Remove Yellow Stripe (Hazardous Waste) |
| 150712 | Remove Painted Pavement Marking |
| 150742 | Remove Roadside Sign |
| 152320 | Reset Roadside Sign |
| 152390 | Relocate Roadside Sign |
| 82010X | Delineator (Class X) |
| 840502 | Thermo Traffic Stripe |
| 846012 | Thermo Crosswalk and Pavement Marking |
| 120090 | Construction Area Signs |
| 84XXXX | Permanent Pavement Delineation |


| Unit | Quantity |  |
| :---: | :---: | :---: |
| EA | 50 | x |
| EA | 10 | x |
| SQFT |  | x |
| SQFT |  | x |
| LF | 51,744 | x |
| LF |  | x |
| SQFT |  | x |
| EA | 60 | x |
| EA |  | x |
| EA |  | x |
| EA |  | x |
| LF | 51,744 | x |
| SQFT |  | x |
| LS | 1 | x |
| LF | 38,808 | x |


| Unit Price (\$) | Cost |  |  |
| :---: | :---: | :---: | :---: |
| 500.00 | $=$ | \$ | 25,000 |
| 600.00 | $=$ | \$ | 6,000 |
|  | $=$ | \$ |  |
|  | $=$ | \$ |  |
| 1.00 | $=$ | \$ | 51,744 |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 150.00 | $=$ | \$ | 9,000 |
|  | = | \$ |  |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 0.55 | $=$ | \$ | 28,459 |
|  | $=$ | \$ |  |
| 5,000.00 | $=$ | \$ | 5,000 |
| 0.55 | $=$ | \$ | 21,344 |

$$
\text { Subtotal Traffic Signing and Striping } \$
$$

## 6C - Traffic Management Plan

Item code
12865X Portable Changeable Message Signs

| Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EA |  | x |  | $=$ | \$ |  |
| EA |  | X |  | = | \$ |  |
| EA |  | x |  | = | \$ | - |
| EA | 420 | x | 250.00 | = | \$ | 105,000 |
| LS | 1 | x | 40,000.00 | = | \$ | 40,000 |
| EA |  | x |  | = | \$ | - |
| LF | 38,808 | X | 17.00 | = | \$ | 659,736 |
| SQFT |  | x |  | = | \$ | - |
| LF | 155,232 | x | 2.00 | $=$ | \$ | 310,464 |
| EA |  | x |  | $=$ | \$ | - |
| LS | 1 | x | 48,000.00 | = | \$ | 48,000 |
| Unit | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |

6C - Stage Construction and Traffic Handling

| Item code |  |
| :--- | :--- |
| 120199 | Traffic Plastic Drum |
| $12016 X$ | Channelizer (Type X) |
| 120120 | Type III Barricade |
| 129100 | Temporary Crash Cushion Module |
| 120100 | Traffic Control System |
| 129110 | Temporary Crash Cushion |
| 129000 | Temporary Railing (Type K) |
| 120149 | Temporary Pavement Marking (Paint) |
| 120151 | Temporary Pavement Striping (Paint) |
| 82010X | Delineator (Class X) |
| XXXXXX Temporary Ground Mounted Signs |  |
| XXXXXX | Other Street Improvements |

[^5]SECTION 7: DETOURS
Includes constructing, maintaining, and removal

| Item code | Unit |  |
| :---: | :--- | :---: |
| 190101 | Roadway Excavation | CY |
| 19801X | Imported Borrow | CY/TON |
| 390132 | Hot Mix Asphalt (Type A) | TON |
| $26020 X$ | Class 2 Aggregate Base | TON/CY |
| 250401 | Class 4 Aggregate Subbase | CY |
| 130620 | Temporary Drainage Inlet Protection | EA |
| 129000 | Temporary Railing (Type K) | LF |
| 128601 | Temporary Signal System | LS |
| 120149 | Temporary Pavement Marking (Paint) | SQFT |
| 80010X | Temporary Fence (Type X) | LF |
| XXXXXX Some Item | Unit |  |


| Quantity |  | Unit Price (\$) |  | Cost |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | x | $=$ | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  |  | TOTAL DE | TOURS |  | \$ |  | - |
|  |  | UBTOTAL SECTIO | ONS 1 th | through 7 |  |  | 12,379,300 |

## SECTION 8: MINOR ITEMS

| 8A - Americans with Disabilities Act Items |  |  |  |
| :--- | :--- | :--- | :--- |
| ADA Items <br> 8B - Bike Path Items <br> Bike Path Items <br> 8C - Other Minor Items <br> Other Minor Items |  | $5.0 \%$ | $\$$ |

## SECTIONS 9: MOBILIZATION

## Item code

999990 Total Section 1-8
\$ 14,236,200
10\%
$=\$$
1,423,620
TOTAL MOBILIZATION \$

## SECTION 10: SUPPLEMENTAL WORK

| Item code |  | U |
| :---: | :--- | :---: |
| 066670 | Payment Adjustments For Price Index | L |
| 066094 | Value Analysis | L |
| 066070 | Maintain Traffic | L |
| 066919 | Dispute Resolution Board | L |
| 066921 | Dispute Resolution Advisor | L |
| 066015 | Federal Trainee Program | L |
| 066610 | Partnering | L |
| 066204 | Remove Rock and Debris | L |
| 066222 | Locate Existing Crossover | U |

Uni
LS
LS
LS
LS
LS
LS
LS
LS
LS
Unit

Quantity Unit Price (\$)

## - $x$

(

Cost
$=\$$
$=\$$
$=\$ \quad 200,000$
$=\$$
$=\$$ -
$=\$$
$=\$$
$=\$$
$=\$$
$=\$$
Cost of NPDES Supplemental Work specified in Section 5D $=\underline{\$}$

## PROJECT COST ESTIMATE

SECTION 11: STATE FURNISHED MATERIALS AND EXPENSES


## SECTION 12: TIME-RELATED OVERHEAD

| Total of Roadway and Structures Contract Items excluding Mobilization | \$14,236,200 (used to calculate TRO) |
| :---: | :---: |
| Total Construction Cost (excluding TRO and Contingency) | \$17,777,900 (used to check if project is greater than \$5 million excluding contingency) |
| Estimated Time-Related Overhead (TRO) Perc | \% to $10 \%)=10 \%$ |


| Item code |  | Unit | Quantity |  | Unit Price (\$) |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 070018 | Time-Related Overhead | WD | 650 | X | \$2,190 | = | \$1,423,700 |

## TOTAL TIME-RELATED OVERHEAD

Note: If the building portion of the project is greater than $50 \%$ of the total project cost, then TRO is not included.

## SECTION 13: ROADWAY CONTINGENCY

Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

## II. STRUCTURE ITEMS

Bridge 1

| DATE OF ESTIMATE | 00/00/00 | 00/00/00 | 00/00/00 |
| :---: | :---: | :---: | :---: |
| Bridge Name | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Bridge Number | 57-XXX | 57-XXX | 57-XXX |
| Structure Type | Pedestrian OC | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Width (Feet) [out to out] | 0 LF | 0 LF | 0 LF |
| Total Bridge Length (Feet) | 0 LF | 0 LF | 0 LF |
| Total Area (Square Feet) | 0 SQFT | 0 SQFT | 0 SQFT |
| Structure Depth (Feet) | 0 LF | 0 LF | 0 LF |
| Footing Type (pile or spread) | TBD | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Cost Per Square Foot | \$1,750 | \$0 | \$0 |
| COST OF EACH | \$0 | \$0 | \$0 |

DATE OF ESTIMATE<br>Name<br>Bridge Number<br>Structure Type<br>Width (Feet) [out to out] Total Length (Feet)<br>Total Area (Square Feet)<br>Structure Depth (Feet)<br>Footing Type (pile or spread)<br>Cost Per Square Foot

00/00/00 xxxxxxxxxxxxxxxxxxx 57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF xxxxxxxxxxxxxxxxxxx $\$ 100$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx
$\$ 0$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx $\$ 0$

| COST OF EACH | \$0 |  | $\$ 0$ |  | $\$ 0$ |
| :---: | :---: | :---: | :---: | :---: | :---: |



Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

Structures Contingency Percentage $10 \% \quad$| \$0 |
| :--- |

## TOTAL COST OF STRUCTURES

Estimate Prepared By:

## III. RIGHT OF WAY

Fill in all of the available information from the Right of Way data sheet.

L)

TOTAL RIGHT OF WAY ESTIMATE
\$61,252,589
M)

TOTAL R/W ESTIMATE: Escalated
N)

RIGHT OF WAY SUPPORT
\$2,860,625


[^6]
## IV. SUPPORT COST ESTIMATE SUMMARY

| Note: Use PRSM project data. |  | Escalated Support Cost for Estimate To Completion (ETC) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total by FY |  | PA\&ED | PS\&E | RW | CON | Total \$ |
| <2014 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2015 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2016 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2017 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2018 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2019 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2020 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2021 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2022 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2023 | Expended | \$2,000,000 |  |  |  | \$2,000,000 |
|  | ETC |  |  |  |  |  |
| 2024 | Expended | \$2,375,000 |  |  |  | \$2,375,000 |
|  | ETC |  |  |  |  |  |
| 2025 | Expended |  | \$2,500,000 | \$953,542 |  | \$3,453,542 |
|  | ETC |  |  |  |  |  |
| 2026 | Expended |  | \$2,500,000 | \$1,907,083 |  | \$4,407,083 |
|  | ETC |  |  |  |  |  |
| 2027 | Expended |  |  |  | \$5,000,000 | \$5,000,000 |
|  | ETC |  |  |  |  |  |
| 2028 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2029> | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| EAC (Expended + ETC) |  | \$4,375,000 | \$5,000,000 | \$2,860,625 | \$5,000,000 | \$17,235,625 |
| Approved Budget (PRSM) |  |  |  |  |  |  |
| Difference (Budget - EAC) |  | -\$4,375,000 | -\$5,000,000 | -\$2,860,625 | -\$5,000,000 | -\$17,235,625 |
| Support Ratio (EAC / Cap Cost) |  | 3.9\% | 4.4\% | 2.5\% | 4.4\% | 15.3\% |


| Total Capital Cost: | $\$ 112,832,406$ |
| :---: | :---: |
| Total Capital Outlay Support Cost: | $\$ 17,235,625$ |
| Overall Percent Support Cost: | $15.28 \%$ |

Type of Estimate : PSR/PDS
Project Limits: Canyon Acres Drive to El Toro Road
Project Description: SR-133 (Laguna Canyon Road) Improvements
Scope: Underground utilities, construct bike lane, construct ped path/sidewalks \& improve shoulders
Alternative: 4
SUMMARY OF PROJECT COST ESTIMATE

|  | Current Year Cost |  | Escalated Cost |  |
| :---: | :---: | :---: | :---: | :---: |
| TOTAL ROADWAY COST | \$ | 28,993,100 | \$ | 39,679,059 |
| TOTAL STRUCTURES COST | \$ | - | \$ | - |
| SUBTOTAL CONSTRUCTION COST | \$ | 28,993,100 | \$ | 39,679,059 |
| TOTAL RIGHT OF WAY COST | \$ | 61,378,791 | \$ | 74,882,125 |
| TOTAL CAPITAL OUTLAY COSTS | \$ | 90,079,000 | \$ | 114,561,184 |
| PR/ED SUPPORT | \$ | 4,375,000 | \$ | 5,468,750 |
| PS\&E SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| RIGHT OF WAY SUPPORT | \$ | 3,178,750 | \$ | 3,973,438 |
| CONSTRUCTION SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| TOTAL SUPPORT COST | \$ | 17,553,750 | \$ | 21,942,188 |

Date of Estimate (Month/Year) $\quad \frac{\text { Month }}{6}$ / $\frac{\text { Year }}{2022}$

Estimated Construction Start (Month/Year) $\quad 6 / 2028$
Number of Working Days $=650$
Estimated Mid-Point of Construction (Month/Year) $\quad 9$ / 2029
Estimated Construction End (Month/Year) 9 / 2030
Number of Plant Establishment Days 261

Estimated Project Schedule

| PID Approval | October-18 |
| ---: | :---: |
| PA/ED Approval | December-20 |
| PS\&E | December-22 |
| $R T L$ | May-23 |
| Begin Construction | July-23 |


| Cost Estimate Certifier | ar th. Kotcman | 6/17/2022 | (714) 730-2493 |
| :---: | :---: | :---: | :---: |
|  | Girair Kotchian, PE - Consultant PM | Date | Phone |
| Approved by Program Manager |  | 6/17/2022 | (949) 464-6688 |
|  | Tom Perez, City Program Manajer | Date | Phone |

## I. ROADWAY ITEMS SUMMARY

| Section |  | Cost |  |
| :---: | :---: | :---: | :---: |
| 1 | Earthwork | \$ | 336,500 |
| 2 | Pavement Structural Section | \$ | 4,381,500 |
| 3 | Drainage | \$ | 2,105,500 |
| 4 | Specialty Items | \$ | 54,500 |
| 5 | Environmental | \$ | 1,530,600 |
| 6 | Traffic Items | \$ | 4,509,800 |
| 7 | Detours | \$ | - |
| 8 | Minor Items | \$ | 1,937,800 |
| 9 | Roadway Mobilization | \$ | 1,485,700 |
| 10 | Supplemental Work | \$ | 833,300 |
| 11 | State Furnished | \$ | 1,334,300 |
| 12 | Time-Related Overhead | \$ | 1,485,700 |
| 13 | Roadway Contingency | \$ | 8,997,900 |

## TOTAL ROADWAY ITEMS $\$ 28,993,100$

Estimate Prepared By :
Seepler N.G. Wancf. 6/17/2022 (714)833-2743

Estimate Reviewed By :

| Qirar ff. Notchicer |
| :--- |
| 6/17/2022 |

By signing this estimate you are attesting that you have discussed your project with all functional units and have incorporated all their comments or have discussed with them why they will not be incorporated.

SECTION 1: EARTHWORK

| Item code |  | Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190101 | Roadway Excavation | CY | 7,536 | X | 40.00 | = | \$ | 301,440 |
| 19010X | Roadway Excavation (Type X) ADL | CY |  | X |  | = | \$ | - |
| 194001 | Ditch Excavation | CY |  | x |  | = | \$ |  |
| 19801X | Imported Borrow | CY/TON |  | X |  | = | \$ |  |
| 192037 | Structure Excavation (Retaining Wall) | CY |  | X |  | $=$ | \$ |  |
| 193013 | Structure Backfill (Retaining Wall) | CY |  | X |  | = | \$ |  |
| 193031 | Pervious Backfill Material (Retaining Wall) | CY |  | X |  | = | \$ | - |
| 16010X | Clearing \& Grubbing | LS | 1 | x | 20,000.00 | $=$ | \$ | 20,000 |
| 170101 | Develop Water Supply | LS | 1 | x | 15,000.00 | $=$ | \$ | 15,000 |
| 19801X | Imported Borrow | CY/TON |  | X |  | = | \$ |  |
| 210130 | Duff | ACRE |  | x |  | $=$ | \$ |  |
| XXXXXX | Some Item | Unit |  |  |  |  |  |  |

## SECTION 2: PAVEMENT STRUCTURAL SECTION

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 401050 | Jointed Plain Concrete Pavement | CY | 134 | x |  | $=$ | \$ |  |
| 400050 | Continuously Reinforced Concrete Pavement | CY |  | X |  | = | \$ |  |
| 404092 | Seal Pavement Joint | LF |  | X |  | = | \$ |  |
| 404093 | Seal Isolation Joint | LF |  | x |  | = | \$ |  |
| 413117 | Seal Concrete Pavement Joint (Silicone) | LF |  | x |  | = | \$ | - |
| 413118 | Seal Pavement Joint (Asphalt Rubber) | LF |  | X |  | = | \$ |  |
| 280010 | Rapid Strength Concrete Base | CY |  | X |  | = | \$ |  |
| 410095 | Dowel Bar (Drill and Bond) | EA |  | X |  | = | \$ | - |
| 390132 | Hot Mix Asphalt (Type A) | TON | 11,064 | x | 160.00 | = | \$ | 1,770,240 |
| 390137 | Rubberized Hot Mix Asphalt (Gap Graded) | TON | 4,538 | x | 135.00 | = | \$ | 612,630 |
| 39300X | Geosynthetic Pavement Interlayer (Type X) | SQYD |  | X |  | = | \$ | - |
| 26020X | Class 2 Aggregate Base | CY | 3,946 | x | 85.00 | = | \$ | 335,410 |
| 390401 | HMA - Open Graded (Open Graded Friction Course) | TON |  | X |  | $=$ | \$ | - |
| 290201 | Asphalt Treated Permeable Base | CY |  | x |  | = | \$ | - |
| 250401 | Class 4 Aggregate Subbase | CY |  | X |  | $=$ | \$ |  |
| 374002 | Asphaltic Emulsion (Fog Seal Coat) | TON |  | X |  | = | \$ |  |
| 397005 | Tack Coat | TON |  | x |  | $=$ | \$ |  |
| 377501 | Slurry Seal | TON |  | X |  | = | \$ |  |
| 3750XX | Screenings (Type XX) | TON |  | x |  | $=$ | \$ |  |
| 374492 | Asphaltic Emulsion (Polymer Modified) | TON |  | X |  | $=$ | \$ |  |
| 370001 | Sand Cover (Seal) | TON |  | X |  | = | \$ | - |
| 731504 | Minor Concrete (Curb and Gutter) | CY | 1,483 | x | 440.00 | $=$ | \$ | 652,520 |
| 731521 | Minor Concrete (Sidewalk) | CY | 1,528 | X | 600.00 | = | \$ | 916,800 |
| 39407X | Place Hot Mix Asphalt Dike (Type X) | LF |  | X |  | = | \$ |  |
| 150771 | Remove Asphalt Concrete Dike | LF |  | X |  | = | \$ |  |
| 420201 | Grind Existing Concrete Pavement | SQYD |  | X |  | $=$ | \$ | - |
| 150860 | Remove Base and Surfacing | CY |  | x |  | $=$ | \$ | - |
| 390095 | Replace Asphalt Concrete Surfacing | CY |  | x |  | $=$ | \$ | - |
| 15312X | Remove Concrete | LF/CY/LS |  | X |  | $=$ | \$ |  |
| 394090 | Place Hot Mix Asphalt (Miscellaneous Area) | SQYD |  | X |  | $=$ | \$ | - |
| 153103 | Cold Plane Asphalt Concrete Pavement | SQYD | 4,694 | x | 20.00 | = | \$ | 93,880 |
| 39405X | Shoulder Rumble Strip (HMA, X-In Indentations) | STA |  | x |  | $=$ | \$ | - |
| 413113 | Repair Spalled Joints, Polyester Grout | SQYD |  | x |  | $=$ | \$ |  |
| 420102 | Groove Existing Concrete Pavement | SQYD |  | X |  | $=$ | \$ |  |
| 390136 | Minor Hot Mix Asphalt | TON |  | X |  |  | \$ | - |
| 394095 | Roadside Paving (Miscellaneous Areas) | SQYD |  | X |  |  | \$ | - |
| XXXXXX | Open Grade Finishing Course (OGFC) | CY |  | x |  |  | \$ | - |

TOTAL PAVEMENT STRUCTURAL SECTION ITEMS \$

SECTION 3: DRAINAGE

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15080X | Remove Culvert | EA/LF |  | x |  | $=$ | \$ | - |
| 150820 | Modify Inlet | EA |  | X |  | = | \$ | - |
| 155232 | Sand Backfill | CY |  | X |  | = | \$ | - |
| 15020X | Abandon Culvert | EA/LF |  | X |  | $=$ | \$ | - |
| 152430 | Adjust Inlet | LF |  | X |  | = | \$ | - |
| 155003 | Cap Inlet | EA |  | x |  | = | \$ | - |
| 510501 | Minor Concrete | CY |  | x |  | $=$ | \$ | - |
| 510502 | Minor Concrete (Minor Structure) | CY | 62 | x | 2,000.00 | $=$ | \$ | 124,000 |
| 5105XX | Minor Concrete (Type XX) | CY |  | X |  | = | \$ | - |
| 620XXX | XX" Alternative Pipe Culvert (Type X) | LF |  | X |  | $=$ | \$ | - |
| 6411XX | XX" Plastic Pipe | LF |  | X |  | = | \$ | - |
| 65XXXX | 24" Reinforced Concrete Pipe (Type X) | LF | 2,023 | X | 200.00 | = | \$ | 404,600 |
| 6650XX | 36" Reinforced Concrete Pipe (Type X) | LF | 1,200 | x | 260.00 | = | \$ | 312,000 |
| 68XXXX | XX" Plastic Pipe (Edge Drain) | LF |  | x |  | = | \$ | - |
| 69011X | XX" Corrugated Steel Pipe Downdrain (0.XXX" Thic | LF |  | x |  | $=$ | \$ | - |
| 70321X | XX" Corrugated Steel Pipe Inlet (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 70XXXX | XX" Corrugated Steel Pipe Riser (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 7050XX | XX" Steel Flared End Section | EA |  | X |  | $=$ | \$ | - |
| 703233 | Grated Line Drain | LF |  | X |  | $=$ | \$ | - |
| 72XXXX | Rock Slope Protection (Type and Method) | CY/TON |  | X |  | = | \$ | - |
| 72901X | Rock Slope Protection Fabric (Class X) | SQYD |  | X |  | = | \$ | - |
| 721420 | Concrete (Ditch Lining) | CY |  | X |  | = | \$ | - |
| 721430 | Concrete (Channel Lining) | CY |  | X |  | = | \$ | - |
| 750001 | Miscellaneous Iron and Steel | LB |  | x |  | = | \$ | - |
| 750029 | Inlet Frame and Grate | EA | 16 | x | 927.00 | $=$ | \$ | 14,832 |
| 7500xx | Other Drainage Items (7\% of Roadway) | LS | 1 | x | 1,250,000.00 | $=$ | \$ | 1,250,000 |

TOTAL DRAINAGE ITEMS

## SECTION 4: SPECIALTY ITEMS

| Item code |  |
| ---: | :--- |
| 080050 | Progress Schedule (Critical Path Method) |
| 582001 | Sound Wall (Masonry Block) |
| 510530 | Minor Concrete (Wall) |
| $15325 X$ | Remove Sound Wall |
| 070030 | Lead Compliance Plan |
| 141120 | Treated Wood Waste |
| 153221 | Remove Concrete Barrier |
| 150661 | Remove Metal Beam Guard Railing |
| 150668 | Remove Flared End Section |
| 8000 XX | Chain Link Fence (Type XX) |
| 80 XXXX | XX" Chain Link Gate (Type CL-6) |
| 832005 | Midwest Guardrail System |
| 839301 | Single Thrie Beam Barrier |
| 839310 | Double Thrie Beam Barrier |
| 839521 | Cable Railing |
| 839539 | Terminal System (Type SKT) |
| 839585 | Alternative Flared Terminal System |
| 839584 | Alternative In-line Terminal System |
| 4906 XX | CIDH Concrete Piling (Insert Diameter) |
| $839 X X X$ | Crash Cushion (Insert Type) |
| 839701 | Bike Trail Barrier (Type TBD) |
| 520103 | Bar Reinforced Steel (Retaining Wall) |
| 510060 | Structural Concrete, Retaining Wall |
| 513553 | Retaining Wall (Masonry Wall) |
| 511035 | Architectural Treatment |
| 598001 | Anti-Graffiti Coating |
| 203070 | Rock Stain |
| 5136 XX | Reinforced Concrete Crib Wall (Type X) |
| $83954 X$ | Transition Railing (Type X) |
| 597601 | Prepare and Stain Concrete |
| 839561 | Rail Tensioning Assembly |
| $83958 X$ | Some Item |
| 839701 | Some Item |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | X | 40,000.00 | $=$ | \$ | 40,000 |
| SQFT |  | X |  | = | \$ | - |
| CY |  | X |  | = | \$ | - |
| LF/LS |  | X |  | $=$ | \$ | - |
| LS |  | X |  | = | \$ | - |
| LB |  | X |  | = | \$ | - |
| LF |  | X |  | = | \$ | - |
| LF | 200 | x | 10.00 | = | \$ | 2,000 |
| EA | 3 | x | 500.00 | = | \$ | 1,500 |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF | 200 | x | 40.00 | = | \$ | 8,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA | 3 | x | 1,000.00 | = | \$ | 3,000 |
| EA |  | X |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF |  | x | 150.00 | = | \$ | - |
| LB |  | x |  | = | \$ | - |
| CY |  | x |  | = | \$ | - |
| SQFT | 1,430 | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| Unit |  | x |  | = | \$ | - |

## SECTION 5: ENVIRONMENTAL

5A - ENVIRONMENTAL MITIGATION

| Item code |  |
| :--- | :--- |
| 14XXXX | Biological Mitigation |
| 14XXXX | Archaeological Commitments |
| 14XXXX | Historical Commitments |
| 130670 | Temporary Reinforced Silt Fence |
| 141000 | Temporary Fence (Type ESA) |
| 14XXXX | Other Environmental Mitigation |
|  |  |
| 5B - LANDSCAPE AND IRRIGATION |  |
| Item code |  |
| 20XXXX | Highway Planting |
| 20XXXX | Irrigation System |
| 204099 | Plant Establishment Work |
| 204101 | Extend Plant Establishment Work |
| 20XXXX | Follow-up Landscape Project |
| 150685 | Remove Irrigation Facility |
| 20XXXX | Maintain Existing (Irrigation or Planted Areas) |
| 206400 | Check and Test Existing Irrigation Facilities |
| 21011X | Imported Topsoil (X) |
| 20XXXX | Rock Blanket, Rock Mulch, DG, Gravel Mulch |
| 200122 | Weed Germination |
| 208304 | Water Meter |
| 2087XX | XX" Conduit (Use for Irrigation x-overs) |
| 20890X | Extend X" Conduit (Irrigation X-overs) |

## 5C - EROSION CONTROL

| Item code |  |
| :--- | :--- |
| 210010 | Move In/Move Out (Erosion Control) |
| 210350 | Fiber Rolls |
| 210360 | Compost Sock |
| 2102 XX | Rolled Erosion Control Product (X) |
| $21025 X$ | Bonded Fiber Matrix |
| 210300 | Hydromulch |
| 210420 | Straw |
| 210430 | Hydroseed |
| 210600 | Compost |
| 210630 | Incorporate Materials |
| 2106 XX | Other Erosion Control |
|  |  |
| 5D - NPDES |  |
| Item code |  |
| 130300 | Prepare SWPPP |
| 130200 | Prepare WPCP |
| 130100 | Job Site Management |
| 130330 | Storm Water Annual Report |
| 130310 | Rain Event Action Plan (REAP) |
| 130320 | Storm Water Sampling and Analysis Day |
| 130520 | Temporary Hydraulic Mulch |
| 130550 | Temporary Hydroseed |
| 130505 | Move-In/Move-Out (Temp Erosion Control) |
| 130640 | Temporary Fiber Roll |
| 130900 | Temporary Concrete Washout |
| 130710 | Temporary Construction Entrance |
| 130610 | Temporary Check Dam |
| 130620 | Temporary Drainage Inlet Protection |
| 130730 | Street Sweeping |
| XXXXXX | Permenant BMPs |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 20,000.00 | $=$ | \$ | 20,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LS | 1 | x | 250,000.00 | = | \$ | 250,000 |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |
| LS | 1 | X | 100,000.00 | = | \$ | 100,000 |
| LS | 1 | X | 50,000.00 | = | \$ | 50,000 |
| LS |  | x |  | = | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | = | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | = | \$ | - |
| CY/TON |  | x |  | $=$ | \$ | - |
| SF/SY |  | x |  | = | \$ | - |
| SQYD |  | x |  | $=$ | \$ | - |
| EA |  | x |  | $=$ | \$ | - |
| LF |  | x |  | $=$ | \$ | - |
| LF |  | x |  | = | \$ | - |


| Unit | Quantity |
| :---: | :---: |
| EA |  |
| LF |  |
| LF |  |
| SQFT |  |
| FT/ACRE |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| LS | 1 |


Unit
LS

## 6A - Traffic Electrical

| Item code | Unit |  |
| ---: | :--- | ---: |
| 860460 | Lighting and Sign Illumination | LS |
| 860201 | Signal and Lighting | EA |
| 860990 | Closed Circuit Television System | LS |
| 86110X | Ramp Metering System (Location X) | LS |
| 86070X | Interconnection Conduit and Cable | LS |
| $5602 X X$ | Furnish Sign Structure (Type X) | LB |
| $5602 X X$ | Install Sign Structure (Type X) | LF |
| 498040 | XX" CIDHC Pile (Sign Foundation) | LS |
| 860806 | Inductive Loop Detectors | LS |
| 8609XX | Traffic Monitoring Station (Type X) | EA/LS |
| $15075 X$ | Remove Sign Structure | EA |
| 151581 | Reconstruct Sign Structure | EA |
| 152641 | Modify Sign Structure | LS |
| 860090 | Maintain Existing Traffic Mgt. System | LS |
| 86XXXX | Fiber Optic Conduit System | LS |

6B - Traffic Signing and Striping

| Item code |  |
| :--- | :--- |
| 566011 | Roadside Sign - One Post |
| 566012 | Roadside Sign - Two Post |
| 5602 XX | Furnish Sign |
| 568016 | Install Sign Panel on Existing Frame |
| 150711 | Remove Painted Traffic Stripe |
| 141101 | Remove Yellow Stripe (Hazardous Waste) |
| 150712 | Remove Painted Pavement Marking |
| 150742 | Remove Roadside Sign |
| 152320 | Reset Roadside Sign |
| 152390 | Relocate Roadside Sign |
| 82010X | Delineator (Class X) |
| 840502 | Thermo Traffic Stripe |
| 846012 | Thermo Crosswalk and Pavement Marking |
| 120090 | Construction Area Signs |
| 84XXXX | Permanent Pavement Delineation |


| Unit | Quantity |  |
| :---: | :---: | :---: |
| EA | 50 | x |
| EA | 10 | x |
| SQFT |  | x |
| SQFT |  | x |
| LF | 51,744 | x |
| LF |  | x |
| SQFT |  | x |
| EA | 60 | x |
| EA |  | x |
| EA |  | x |
| EA |  | x |
| LF | 51,744 | x |
| SQFT |  | x |
| LS | 1 | x |
| LF | 38,808 | x |


| Unit Price (\$) | Cost |  |  |
| :---: | :---: | :---: | :---: |
| 500.00 | $=$ | \$ | 25,000 |
| 600.00 | $=$ | \$ | 6,000 |
|  | $=$ | \$ |  |
|  | $=$ | \$ |  |
| 1.00 | $=$ | \$ | 51,744 |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 150.00 | $=$ | \$ | 9,000 |
|  | = | \$ |  |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 0.55 | $=$ | \$ | 28,459 |
|  | $=$ | \$ |  |
| 5,000.00 | $=$ | \$ | 5,000 |
| 0.55 | $=$ | \$ | 21,344 |

$$
\text { Subtotal Traffic Signing and Striping } \$
$$

## 6C - Traffic Management Plan

Item code
12865X Portable Changeable Message Signs

| Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EA |  | x |  | $=$ | \$ | - |
| EA |  | x |  | = | \$ | - |
| EA |  | x |  | $=$ | \$ | - |
| EA | 420 | x | 250.00 | = | \$ | 105,000 |
| LS | 1 | x | 40,000.00 | = | \$ | 40,000 |
| EA |  | x |  | = | \$ | - |
| LF | 38,808 | x | 17.00 | $=$ | \$ | 659,736 |
| SQFT |  | x |  | = | \$ | - |
| LF | 155,232 | X | 2.00 | = | \$ | 310,464 |
| EA |  | x |  | = | \$ | - |
| LS | 1 | x | 48,000.00 | = | \$ | 48,000 |
| Unit | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |

6C - Stage Construction and Traffic Handling

| Item code |  |
| :--- | :--- |
| 120199 | Traffic Plastic Drum |
| $12016 X$ | Channelizer (Type X) |
| 120120 | Type III Barricade |
| 129100 | Temporary Crash Cushion Module |
| 120100 | Traffic Control System |
| 129110 | Temporary Crash Cushion |
| 129000 | Temporary Railing (Type K) |
| 120149 | Temporary Pavement Marking (Paint) |
| 120151 | Temporary Pavement Striping (Paint) |
| 82010X | Delineator (Class X) |
| XXXXXX Temporary Ground Mounted Signs |  |
| XXXXXX | Other Street Improvements |

[^7]SECTION 7: DETOURS
Includes constructing, maintaining, and removal

| Item code | Unit |  |
| :---: | :--- | :---: |
| 190101 | Roadway Excavation | CY |
| 19801X | Imported Borrow | CY/TON |
| 390132 | Hot Mix Asphalt (Type A) | TON |
| $26020 X$ | Class 2 Aggregate Base | TON/CY |
| 250401 | Class 4 Aggregate Subbase | CY |
| 130620 | Temporary Drainage Inlet Protection | EA |
| 129000 | Temporary Railing (Type K) | LF |
| 128601 | Temporary Signal System | LS |
| 120149 | Temporary Pavement Marking (Paint) | SQFT |
| 80010X | Temporary Fence (Type X) | LF |
| XXXXXX Some Item | Unit |  |


| Quantity |  | Unit Price (\$) |  | Cost |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | X | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | X | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  | x | $=$ | \$ | - |  |  |
|  |  | TOTAL DE | TOURS |  | \$ | - |
|  |  | SUBTOTAL SECTIO | ONS 1 th | through 7 | \$ | 12,918,400 |

## SECTION 8: MINOR ITEMS

| 8A - Americans with Disabilities Act Items |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADA Items |  |  |  | 5.0\% |  | \$ | 645,920 |
| 8B - Bike Path Items |  |  |  |  |  |  |  |
| Bike Path Items |  |  |  | 0.0\% |  | \$ | - |
| 8C-Other Minor Items |  |  |  |  |  |  |  |
| Other Minor Items |  |  |  | 10.0\% |  | \$ | 1,291,840 |
| Total of Section 1-7 | \$ | 12,918,400 | X | 15.0\% | $=$ | \$ | 1,937,760 |

## SECTIONS 9: MOBILIZATION

## Item code

999990 Total Section 1-8
$10 \%=\$$
1,485,620
TOTAL MOBILIZATION \$

## SECTION 10: SUPPLEMENTAL WORK

| Item code |  | U |
| :---: | :--- | :---: |
| 066670 | Payment Adjustments For Price Index | L |
| 066094 | Value Analysis | L |
| 066070 | Maintain Traffic | L |
| 066919 | Dispute Resolution Board | L |
| 066921 | Dispute Resolution Advisor | L |
| 066015 | Federal Trainee Program | L |
| 066610 | Partnering | L |
| 066204 | Remove Rock and Debris | L |
| 066222 | Locate Existing Crossover | L |
| XXXXXX | Some Item | U |

Uni
LS
LS
LS
LS
LS
LS
LS
LS
LS
Unit

Quantity Unit Price (\$)

## Quantity

(

Cost
$\square$

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=\$
$$

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\begin{array}{llr}
= & \$ & - \\
= & \$ & 200,000
\end{array}
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Cost of NPDES Supplemental Work specified in Section 5D $=\underline{\$}$
Total Section 1-8 $\$ 14,856,200 \quad 4 \% \quad \$ \quad 594,248$

## PROJECT COST ESTIMATE

SECTION 11: STATE FURNISHED MATERIALS AND EXPENSES

| Item code |  | Unit |  | Quantity |  | Unit Price (\$) |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 066105 | Resident Engineers Office | LS |  | 1 | X | 200,000.00 | = | \$200,000 |  |
| 066063 | Traffic Management Plan - Public Information | LS |  | 1 | X | 120,000.00 | = | \$120,000 |  |
| 066901 | Water Expenses | LS |  |  | X |  | = | \$0 |  |
| 8609XX | Traffic Monitoring Station (X) | LS |  |  | X |  | = | \$0 |  |
| 066841 | Traffic Controller Assembly | LS |  |  | X |  | = | \$0 |  |
| 066840 | Traffic Signal Controller Assembly | LS |  |  | x |  | = | \$0 |  |
| 066062 | COZEEP Contract | LS |  | 1 | X | 170,000.00 | = | \$170,000 |  |
| 066838 | Reflective Numbers and Edge Sealer | LS |  |  | X |  | = | \$0 |  |
| 066065 | Tow Truck Service Patrol | LS |  | 1 | X | 250,000.00 | = | \$250,000 |  |
| 066916 | Annual Construction General Permit Fee | LS |  |  | X |  | = | \$0 |  |
| XXXXXX | Some Item | Unit |  |  | x |  | = | \$0 |  |
|  | Total Section 1-8 |  | \$ | 14,856,200 |  | 4\% | $=\$$ | 594,248 |  |
|  |  |  |  |  | TOTAL STATE FURNISHED |  |  |  | \$1,334,300 |

## SECTION 12: TIME-RELATED OVERHEAD

## Total of Roadway and Structures Contract Items excluding Mobilization <br> Total Construction Cost (excluding TRO and Contingency)

\$14,856,200 (used to calculate TRO)
$\$ 18,509,500$ (used to check if project is greater than $\$ 5$ million excluding contingency)
Estimated Time-Related Overhead (TRO) Percentage (0\% to 10\%) =
10\%

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 070018 | Time-Related Overhead | WD | 650 | X | \$2,286 | = | \$1,485,700 |

## TOTAL TIME-RELATED OVERHEAD

Note: If the building portion of the project is greater than $50 \%$ of the total project cost, then TRO is not included.

## SECTION 13: ROADWAY CONTINGENCY

Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

## II. STRUCTURE ITEMS

Bridge 1

| DATE OF ESTIMATE | 00/00/00 | 00/00/00 | 00/00/00 |
| :---: | :---: | :---: | :---: |
| Bridge Name | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Bridge Number | 57-XXX | 57-XXX | 57-XXX |
| Structure Type | Pedestrian OC | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Width (Feet) [out to out] | 0 LF | 0 LF | 0 LF |
| Total Bridge Length (Feet) | 0 LF | 0 LF | 0 LF |
| Total Area (Square Feet) | 0 SQFT | 0 SQFT | 0 SQFT |
| Structure Depth (Feet) | 0 LF | 0 LF | 0 LF |
| Footing Type (pile or spread) | TBD | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Cost Per Square Foot | \$1,750 | \$0 | \$0 |
| COST OF EACH | \$0 | \$0 | \$0 |

DATE OF ESTIMATE<br>Name<br>Bridge Number<br>Structure Type<br>Width (Feet) [out to out] Total Length (Feet)<br>Total Area (Square Feet)<br>Structure Depth (Feet)<br>Footing Type (pile or spread)<br>Cost Per Square Foot

00/00/00 xxxxxxxxxxxxxxxxxxx 57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF xxxxxxxxxxxxxxxxxxx $\$ 100$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx
$\$ 0$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx $\$ 0$

| COST OF EACH | \$0 |  | $\$ 0$ |  | $\$ 0$ |
| :---: | :---: | :---: | :---: | :---: | :---: |



Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

Structures Contingency Percentage $10 \% \quad$| \$0 |
| :--- |

## TOTAL COST OF STRUCTURES

Estimate Prepared By:

## III. RIGHT OF WAY

Fill in all of the available information from the Right of Way data sheet.

L)

TOTAL RIGHT OF WAY ESTIMATE
\$61,378,791
M)

TOTAL R/W ESTIMATE: Escalated
\$74,882,125
N)

RIGHT OF WAY SUPPORT
\$3,178,750


[^8]
## IV. SUPPORT COST ESTIMATE SUMMARY

| Note: Use PRSM project data. |  | Escalated Support Cost for Estimate To Completion (ETC) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total by FY |  | PA\&ED | PS\&E | RW | CON | Total \$ |
| <2014 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2015 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2016 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2017 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2018 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2019 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2020 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2021 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2022 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2023 | Expended | \$2,000,000 |  |  |  | \$2,000,000 |
|  | ETC |  |  |  |  | \$2,000,000 |
| 2024 | Expended | \$2,375,000 |  |  |  |  |
|  | ETC |  |  |  |  | \$2,375,000 |
| 2025 | Expended |  | \$2,500,000 | \$1,059,583 |  | \$3,559,583 |
|  | ETC |  |  |  |  | \$3,559,583 |
| 2026 | Expended |  | \$2,500,000 | \$2,119,167 |  | \$4,619,167 |
|  | ETC |  |  |  |  | \$4,619,167 |
| 2027 | Expended |  |  |  | \$5,000,000 | \$5,000,000 |
|  | ETC |  |  |  |  |  |
| 2028 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2029> | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| EAC (Expended + ETC) |  | \$4,375,000 | \$5,000,000 | \$3,178,750 | \$5,000,000 | \$17,553,750 |
| Approved Budget (PRSM) |  |  |  |  |  |  |
| Difference (Budget - EAC) |  | -\$4,375,000 | -\$5,000,000 | -\$3,178,750 | -\$5,000,000 | -\$17,553,750 |
| Support Ratio (EAC / Cap Cost) |  | 3.8\% | 4.4\% | 2.8\% | 4.4\% | 15.3\% |


| Total Capital Cost: | $\$ 114,561,184$ |
| :---: | :---: |
| Total Capital Outlay Support Cost: | $\$ 17,553,750$ |
| Overall Percent Support Cost: | $15.32 \%$ |

Type of Estimate : PSR/PDS
Project Limits: Canyon Acres Drive to El Toro Road
Project Description: SR-133 (Laguna Canyon Road) Improvements
Scope: Underground utilities, construct bike lane, construct ped path/sidewalks \& improve shoulders
Alternative : 5

SUMMARY OF PROJECT COST ESTIMATE

| TOTAL ROADWAY COST | Current Year Cost |  | Escalated Cost |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \$ | 29,421,700 | \$ | 40,265,628 |
| TOTAL STRUCTURES COST | \$ | - | \$ | - |
| SUBTOTAL CONSTRUCTION COST | \$ | 29,421,700 | \$ | 40,265,628 |
| TOTAL RIGHT OF WAY COST | \$ | 63,688,677 | \$ | 77,700,186 |
| TOTAL CAPITAL OUTLAY COSTS | \$ | 90,079,000 | \$ | 117,965,814 |
| PR/ED SUPPORT | \$ | 4,375,000 | \$ | 5,468,750 |
| PS\&E SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| RIGHT OF WAY SUPPORT | \$ | 3,846,875 | \$ | 4,808,594 |
| CONSTRUCTION SUPPORT | \$ | 5,000,000 | \$ | 6,250,000 |
| TOTAL SUPPORT COST | \$ | 18,221,875 | \$ | 22,777,344 |


| TOTAL PROJECT COST | $\$ 108,300,875$ | $\$$ | $140,743,158$ |
| :---: | :---: | :---: | :---: | :---: |

If Project has been programmed enter Programmed Amount

| Date of Estimate (Month/Year) | Month | 1 | Year |
| :---: | :---: | :---: | :---: |
|  | 6 | 1 | 2022 |
| Estimated Construction Start (Month/Year) | 6 | 1 | 2028 |
|  | Number of Working Days $=$ |  | 650 |
| Estimated Mid-Point of Construction (Month/Year) | 9 | 1 | 2029 |
| Estimated Construction End (Month/Year) | 9 | 1 | 2030 |
| Number of Plant Establishment Days |  |  | 261 |

Estimated Project Schedule

| PID Approval | October-18 |
| ---: | :---: |
| PA/ED Approval | December-20 |
| PS\&E | December-22 |
| $R T L$ | May-23 |
| Begin Construction | July-23 |


| Cost Estimate Certifier | ar th. Kotchion | 6/17/2022 | (714) 730-2493 |
| :---: | :---: | :---: | :---: |
|  | Girair Kotchian, PE - Consultant PM | Date | Phone |
| Approved by Program Manager |  | 6/17/2022 | (949) 464-6688 |
|  | Tom Perez, City Program Manzger | Date | Phone |

## I. ROADWAY ITEMS SUMMARY

| Section |  | Cost |  |
| :---: | :---: | :---: | :---: |
| 1 | Earthwork | \$ | 354,400 |
| 2 | Pavement Structural Section | \$ | 4,564,500 |
| 3 | Drainage | \$ | 2,105,500 |
| 4 | Specialty Items | \$ | 54,500 |
| 5 | Environmental | \$ | 1,530,600 |
| 6 | Traffic Items | \$ | 4,509,800 |
| 7 | Detours | \$ | - |
| 8 | Minor Items | \$ | 1,967,900 |
| 9 | Roadway Mobilization | \$ | 1,508,800 |
| 10 | Supplemental Work | \$ | 842,500 |
| 11 | State Furnished | \$ | 1,343,500 |
| 12 | Time-Related Overhead | \$ | 1,508,800 |
| 13 | Roadway Contingency | \$ | 9,130,900 |

## TOTAL ROADWAY ITEMS $\$ \mathbf{2 9 , 4 2 1 , 7 0 0}$

Estimate Prepared By :
Seepler N.G. Wanef. 6/17/2022 (714)833-2743

Estimate Reviewed By :

| Qirar ff. Notchicer |
| :--- |
| 6/17/2022 |

By signing this estimate you are attesting that you have discussed your project with all functional units and have incorporated all their comments or have discussed with them why they will not be incorporated.

SECTION 1: EARTHWORK

| Item code |  | Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190101 | Roadway Excavation | CY | 7,983 | X | 40.00 | = | \$ | 319,320 |
| 19010X | Roadway Excavation (Type X) ADL | CY |  | X |  | = | \$ | - |
| 194001 | Ditch Excavation | CY |  | x |  | $=$ | \$ |  |
| 19801X | Imported Borrow | CY/TON |  | X |  | $=$ | \$ |  |
| 192037 | Structure Excavation (Retaining Wall) | CY |  | X |  | $=$ | \$ |  |
| 193013 | Structure Backfill (Retaining Wall) | CY |  | X |  | $=$ | \$ |  |
| 193031 | Pervious Backfill Material (Retaining Wall) | CY |  | X |  | = | \$ | - |
| 16010X | Clearing \& Grubbing | LS | 1 | x | 20,000.00 | = | \$ | 20,000 |
| 170101 | Develop Water Supply | LS | 1 | X | 15,000.00 | $=$ | \$ | 15,000 |
| 19801X | Imported Borrow | CY/TON |  | X |  | $=$ | \$ |  |
| 210130 | Duff | ACRE |  | x |  | $=$ | \$ |  |
| XXXXXX | Some Item | Unit |  |  |  |  |  |  |

## SECTION 2: PAVEMENT STRUCTURAL SECTION

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 401050 | Jointed Plain Concrete Pavement | CY | 153 | X |  | $=$ | \$ |  |
| 400050 | Continuously Reinforced Concrete Pavement | CY |  | x |  | $=$ | \$ | - |
| 404092 | Seal Pavement Joint | LF |  | x |  | = | \$ | - |
| 404093 | Seal Isolation Joint | LF |  | X |  | = | \$ | - |
| 413117 | Seal Concrete Pavement Joint (Silicone) | LF |  | x |  | $=$ | \$ |  |
| 413118 | Seal Pavement Joint (Asphalt Rubber) | LF |  | X |  | $=$ | \$ | - |
| 280010 | Rapid Strength Concrete Base | CY |  | X |  | $=$ | \$ | - |
| 410095 | Dowel Bar (Drill and Bond) | EA |  | x |  | = | \$ | - |
| 390132 | Hot Mix Asphalt (Type A) | TON | 11,719 | x | 160.00 | = | \$ | 1,875,040 |
| 390137 | Rubberized Hot Mix Asphalt (Gap Graded) | TON | 4,801 | x | 135.00 | = | \$ | 648,135 |
| 39300X | Geosynthetic Pavement Interlayer (Type X) | SQYD |  | x |  | $=$ | \$ | - |
| 26020X | Class 2 Aggregate Base | CY | 4,195 | x | 85.00 | = | \$ | 356,575 |
| 390401 | HMA - Open Graded (Open Graded Friction Course) | TON |  | X |  | $=$ | \$ | - |
| 290201 | Asphalt Treated Permeable Base | CY |  | X |  | $=$ | \$ | - |
| 250401 | Class 4 Aggregate Subbase | CY |  | x |  | $=$ | \$ | - |
| 374002 | Asphaltic Emulsion (Fog Seal Coat) | TON |  | x |  | $=$ | \$ | - |
| 397005 | Tack Coat | TON |  | x |  | = | \$ | - |
| 377501 | Slurry Seal | TON |  | X |  | $=$ | \$ | - |
| 3750XX | Screenings (Type XX) | TON |  | X |  |  | \$ | - |
| 374492 | Asphaltic Emulsion (Polymer Modified) | TON |  | x |  | = | \$ | - |
| 370001 | Sand Cover (Seal) | TON |  | x |  | $=$ | \$ | - |
| 731504 | Minor Concrete (Curb and Gutter) | CY | 1,480 | x | 440.00 | = | \$ | 651,200 |
| 731521 | Minor Concrete (Sidewalk) | CY | 1,557 | X | 600.00 | $=$ | \$ | 934,200 |
| 39407X | Place Hot Mix Asphalt Dike (Type X) | LF |  | X |  | $=$ | \$ | - |
| 150771 | Remove Asphalt Concrete Dike | LF |  | x |  | $=$ | \$ | - |
| 420201 | Grind Existing Concrete Pavement | SQYD |  | x |  | $=$ | \$ | - |
| 150860 | Remove Base and Surfacing | CY |  | x |  | $=$ | \$ | - |
| 390095 | Replace Asphalt Concrete Surfacing | CY |  | X |  |  | \$ | - |
| 15312X | Remove Concrete | LF/CY/LS |  | X |  | $=$ | \$ | - |
| 394090 | Place Hot Mix Asphalt (Miscellaneous Area) | SQYD |  | x |  | $=$ | \$ | - |
| 153103 | Cold Plane Asphalt Concrete Pavement | SQYD | 4,963 | x | 20.00 | $=$ | \$ | 99,260 |
| 39405X | Shoulder Rumble Strip (HMA, X-In Indentations) | STA |  | X |  | $=$ | \$ | - |
| 413113 | Repair Spalled Joints, Polyester Grout | SQYD |  | X |  |  | \$ | - |
| 420102 | Groove Existing Concrete Pavement | SQYD |  | x |  |  | \$ | - |
| 390136 | Minor Hot Mix Asphalt | TON |  | x |  |  | \$ | - |
| 394095 | Roadside Paving (Miscellaneous Areas) | SQYD |  | X |  |  | \$ | - |
| XXXXXX | Open Grade Finishing Course (OGFC) | CY |  | X |  |  | \$ | - |

SECTION 3: DRAINAGE

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15080X | Remove Culvert | EA/LF |  | x |  | $=$ | \$ | - |
| 150820 | Modify Inlet | EA |  | X |  | = | \$ | - |
| 155232 | Sand Backfill | CY |  | X |  | = | \$ | - |
| 15020X | Abandon Culvert | EA/LF |  | X |  | $=$ | \$ | - |
| 152430 | Adjust Inlet | LF |  | X |  | = | \$ | - |
| 155003 | Cap Inlet | EA |  | x |  | = | \$ | - |
| 510501 | Minor Concrete | CY |  | x |  | $=$ | \$ | - |
| 510502 | Minor Concrete (Minor Structure) | CY | 62 | x | 2,000.00 | $=$ | \$ | 124,000 |
| 5105XX | Minor Concrete (Type XX) | CY |  | X |  | = | \$ | - |
| 620XXX | XX" Alternative Pipe Culvert (Type X) | LF |  | X |  | $=$ | \$ | - |
| 6411XX | XX" Plastic Pipe | LF |  | X |  | = | \$ | - |
| 65XXXX | 24" Reinforced Concrete Pipe (Type X) | LF | 2,023 | X | 200.00 | = | \$ | 404,600 |
| 6650XX | 36" Reinforced Concrete Pipe (Type X) | LF | 1,200 | x | 260.00 | = | \$ | 312,000 |
| 68XXXX | XX" Plastic Pipe (Edge Drain) | LF |  | x |  | = | \$ | - |
| 69011X | XX" Corrugated Steel Pipe Downdrain (0.XXX" Thic | LF |  | x |  | $=$ | \$ | - |
| 70321X | XX" Corrugated Steel Pipe Inlet (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 70XXXX | XX" Corrugated Steel Pipe Riser (0.XXX" Thick) | LF |  | X |  | $=$ | \$ | - |
| 7050XX | XX" Steel Flared End Section | EA |  | X |  | $=$ | \$ | - |
| 703233 | Grated Line Drain | LF |  | X |  | $=$ | \$ | - |
| 72XXXX | Rock Slope Protection (Type and Method) | CY/TON |  | X |  | = | \$ | - |
| 72901X | Rock Slope Protection Fabric (Class X) | SQYD |  | X |  | = | \$ | - |
| 721420 | Concrete (Ditch Lining) | CY |  | X |  | = | \$ | - |
| 721430 | Concrete (Channel Lining) | CY |  | X |  | = | \$ | - |
| 750001 | Miscellaneous Iron and Steel | LB |  | x |  | = | \$ | - |
| 750029 | Inlet Frame and Grate | EA | 16 | x | 927.00 | $=$ | \$ | 14,832 |
| 7500xx | Other Drainage Items (7\% of Roadway) | LS | 1 | x | 1,250,000.00 | $=$ | \$ | 1,250,000 |

TOTAL DRAINAGE ITEMS

## SECTION 4: SPECIALTY ITEMS

| Item code |  |
| ---: | :--- |
| 080050 | Progress Schedule (Critical Path Method) |
| 582001 | Sound Wall (Masonry Block) |
| 510530 | Minor Concrete (Wall) |
| $15325 X$ | Remove Sound Wall |
| 070030 | Lead Compliance Plan |
| 141120 | Treated Wood Waste |
| 153221 | Remove Concrete Barrier |
| 150661 | Remove Metal Beam Guard Railing |
| 150668 | Remove Flared End Section |
| 8000 XX | Chain Link Fence (Type XX) |
| 80 XXXX | XX" Chain Link Gate (Type CL-6) |
| 832005 | Midwest Guardrail System |
| 839301 | Single Thrie Beam Barrier |
| 839310 | Double Thrie Beam Barrier |
| 839521 | Cable Railing |
| 839539 | Terminal System (Type SKT) |
| 839585 | Alternative Flared Terminal System |
| 839584 | Alternative In-line Terminal System |
| 4906 XX | CIDH Concrete Piling (Insert Diameter) |
| $839 X X X$ | Crash Cushion (Insert Type) |
| 839701 | Bike Trail Barrier (Type TBD) |
| 520103 | Bar Reinforced Steel (Retaining Wall) |
| 510060 | Structural Concrete, Retaining Wall |
| 513553 | Retaining Wall (Masonry Wall) |
| 511035 | Architectural Treatment |
| 598001 | Anti-Graffiti Coating |
| 203070 | Rock Stain |
| 5136 XX | Reinforced Concrete Crib Wall (Type X) |
| $83954 X$ | Transition Railing (Type X) |
| 597601 | Prepare and Stain Concrete |
| 839561 | Rail Tensioning Assembly |
| $83958 X$ | Some Item |
| 839701 | Some Item |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | X | 40,000.00 | $=$ | \$ | 40,000 |
| SQFT |  | X |  | = | \$ | - |
| CY |  | X |  | = | \$ | - |
| LF/LS |  | X |  | $=$ | \$ | - |
| LS |  | X |  | = | \$ | - |
| LB |  | X |  | = | \$ | - |
| LF |  | X |  | = | \$ | - |
| LF | 200 | x | 10.00 | = | \$ | 2,000 |
| EA | 3 | x | 500.00 | = | \$ | 1,500 |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF | 200 | X | 40.00 | = | \$ | 8,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA | 3 | x | 1,000.00 | = | \$ | 3,000 |
| EA |  | X |  | = | \$ | - |
| EA |  | X |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LB |  | x |  | = | \$ | - |
| CY |  | X |  | = | \$ | - |
| SQFT | 1,590 | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| SQFT |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| SQFT |  | X |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| EA |  | x |  | = | \$ | - |
| Unit |  | x |  | = | \$ | - |

## SECTION 5: ENVIRONMENTAL

5A - ENVIRONMENTAL MITIGATION

| Item code |  |
| :--- | :--- |
| 14XXXX | Biological Mitigation |
| 14XXXX | Archaeological Commitments |
| 14XXXX | Historical Commitments |
| 130670 | Temporary Reinforced Silt Fence |
| 141000 | Temporary Fence (Type ESA) |
| 14XXXX | Other Environmental Mitigation |
|  |  |
| 5B - LANDSCAPE AND IRRIGATION |  |
| Item code |  |
| 20XXXX | Highway Planting |
| 20XXXX | Irrigation System |
| 204099 | Plant Establishment Work |
| 204101 | Extend Plant Establishment Work |
| 20XXXX | Follow-up Landscape Project |
| 150685 | Remove Irrigation Facility |
| 20XXXX | Maintain Existing (Irrigation or Planted Areas) |
| 206400 | Check and Test Existing Irrigation Facilities |
| 21011X | Imported Topsoil (X) |
| 20XXXX | Rock Blanket, Rock Mulch, DG, Gravel Mulch |
| 200122 | Weed Germination |
| 208304 | Water Meter |
| 2087XX | XX" Conduit (Use for Irrigation x-overs) |
| 20890X | Extend X" Conduit (Irrigation X-overs) |

## 5C - EROSION CONTROL

| Item code |  |
| :--- | :--- |
| 210010 | Move In/Move Out (Erosion Control) |
| 210350 | Fiber Rolls |
| 210360 | Compost Sock |
| 2102 XX | Rolled Erosion Control Product (X) |
| $21025 X$ | Bonded Fiber Matrix |
| 210300 | Hydromulch |
| 210420 | Straw |
| 210430 | Hydroseed |
| 210600 | Compost |
| 210630 | Incorporate Materials |
| 2106 XX | Other Erosion Control |
|  |  |
| 5D - NPDES |  |
| Item code |  |
| 130300 | Prepare SWPPP |
| 130200 | Prepare WPCP |
| 130100 | Job Site Management |
| 130330 | Storm Water Annual Report |
| 130310 | Rain Event Action Plan (REAP) |
| 130320 | Storm Water Sampling and Analysis Day |
| 130520 | Temporary Hydraulic Mulch |
| 130550 | Temporary Hydroseed |
| 130505 | Move-In/Move-Out (Temp Erosion Control) |
| 130640 | Temporary Fiber Roll |
| 130900 | Temporary Concrete Washout |
| 130710 | Temporary Construction Entrance |
| 130610 | Temporary Check Dam |
| 130620 | Temporary Drainage Inlet Protection |
| 130730 | Street Sweeping |
| XXXXXX | Permenant BMPs |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 20,000.00 | $=$ | \$ | 20,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LS | 1 | x | 10,000.00 | $=$ | \$ | 10,000 |
| LF |  | x |  | = | \$ | - |
| LF |  | x |  | = | \$ | - |
| LS | 1 | x | 250,000.00 | = | \$ | 250,000 |


| Unit | Quantity | Unit Price (\$) |  |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |
| LS | 1 | X | 100,000.00 | = | \$ | 100,000 |
| LS | 1 | X | 50,000.00 | = | \$ | 50,000 |
| LS |  | x |  | = | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | = | \$ | - |
| LS |  | x |  | $=$ | \$ | - |
| LS |  | x |  | = | \$ | - |
| CY/TON |  | x |  | $=$ | \$ | - |
| SF/SY |  | x |  | = | \$ | - |
| SQYD |  | x |  | $=$ | \$ | - |
| EA |  | x |  | $=$ | \$ | - |
| LF |  | x |  | $=$ | \$ | - |
| LF |  | x |  | = | \$ | - |


| Unit | Quantity |
| :---: | :---: |
| EA |  |
| LF |  |
| LF |  |
| SQFT |  |
| FT/ACRE |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| SQFT |  |
| LS | 1 |


Unit
LS

## 6A - Traffic Electrical

| Item code | Unit |  |
| ---: | :--- | ---: |
| 860460 | Lighting and Sign Illumination | LS |
| 860201 | Signal and Lighting | EA |
| 860990 | Closed Circuit Television System | LS |
| 86110X | Ramp Metering System (Location X) | LS |
| 86070X | Interconnection Conduit and Cable | LS |
| $5602 X X$ | Furnish Sign Structure (Type X) | LB |
| $5602 X X$ | Install Sign Structure (Type X) | LF |
| 498040 | XX" CIDHC Pile (Sign Foundation) | LS |
| 860806 | Inductive Loop Detectors | LS |
| 8609XX | Traffic Monitoring Station (Type X) | EA/LS |
| $15075 X$ | Remove Sign Structure | EA |
| 151581 | Reconstruct Sign Structure | EA |
| 152641 | Modify Sign Structure | LS |
| 860090 | Maintain Existing Traffic Mgt. System | LS |
| 86XXXX | Fiber Optic Conduit System | LS |

6B - Traffic Signing and Striping

| Item code |  |
| :--- | :--- |
| 566011 | Roadside Sign - One Post |
| 566012 | Roadside Sign - Two Post |
| 5602 XX | Furnish Sign |
| 568016 | Install Sign Panel on Existing Frame |
| 150711 | Remove Painted Traffic Stripe |
| 141101 | Remove Yellow Stripe (Hazardous Waste) |
| 150712 | Remove Painted Pavement Marking |
| 150742 | Remove Roadside Sign |
| 152320 | Reset Roadside Sign |
| 152390 | Relocate Roadside Sign |
| 82010X | Delineator (Class X) |
| 840502 | Thermo Traffic Stripe |
| 846012 | Thermo Crosswalk and Pavement Marking |
| 120090 | Construction Area Signs |
| 84XXXX | Permanent Pavement Delineation |


| Unit | Quantity |  |
| :---: | :---: | :---: |
| EA | 50 | x |
| EA | 10 | x |
| SQFT |  | x |
| SQFT |  | x |
| LF | 51,744 | x |
| LF |  | x |
| SQFT |  | x |
| EA | 60 | x |
| EA |  | x |
| EA |  | x |
| EA |  | x |
| LF | 51,744 | x |
| SQFT |  | x |
| LS | 1 | x |
| LF | 38,808 | x |


| Unit Price (\$) | Cost |  |  |
| :---: | :---: | :---: | :---: |
| 500.00 | $=$ | \$ | 25,000 |
| 600.00 | $=$ | \$ | 6,000 |
|  | $=$ | \$ |  |
|  | $=$ | \$ |  |
| 1.00 | $=$ | \$ | 51,744 |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 150.00 | $=$ | \$ | 9,000 |
|  | = | \$ |  |
|  | = | \$ |  |
|  | $=$ | \$ |  |
| 0.55 | $=$ | \$ | 28,459 |
|  | $=$ | \$ |  |
| 5,000.00 | $=$ | \$ | 5,000 |
| 0.55 | $=$ | \$ | 21,344 |

$$
\text { Subtotal Traffic Signing and Striping } \$
$$

## 6C - Traffic Management Plan

Item code
12865X Portable Changeable Message Signs

| Unit | Quantity |  | Unit Price (\$) |  |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EA |  | x |  | $=$ | \$ | - |
| EA |  | x |  | = | \$ | - |
| EA |  | x |  | $=$ | \$ | - |
| EA | 420 | x | 250.00 | = | \$ | 105,000 |
| LS | 1 | x | 40,000.00 | = | \$ | 40,000 |
| EA |  | x |  | = | \$ | - |
| LF | 38,808 | x | 17.00 | $=$ | \$ | 659,736 |
| SQFT |  | x |  | = | \$ | - |
| LF | 155,232 | X | 2.00 | = | \$ | 310,464 |
| EA |  | x |  | = | \$ | - |
| LS | 1 | x | 48,000.00 | = | \$ | 48,000 |
| Unit | 1 | x | 300,000.00 | $=$ | \$ | 300,000 |

6C - Stage Construction and Traffic Handling

| Item code |  |
| :--- | :--- |
| 120199 | Traffic Plastic Drum |
| $12016 X$ | Channelizer (Type X) |
| 120120 | Type III Barricade |
| 129100 | Temporary Crash Cushion Module |
| 120100 | Traffic Control System |
| 129110 | Temporary Crash Cushion |
| 129000 | Temporary Railing (Type K) |
| 120149 | Temporary Pavement Marking (Paint) |
| 120151 | Temporary Pavement Striping (Paint) |
| 82010X | Delineator (Class X) |
| XXXXXX Temporary Ground Mounted Signs |  |
| XXXXXX | Other Street Improvements |

[^9]SECTION 7: DETOURS
Includes constructing, maintaining, and removal

| Item code | Unit |  |
| :---: | :--- | :---: |
| 190101 | Roadway Excavation | CY |
| 19801X | Imported Borrow | CY/TON |
| 390132 | Hot Mix Asphalt (Type A) | TON |
| $26020 X$ | Class 2 Aggregate Base | TON/CY |
| 250401 | Class 4 Aggregate Subbase | CY |
| 130620 | Temporary Drainage Inlet Protection | EA |
| 129000 | Temporary Railing (Type K) | LF |
| 128601 | Temporary Signal System | LS |
| 120149 | Temporary Pavement Marking (Paint) | SQFT |
| 80010X | Temporary Fence (Type X) | LF |
| XXXXXX Some Item | Unit |  |


| Quantity |  | Unit Price (\$) |  | Cost |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | x | = | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | $x$ | = | \$ | - |  |  |  |
|  | x | = | \$ | - |  |  |  |
|  | $x$ |  | \$ | - |  |  |  |
|  | x | $=$ | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x | = | \$ | - |  |  |  |
|  | x |  | \$ | - |  |  |  |
|  | x | = | \$ | - |  |  |  |
|  | x | = | \$ | - |  |  |  |
|  |  | TOTAL DE | TOURS |  | \$ |  | - |
|  |  | UBTOTAL SECTIO | ONS 1 th | through 7 |  |  | 13,119,300 |

## SECTION 8: MINOR ITEMS

| 8A - Americans with Disabilities Act Items |  |  |  |
| :--- | :--- | :--- | :--- |
| ADA Items <br> 8B - Bike Path Items <br> Bike Path Items <br> 8C - Other Minor Items <br> Other Minor Items |  | $5.0 \%$ | $\$$ |

## SECTIONS 9: MOBILIZATION

## Item code

999990 Total Section 1-8
\$ 15,087,200
10\%
$1,508,720$

TOTAL MOBILIZATION \$

## SECTION 10: SUPPLEMENTAL WORK

| Item code |  | U |
| :---: | :--- | :---: |
| 066670 | Payment Adjustments For Price Index | L |
| 066094 | Value Analysis | L |
| 066070 | Maintain Traffic | L |
| 066919 | Dispute Resolution Board | L |
| 066921 | Dispute Resolution Advisor | L |
| 066015 | Federal Trainee Program | L |
| 066610 | Partnering | L |
| 066204 | Remove Rock and Debris | L |
| 066222 | Locate Existing Crossover | U |

LS
LS
LS
LS
LS
LS
LS
LS
LS
Unit

Quantity Unit Price (\$)

|  | $=\$$ | - |
| :--- | :--- | ---: |
|  | $=\$$ | - |
| $200,000.00$ | $=\$$ | 200,000 |
|  | $=\$$ | - |
|  | $=\$$ | - |
|  | $=\$$ | - |
|  | $=\$$ | - |
|  | $=\$$ | - |
|  | $=\$$ | - |
|  | $=\$$ | - |

Cost of NPDES Supplemental Work specified in Section 5D $=\underline{\$}$

## PROJECT COST ESTIMATE

SECTION 11: STATE FURNISHED MATERIALS AND EXPENSES

| Item code |  | Unit |  | Quantity |  | Unit Price (\$) |  | Cost |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 066105 | Resident Engineers Office | LS |  | 1 | X | 200,000.00 | = | \$200,000 |  |
| 066063 | Traffic Management Plan - Public Information | LS |  | 1 | X | 120,000.00 | = | \$120,000 |  |
| 066901 | Water Expenses | LS |  |  | X |  | = | \$0 |  |
| 8609XX | Traffic Monitoring Station (X) | LS |  |  | X |  | = | \$0 |  |
| 066841 | Traffic Controller Assembly | LS |  |  | X |  | = | \$0 |  |
| 066840 | Traffic Signal Controller Assembly | LS |  |  | x |  | = | \$0 |  |
| 066062 | COZEEP Contract | LS |  | 1 | X | 170,000.00 | = | \$170,000 |  |
| 066838 | Reflective Numbers and Edge Sealer | LS |  |  | X |  | = | \$0 |  |
| 066065 | Tow Truck Service Patrol | LS |  | 1 | X | 250,000.00 | = | \$250,000 |  |
| 066916 | Annual Construction General Permit Fee | LS |  |  | X |  | = | \$0 |  |
| XXXXXX | Some Item | Unit |  |  | x |  | = | \$0 |  |
|  | Total Section 1-8 |  | \$ | 15,087,200 |  | 4\% | $=\$$ | 603,488 |  |
|  |  |  |  |  | TOTAL STATE FURNISHED |  |  |  | \$1,343,500 |

## SECTION 12: TIME-RELATED OVERHEAD

## Total of Roadway and Structures Contract Items excluding Mobilization <br> Total Construction Cost (excluding TRO and Contingency)

\$15,087,200 (used to calculate TRO)
$\$ 18,782,000$ (used to check if project is greater than $\$ 5$ million excluding contingency)
Estimated Time-Related Overhead (TRO) Percentage (0\% to 10\%) =
10\%

| Item code |  | Unit | Quantity |  | Unit Price (\$) |  | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 070018 | Time-Related Overhead | WD | 650 | X | \$2,321 | = | \$1,508,800 |

## TOTAL TIME-RELATED OVERHEAD

Note: If the building portion of the project is greater than $50 \%$ of the total project cost, then TRO is not included.

## SECTION 13: ROADWAY CONTINGENCY

Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

## II. STRUCTURE ITEMS

Bridge 1

| DATE OF ESTIMATE | 00/00/00 | 00/00/00 | 00/00/00 |
| :---: | :---: | :---: | :---: |
| Bridge Name | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Bridge Number | 57-XXX | 57-XXX | 57-XXX |
| Structure Type | Pedestrian OC | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Width (Feet) [out to out] | 0 LF | 0 LF | 0 LF |
| Total Bridge Length (Feet) | 0 LF | 0 LF | 0 LF |
| Total Area (Square Feet) | 0 SQFT | 0 SQFT | 0 SQFT |
| Structure Depth (Feet) | 0 LF | 0 LF | 0 LF |
| Footing Type (pile or spread) | TBD | xxxxxxxxxxxxxxxxxxx | xxxxxxxxxxxxxxxxxxx |
| Cost Per Square Foot | \$1,750 | \$0 | \$0 |
| COST OF EACH | \$0 | \$0 | \$0 |

DATE OF ESTIMATE<br>Name<br>Bridge Number<br>Structure Type<br>Width (Feet) [out to out] Total Length (Feet)<br>Total Area (Square Feet)<br>Structure Depth (Feet)<br>Footing Type (pile or spread)<br>Cost Per Square Foot

00/00/00 xxxxxxxxxxxxxxxxxxx 57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF xxxxxxxxxxxxxxxxxxx $\$ 100$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx
$\$ 0$

00/00/00
xxxxxxxxxxxxxxxxxxx
57-XXX xxxxxxxxxxxxxxxxxxx

0 LF
0 LF
0 SQFT
0 LF
xxxxxxxxxxxxxxxxxxx $\$ 0$

| COST OF EACH | \$0 |  | $\$ 0$ |  | $\$ 0$ |
| :---: | :---: | :---: | :---: | :---: | :---: |



Recommended Contingency: (Pre-PSR 30\%-50\%, PSR 25\%, Draft PR 20\%, PR 15\%, after PR approval 10\%, Final PS\&E 5\%)

Structures Contingency Percentage $10 \% \quad$| \$0 |
| :--- |

## TOTAL COST OF STRUCTURES

Estimate Prepared By:

## III. RIGHT OF WAY

Fill in all of the available information from the Right of Way data sheet.

L)

TOTAL RIGHT OF WAY ESTIMATE
\$63,688,677
M)

TOTAL R/W ESTIMATE: Escalated
\$77,700,186
N)

RIGHT OF WAY SUPPORT
\$3,846,875


[^10]
## IV. SUPPORT COST ESTIMATE SUMMARY

| Note: Use PRSM project data. |  | Escalated Support Cost for Estimate To Completion (ETC) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total by FY |  | PA\&ED | PS\&E | RW | CON | Total \$ |
| <2014 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2015 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2016 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2017 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2018 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2019 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2020 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2021 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2022 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2023 | Expended | \$2,000,000 |  |  |  | \$2,000,000 |
|  | ETC |  |  |  |  |  |
| 2024 | Expended | \$2,375,000 |  |  |  | \$2,375,000 |
|  | ETC |  |  |  |  |  |
| 2025 | Expended |  | \$2,500,000 | \$1,282,292 |  | \$3,782,292 |
|  | ETC |  |  |  |  |  |
| 2026 | Expended |  | \$2,500,000 | \$2,564,583 |  | \$5,064,583 |
|  | ETC |  |  |  |  |  |
| 2027 | Expended |  |  |  | \$5,000,000 | \$5,000,000 |
|  | ETC |  |  |  |  |  |
| 2028 | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| 2029> | Expended |  |  |  |  |  |
|  | ETC |  |  |  |  |  |
| EAC (Expended + ETC) |  | \$4,375,000 | \$5,000,000 | \$3,846,875 | \$5,000,000 | \$18,221,875 |
| Approved Budget (PRSM) |  |  |  |  |  |  |
| Difference (Budget - EAC) |  | -\$4,375,000 | -\$5,000,000 | -\$3,846,875 | -\$5,000,000 | -\$18,221,875 |
| Support Ratio (EAC / Cap Cost) |  | 3.7\% | 4.2\% | 3.3\% | 4.2\% | 15.4\% |


| Total Capital Cost: | $\$ 117,965,814$ |
| :---: | :---: |
| Total Capital Outlay Support Cost: | $\$ 18,221,875$ |
| Overall Percent Support Cost: | $15.45 \%$ |

## ATTACHMENT D

## TRAFFIC ENGINEERING PERFORMANCE ASSESSMENT (TEPA)

(With Attachments)

## $1-22$



# Traffic Engineering <br> Performance Assessment 

Laguna Canyon Road Improvements
12-OC-133 - PM 0.9-3.4
EA: 0Q670K - ID 1217000086
Laguna Beach, CA June 13, 2022


Caltrans:

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## 1 Introduction

This section describes the purpose of this study, study area, and report organization.

### 1.1 Project Description

One of the most significant challenges facing City of Laguna Beach is managing increasing traffic congestion along Laguna Canyon Road (LCR) (State Route 133). The City of Laguna Beach (City), in cooperation with the California Department of Transportation (CALTRANS) proposes improvements along State Route 133 (SR133), Laguna Canyon Road. The project area extends from approximately Canyon Acres Drive to El Toro Road. LCR is one of the three gateways to Laguna Beach and provides critical access to adjacent recreational spaces as well as activities in the City. Figure 1-1 shows the regional location and project vicinity and Figure 1-2 presents the project area limits.

This project is intended as a 'Complete Streets' project which is consistent with Caltrans' latest Transportation Concept Report (TCR) for SR-133. No capacity improvements are proposed as part of this project. The project would include operational improvements at select locations, provide transit access and bike and pedestrian facilities and undergrounding of existing utilities.

### 1.2 Study Area and Project Background

As part of the State Highway System, LCR connects Pacific Coast Highway (SR-1) and other coastal areas with three of the key inland freeways namely I-5, l-405 and SR-73. The study area extends approximately 2.5 miles along LCR and transitions from the Laguna Canyon area into unincorporated Orange County extending to the junction with El Toro Road. This segment of the corridor consists of a two-lane highway with a center two-way left turn lane (TWLTL) and limited on-street parking and no designated bikeways. The corridor lacks adequate shoulders and pedestrian and bicycle facilities within the project limits. The right-of-way is constrained by residential and light commercial developments as well as various open space/environmental constraints along the route. The route is further constrained by overhead Southern California Edison's (SCE) transmission and distribution lines in close proximity to the roadway that pose safety concerns.

Figure 1-1. Project Location \& Vicinity Map


Figure 1-2. Project Limits


Based on discussions with the City and Caltrans, the study area consists of nine (9) study intersections/locations along the corridor between El Toro Road and Canyon Acres Drive. Figure 1-3 shows the study intersections and driveways.

## Study Intersections/Driveways:

1. Laguna Canyon Road (LCR)/SR-133 at El Toro Road
2. Laguna Canyon Road (LCR)/SR-133 at Anneliese's School Driveway
3. Laguna Canyon Road (LCR)/SR-133 at Sun Valley Drive
4. Laguna Canyon Road (LCR)/SR-133 at Laguna Beach Dog Park Driveway
5. Laguna Canyon Road (LCR)/SR-133 at Stan Oaks Drive
6. Laguna Canyon Road (LCR)/SR-133 at Castle Rock Road
7. Laguna Canyon Road (LCR)/SR-133 at Laguna College of Art and Design Driveway
8. Laguna Canyon Road (LCR)/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway
9. Laguna Canyon Road (LCR)/SR-133 at Canyon Acres Drive

Figure 1-3. Study Intersections


### 1.3 Need and Purpose

LCR is a critical access route for the City of Laguna Beach today and will continue to remain so in the future. Traffic demand for the corridor is at capacity during peak hours of the day/week and is expected to increase by nearly 50 percent from approximately 36,000 to approximately 54,500 vehicles per day by the year 2050. The corridor within the project limits experiences substantial congestion at two bottleneck locations during the period of high visitor travel to the City. These periods include typical weekdays, most summer weekends and holidays. Additionally, congestion is observed during a typical weekday peak period without high visitor travel. The two bottlenecks occur at the southbound travel lane just south of El Toro Road intersection, and the northbound travel lane just north of Canyon Acres Drive where the corridor transitions from two northbound lanes to one northbound lane. According to Caltrans Table C, which lists the potential investigation locations, these locations are above average collision locations compared to similar facilities statewide with a high concentration of collisions at the non-standard lane merges.

The corridor consists of a two-lane highway with limited on-street parking and no designated bikeway. The right-of-way is constrained by residential and light commercial developments as well as various environmental constraints along the route. The route is further constrained by overhead SCE transmission and distribution lines in close proximity to the roadway that pose safety concerns. Pedestrians and bicycles come in close proximity of high speeding vehicles due to lack of pedestrian and bicycle facilities. Lack of sight distance around the Big Bend area have resulted in high number of accidents along the corridor. The on-street parking at the dog park area creates congestion and increases the potential for collisions. Based on field observations, there are several other safety hot-spot locations along the corridor which are prone to high accidents due to illegal U-turns, angled on-street parking, unsafe driveway exits, failing to stay in their travel lane due to inadequate superelevation along the curves, red light violations, and improper merge at lane drops. Based on information from the City's police department, the corridor within the project limits has experienced approximately 75 traffic accidents per year over a period of seven and half years. Additionally, the data obtained from Caltrans' Traffic Accident and Surveillance Analysis Systems (TASAS) was used to conduct the accident analysis presented in this report.

Without operational improvements, including accommodations for safety improvements and provisions for alternative transportation modes such as City transit services and bike and pedestrian paths, the quality and level of service along the corridor would continue to degrade.

The purpose of the project is to provide pedestrian and bike facilities and center twoway left turn lane for the existing two travel lanes along the corridor within the project limits. Under some circumstances and as an alternative, the center two-way left turn lane could be used as a reversible lane. No additional lanes are proposed and the incorporation of traffic calming and active transportation features would provide continuous access to transit and pedestrian and bike facilities. The proposed
improvements include a dedicated pedestrian pathway and off-street bicycle lanes within the project limits. Overhead utilities within the right-of-way and in close proximity to the edge of travel way are proposed to be relocated or undergrounded where feasible.

### 1.4 Report Organization

Following this introduction chapter, this report is organized into the following chapters:
2.0 Project Alternatives - This chapter describes four proposed project alternatives.
3.0 Existing Conditions - This chapter describes the existing traffic network within the study area and summarize operational deficiencies for existing traffic conditions including accident analysis.
4.0 Traffic Volume Forecasts - This chapter describes the future forecasting methodology and presents the forecast traffic volumes for Opening Year (2030) and Horizon Year (2050) conditions.
5.0 Analysis Methodology - This chapter describes the methodologies, standards, and thresholds utilized to perform various Levels of Service Analyses.
6.0 Traffic Engineering Performance Assessment Findings - This chapter presents the analysis results for Existing (2017), Opening Year (2030) and Horizon Year (2050) conditions. It also presents a discussion on operational deficiencies and results from intersection evaluation.
7.0 Summary and Conclusion - This chapter summarizes the overall study results and presents key findings.
8.0 Scope of Future Traffic Engineering Studies - This chapter describes the scope of future traffic engineering studies intended to address outstanding operational and safety issues.

## 2 Project Alternatives

This section describes the Project Alternatives including a No Build condition. The Project Alternatives include complete street elements such as bike and pedestrian facilities and transit services. Due to limited right-of-way, a constrained condition for each build alternative was analyzed, for which the improvements are proposed within the existing right-of-way along most of the study corridor.

### 2.1 Alternative 1 (No Build)

The No Build Alternative would maintain the corridor in its current condition. No improvements would be implemented therefore, no capital costs are associated with this alternative. Utility poles on both the NB and SB sides of the road would not be undergrounded to allow full use of the State ROW for complete street elements to be incorporated into the corridor that encourage increased use of active modes of transportation. As the traffic demand increases, traffic operation would further deteriorate, which may result in an increase in congestion, vehicle queuing, vehicle delay, and safety issues. This alternative would not satisfy the Purpose and Need of the Project.

The No Build Alternative includes the improvements completed by Caltrans for the Canyon Acres Drive Intersection improvements as further described in Section 7 of this PSR/PDS.

The No Build Alternative is being considered because it serves as the baseline against which to evaluate the effectiveness of the proposed Build Alternatives. This alternative allows decision makers to make a comparison between the impacts of the Build Alternatives and the impacts of the No Build scenario.

### 2.2 Alternative 2

Alternative 2 generally consists of a typical width of approximately 64 feet for the majority of the route including vehicle, pedestrian and bicycle facilities. This alternative includes 11-to-12-foot travel lanes, a 10-to-12-foot center TWLTL, 5-to-7-foot shoulders in both the NB and SB directions, and a pedestrian path/sidewalk on the NB side. Alternative 2 also includes a 12-foot-wide Class IV separated bikeway on the SB side of the roadway. During emergencies, there is space for up to four outbound evacuation travel lanes on the roadway and one inbound emergency vehicle lane by utilizing the bike lane. A representative cross section is presented in Figure 2-1. See PSR/PDS for cross sections in detail.

Within the constrained segment, in the vicinity of the 'Big Bend,' the SB shoulder is eliminated and the adjacent bikeway becomes a Class I shared-use path. At the pinch point of minimum 53 feet available ROW width, the NB parking lane/shoulder would end within this short segment.

### 2.3 Alternative 3

Alternative 3 generally consists of a typical width of approximately 64 feet for the majority of the route, including vehicle, pedestrian and bicycle facilities. This alternative includes 11-to-12-foot travel lanes, a 10-to-12-foot center TWLTL, 5-to-7foot bike lane and 5-to-6-foot pedestrian path/sidewalk on the NB side of the roadway. Alternative 3 also includes a 10-to-12-foot Class IV separated bikeway with adjacent pedestrian path on the SB side of the roadway. During emergencies, there is space for three outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lane. A representative cross section is presented in Figure 2-2. See PSR/PDS for cross sections in detail.

Within the constrained segment, in the vicinity of the 'Big Bend,' the dedicated pedestrian path on the SB side of the roadway would be eliminated and the buffer between the shared-use Class IV bike path and the SB travel lane would be narrowed. At the pinch point of approximately 53 feet available ROW width, the 7 -foot shoulder/Class II bike lane on the NB side would be removed within this short segment.

### 2.4 Alternative 4

Alternative 4 generally consists of a typical width of approximately 64 feet for the majority of the route including vehicle, pedestrian and bicycle facilities. This alternative includes 11-to-12-foot travel lanes, and a 10 -foot center TWLTL, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5-to-8-foot Class II buffered bike lane on both sides of the roadway. During emergencies, there is space for up to four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes. A representative cross section is presented in Figure 2-3. See PSR/PDS for cross sections in detail.
Within the constrained segment, in the vicinity of the 'Big Bend,' the bike lane widths would be reduced to five feet and the travel lanes reduced to 11 feet. At the pinch point of approximately 53 feet available ROW width, the pedestrian paths and bike lane buffers on either side of the roadway would be reduced within this short segment.

### 2.5 Alternative 5

Alternative 5 generally consists of a typical width of approximately 64 feet for the majority of the route including vehicle, pedestrian and bicycle facilities. With a reversible lane, the cross-section would include 11-to-12-foot travel lanes, and a 12-to-14-foot center reversible lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5 -foot Class II buffered bike lane/shoulder on both sides of the roadway. During emergencies, the configuration could provide for up to four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes. A representative cross section is presented in Figure 2-4. See PSR/PDS for cross sections in detail.

Within the constrained segment, in the vicinity of the 'Big Bend', the travel lanes reduced to 11 feet. At the pinch point of approximately 53 feet available ROW width, the pedestrian paths and bike lane buffers on either side of the roadway would be reduced within this short segment.

Figure 2-1. Alternative 2 Cross-Section


Figure 2-2. Alternative 3 Cross-Section


Figure 2-3. Alternative 4 Cross-Section


Figure 2-4. Alternative 5 Cross-Section


## 3 Existing Conditions

This section describes key roadway segments and intersections; reports existing daily roadway and peak hour intersection traffic volume information; and summarizes existing operational deficiencies.

### 3.1 Existing Roadway Network

Laguna Canyon Road (LCR) (SR-133) - it is a 13.6 mile long north-south state highway with a southern terminus in the City of Laguna Beach at Pacific Coast Highway (SR-1) and northern terminus in the City of Irvine at Foothill/Eastern Transportation Corridor Toll Road (SR-241).

El Toro Road - it is an 11.5 mile long east-west major arterial highway with a southern terminus at LCR and a northern terminus with Santiago Canyon Road and Live Oak Canyon Road. El Toro Road is a six-lane highway from San Joaquin Hills Corridor Toll Road (SR-73) extending northeasterly through the cities of Laguna Woods and Lake Forest. El Toro Road is a two-lane highway between LCR and San Joaquin Hills Corridor Toll Road (SR-73). The intersection of LCR and EI Toro Road is signalized.

Anneliese's School Driveway - it is a two lane east-west driveway which provides access to the Anneliese's School. The intersection of LCR and Anneliese's School Driveway is stop-controlled.

Willow Canyon Road - it is an entrance road/trail to Willow Canyon Staging area. Willow Canyon Staging area provides access to the Laguna Coast Wilderness Park and is operated by OC Parks. The intersection of LCR and Willow Canyon Road is stop-controlled.

Sun Valley Drive - it is a two lane east-west roadway which provides access to residential areas. The intersection of LCR and Sun Valley Drive is stop-controlled.
Laguna Beach Dog Park Driveway - it is a two-lane local roadway which provides access to the dog park area from LCR. The intersection of LCR and Laguna Beach Dog Park Driveway is stop-controlled.
Stan Oaks Drive - it is a two lane east-west roadway which provides access to the local businesses. It connects these businesses to LCR. The intersection of LCR and Stan Oaks Drive is stop-controlled.

Castle Rock Road - it is a two lane east-west roadway which provides access to the local businesses and residential areas. It is a winding road which connects these businesses to LCR. The intersection of LCR and Castle Rock Road is stop-controlled.
Laguna College of Arts and Design Driveway - it is a two lane east-west roadway which provides access to the Laguna College of Arts and Design parking lots. It provides a direct access from LCR. The intersection of LCR and Laguna College of Arts and Design Driveway is stop-controlled.

Act V/City Maintenance Yard Facility Parking Lot Driveway - it is a two lane eastwest roadway which provides access to the public parking lot. The parking lot also serves as a trolley stop. The intersection of LCR and Act V/City Maintenance Yard Facility Parking Lot Driveway is stop-controlled.

Canyon Acres Drive - is an east-west collector providing local residents' access to LCR. Canyon Acres Drive eastern terminus is a cul-de-sac approximately 0.5 miles east of LCR. Western terminus of Canyon Acres Drive is at LCR. The intersection of LCR and Canyon Acres Drive is signalized.

### 3.2 Existing Traffic Volumes

For arterial segments, counts were collected over a 24 -hour period and reported in 15minute intervals on Thursday November 30, 2017. Weekday intersection AM and PM peak period counts were collected on $2^{\text {nd }}$ December and $25^{\text {th }}$ January 2018. All traffic counts were collected while all educational institutions in the vicinity of the project were in session, thereby ensuring the validity of data collection. The counts represent a typical weekday commuter traffic during a non-peak season. Since the month of November is within seasonal off-peak period and does not have highest yearly traffic volumes on the corridor, traffic conditions (due to recreational traffic) during peak season are expected to be worse than what is presented in this Study.
For the intersections that traffic counts were not directly collected, turning movement volumes were developed using arterial counts collected and the ITE trip generation manual to estimate the diverging traffic into and out of the cross streets/driveways.

Table 3-1 presents the existing peak hour and daily counts for the four highway segments along the corridor. Table 3-2 and Table 3-3 present the existing AM and PM peak hour segment and intersection turning movement volumes respectively. Figure 3-1 presents existing intersection turning movement volumes under existing conditions. Note that the volumes were balanced to conserve flow. Appendix A provides the traffic count worksheets.

Table 3-1. Existing Highway Segment Volumes

| ID | Segment | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LCR/SR-133 | Btwn. El Toro Road \& Sun Valley Drive | Northbound | 1,006 | 1,348 | 36,337 |
|  |  |  | Southbound | 1,239 | 1,251 |  |
| 2 | LCR/SR-133 | Btwn. Sun Valley Drive \& Stan Oaks Drive | Northbound | 988 | 1,350 | 36,373 |
|  |  |  | Southbound | 1,267 | 1,264 |  |
| 3 | LCR/SR-133 | Btwn. Stan Oaks Drive \& LCAD Driveway | Northbound | 989 | 1,306 | 35,690 |
|  |  |  | Southbound | 1,249 | 1,282 |  |
| 4 | LCR/SR-133 | Btwn. LCAD Driveway \& Canyon Acres Drive | Northbound | 1,032 | 1,307 | 36,088 |
|  |  |  | Southbound | 1,235 | 1,301 |  |

Table 3-2. Existing AM Peak Hour Intersection Turning Movement Volumes

| ID | Description | NBL ${ }^{1}$ | NBT ${ }^{2}$ | NBR ${ }^{3}$ | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LCR/SR-133 at El Toro Road | 0 | 915 | 511 | 19 | 895 | 0 | 0 | 0 | 657 | 12 | 3009 |
| 2 | LCR/SR-133 at Anneliese's School Driveway | 0 | 1292 | 27 | 165 | 1383 | 0 | 0 | 0 | 17 | 143 | 3027 |
| 3 | LCR/SR-133 at Sun Valley Drive | 0 | 1194 | 1 | 2 | 1351 | 0 | 0 | 0 | 4 | 6 | 2558 |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | 0 | 1184 | 11 | 14 | 1341 | 0 | 0 | 0 | 9 | 11 | 2570 |
| 5 | LCR/SR-133 at Stan Oaks Drive | 0 | 1189 | 1 | 2 | 1348 | 0 | 0 | 0 | 4 | 6 | 2550 |
| 6 | LCR/SR-133 at Castle Rock Road | 0 | 1182 | 2 | 3 | 1349 | 0 | 0 | 0 | 6 | 8 | 2550 |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | 52 | 1129 | 0 | 0 | 1313 | 42 | 55 | 45 | 0 | 0 | 2636 |
| 8 | LCR/SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 76 | 1101 | 0 | 0 | 1296 | 62 | 80 | 66 | 0 | 0 | 2681 |
| 9 | LCR/SR-133 at Canyon Acres Drive | 7 | 1307 | 13 | 11 | 1280 | 0 | 0 | 0 | 37 | 14 | 2669 |
| ${ }^{1} \mathrm{~L}=$ Left $-{ }^{2} \mathrm{~T}=$ Through $-{ }^{3} \mathrm{R}=$ Right |  |  |  |  |  |  |  |  |  |  |  |  |

Table 3-3. Existing PM Peak Hour Intersection Turning Movement Volumes

| ID | Description | NBL1 | NBT ${ }^{2}$ | NBR ${ }^{3}$ | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LCR/SR-133 at El Toro Road | 0 | 652 | 699 | 32 | 789 | 0 | 0 | 0 | 517 | 29 | 2718 |
| 2 | LCR/SR-133 at Anneliese's School Driveway | 0 | 1282 | 8 | 49 | 1257 | 0 | 0 | 0 | 10 | 56 | 2662 |
| 3 | LCR/SR-133 at Sun Valley Drive | 0 | 1321 | 6 | 2 | 1147 | 0 | 0 | 0 | 2 | 2 | 2480 |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | 0 | 1324 | 5 | 2 | 1147 | 0 | 0 | 0 | 4 | 3 | 2485 |
| 5 | LCR/SR-133 at Stan Oaks Drive | 0 | 1327 | 6 | 2 | 1149 | 0 | 0 | 0 | 3 | 2 | 2489 |
| 6 | LCR/SR-133 at Castle Rock Road | 0 | 1330 | 8 | 3 | 1149 | 0 | 0 | 0 | 4 | 3 | 2497 |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | 4 | 1325 | 0 | 0 | 1143 | 10 | 13 | 19 | 0 | 0 | 2514 |
| 8 | LCR/SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 6 | 1310 | 0 | 0 | 1147 | 15 | 19 | 29 | 0 | 0 | 2526 |
| 9 | LCR/SR-133 at Canyon Acres Drive | 11 | 1201 | 28 | 14 | 1191 | 0 | 0 | 0 | 18 | 13 | 2476 |
| ${ }^{1} \mathrm{~L}=$ Left $-{ }^{2} \mathrm{~T}=$ Through $-{ }^{3} \mathrm{R}=$ Right |  |  |  |  |  |  |  |  |  |  |  |  |

Figure 3-1. Existing Intersection Peak Hour Volumes


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20 | June 13, 2022

### 3.3 Accident Analysis

Traffic accident data was assembled from Caltrans' Traffic Accident and Surveillance Analysis Systems (TASAS) for a 60-month period, January 1, 2016 through December 31, 2020. Table 3-4 provides a summary of Caltrans' TASAS Table B - Selective Accident Rate Calculation (Table B). Table B provides actual and average rates for highways and intersections. TASAS Selective Accident Retrieval (TSAR) provides a summary of type of accident by location. Table $B$ and TSAR accident data are provided in Appendix B.

In order to analyze accident data for various sections of LCR, the corridor was divided into five zones. Zone 1 is located south of Canyon Acres Drive outside of the accident data area and project study area. Therefore, no accident data is presented for Zone 1 in Table 3-4 and Table 3-5. Zone 2 is the section from Canyon Acres Drive to Laguna College of Art and Design which is 3,200 feet north of Canyon Acres Drive. Zone 3 is from Laguna College of Art and Design to Stan Oaks Drive. Zone 4 is from Stan Oaks Drive to Anneliese's School. Zone 5 is from Anneliese's School to 350 feet north of El Toro Road. Figure 3-2 shows the accident analysis zones.

Caltrans' TASAS data for January 1, 2016 to December 31, 2020 indicates a total of 166 collisions for all the zones within the study area, Canyon Acres Drive to El Toro Road (Zone 2 to Zone 5). The majority of the collisions were classified as rear end type collision with the majority cited for unsafe speed. The $2^{\text {nd }}$ leading collision type was hit object followed by sideswipe type of collision. Table 3-4 provides a summary of Caltrans' accident rates. Table 3-5 provides a summary of accident type.

Figure 3-2. Accident Analysis Zones


Table 3-4. Summary of Caltrans' TASAS Table B

| Post Mile (PM) | Location | Number of Accidents |  |  |  | Actual Accident Rates ${ }^{1}$ |  |  | Average Accident Rates ${ }^{1}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total (T) | Fatal (F) | Injury <br> (I) | F+l | Fatal | F+I | Total | Fatal | F+I | Total |
| Zone 2 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Road/SR-133 Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 0.94 \text { to } \\ 1.573 \end{gathered}$ | From Canyon Acres Drive to Laguna Canyon of Arts and Design | 35 | 0 | 14 | 14 | 0.00 | 0.68 | 1.70 | 0.012 | 0.40 | 0.83 |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 0.94 \text { to } \\ 1.573 \end{gathered}$ | From Laguna Canyon Arts and Design to Canyon Acres Drive | 16 | 0 | 7 | 7 | 0.00 | 0.34 | 0.78 | 0.012 | 0.40 | 0.83 |
| Zone 3 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 1.573 \text { to } \\ 2.446 \end{gathered}$ | From Laguna Canyon Arts and Design to Stan Oaks Drive | 30 | 0 | 16 | 16 | 0.00 | 0.55 | 1.03 | 0.013 | 0.40 | 0.82 |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 1.573 \text { to } \\ 2.446 \end{gathered}$ | From Stan Oaks Drive to Laguna Canyon Arts and Design | 17 | 0 | 10 | 10 | 0.00 | 0.34 | 0.58 | 0.013 | 0.40 | 0.82 |
| Zone 4 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 2.446 \text { to } \\ 3.330 \end{gathered}$ | From Stan Oaks Drive to Anneliese's School | 36 | 0 | 20 | 20 | 0.00 | 0.66 | 1.19 | 0.013 | 0.40 | 0.82 |

Table 3-4. Summary of Caltrans' TASAS Table B

| Post Mile (PM) | Location | Number of Accidents |  |  |  | Actual Accident Rates ${ }^{1}$ |  |  | Average Accident Rates ${ }^{1}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total (T) | Fatal (F) | Injury <br> (I) | F+l | Fatal | F+I | Total | Fatal | F+I | Total |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 2.446 \text { to } \\ 3.330 \end{gathered}$ | From Anneliese's School to Stan Oaks Drive | 24 | 0 | 17 | 17 | 0.00 | 0.56 | 0.79 | 0.013 | 0.40 | 0.82 |
| Zone 5 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 3.330 \text { to } \\ 3.415 \end{gathered}$ | From Anneliese's School to El Toro Road | 2 | 0 | 0 | 0 | 0.00 | 0.00 | 0.74 | 0.013 | 0.40 | 0.82 |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 3.330 \text { to } \\ 3.415 \end{gathered}$ | From El Toro Road to Anneliese's School | 6 | 0 | 2 | 2 | 0.00 | 0.74 | 2.23 | 0.013 | 0.40 | 0.82 |

Source: Caltrans District 12 TASAS Table B (January 2016 to December 2020)
Notes: 1 - the accident rate is the number of accidents per million vehicle-miles.
Bold indicates an actual accident rate that is higher than the average accident rate.

Table 3-5. Summary of Accidents by Type

| $\begin{aligned} & \text { PM (post } \\ & \text { mile) } \end{aligned}$ | Location | Accident Type |  | $\%$ $\frac{\circ}{3}$ $\frac{8}{6}$ $\frac{\circ}{\circ}$ |  | $\circ$ <br> $\stackrel{0}{0}$ <br> 0 <br> 0 <br> 0 | $\begin{aligned} & \text { 허 } \\ & \stackrel{0}{\circ} \\ & \stackrel{0}{2} \\ & \text { 호 } \end{aligned}$ | 돌 눙 0 0 | $\frac{\stackrel{c}{\frac{N}{5}}}{\frac{1}{6}}$ | $\begin{aligned} & \text { あ } \\ & \stackrel{5}{\mathbf{0}} \end{aligned}$ | $\frac{1}{\frac{1}{l}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ZONE 2 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| PM 0.94 to | From Canyon Acres Drive to | Total | 3 | 4 | 22 | 3 | 2 | 1 | 0 | 0 | 35 |
| 1.573 | Design | Percent | 8.6\% | 11.4\% | 62.9\% | 8.6\% | 5.7\% | 2.9\% | 0.0\% | 0.0\% | 100\% |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 0.94 \text { to } \\ 1.573 \end{gathered}$ | From Laguna Canyon Arts and Design to Canyon Acres Drive | Total | 2 | 2 | 4 | 0 | 4 | 2 | 0 | 2 | 16 |
|  |  | Percent | 12.5\% | 12.5\% | 25.0\% | 0.0\% | 25.0\% | 12.5\% | 0.0\% | 12.5\% | 100\% |
| ZONE 3 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 1.573 \text { to } \\ 2.446 \end{gathered}$ | From Laguna Canyon Arts and Design to Stan Oaks Drive | Total | 3 | 5 | 11 | 6 | 3 | 1 | 1 | 0 | 30 |
|  |  | Percent | 10.0\% | 16.7\% | 36.7\% | 20.0\% | 10.0\% | 3.3\% | 3.3\% | 0.0\% | 100.0\% |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 1.573 \text { to } \\ 2.446 \end{gathered}$ | From Stan Oaks Drive to Laguna Canyon Arts and Design | Total | 3 | 0 | 7 | 0 | 6 | 0 | 1 | 0 | 17 |
|  |  | Percent | 17.6\% | 0.0\% | 41.2\% | 0.0\% | 35.3\% | 0.0\% | 5.9\% | 0.0\% | 100.0\% |
| ZONE 4 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 2.446 \text { to } \\ 3.330 \end{gathered}$ | From Stan Oaks Drive to Anneliese's School | Total | 2 | 3 | 20 | 4 | 4 | 1 | 1 | 1 | 36 |
|  |  | Percent | 5.6\% | 8.3\% | 55.6\% | 11.1\% | 11.1\% | 2.8\% | 2.8\% | 2.8\% | 100\% |

Table 3-5. Summary of Accidents by Type

| PM (post mile) | Location | Accident Type |  | $\circ$ $\frac{2}{3}$ $\%$ $\frac{0}{\omega}$ |  |  | $\begin{aligned} & \text { 허 } \\ & \stackrel{0}{\circ} \\ & \stackrel{1}{0} \\ & \text { 호 } \end{aligned}$ | $\begin{aligned} & \text { 등 } \\ & \text { 年 } \\ & 0 \end{aligned}$ |  | $\begin{gathered} \stackrel{\text { ¢ }}{屯} \\ \hline \end{gathered}$ | $\frac{1}{\frac{1}{6}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\text { PM } 2.446 \text { to }$$3.330$ | From Anneliese's School to Stan Oaks Drive | Total | 2 | 2 | 13 | 0 | 3 | 3 | 0 | 1 | 24 |
|  |  | Percent | 8.3\% | 8.2\% | 54.2\% | 0.0\% | 12.5\% | 12.5\% | 0.0\% | 4.2\% | 100\% |
| ZONE 5 |  |  |  |  |  |  |  |  |  |  |  |
| Laguna Canyon Rd Northbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 3.330 \text { to } \\ 3.415 \end{gathered}$ | From Anneliese's School to El Toro Road | Total | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
|  |  | Percent | 0.0\% | 0.0\% | 0.0\% | 50.0\% | 50.0\% | 0.0\% | 0.0\% | 0.0\% | 100\% |
| Laguna Canyon Rd Southbound |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { PM } 3.330 \text { to } \\ 3.415 \end{gathered}$ | From El Toro Road to Anneliese's School | Total | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 0 | 6 |
|  |  | Percent | 0.0\% | 33.3\% | 33.3\% | 0.0\% | 33.3\% | 0.0\% | 0.0\% | 0.0\% | 100\% |

[^11]LCR - Zone 2 (Canyon Acres Drive to Laguna Canyon Arts and Design). This segment consists of one northbound lane, one southbound lane divided by a TWLTL.

Traffic accident data indicates 51 collisions occurred during this 60 -month period with 12 collisions in 2016, 7 collisions in 2017, 17 collisions in 2018, 8 collisions in 2019, and 7 collisions in 2020.

For primary collision factors of the 51 collisions, 30 (i.e., $59 \%$ ) of the accidents was speeding, 2 were under influence of alcohol, 1 was failure to yield, 6 were improper turn, 6 were other violations, 1 was other than driver, and 5 were unknown. Also, 26 (i.e., $51 \%$ ) of the collisions were classified as rear end type collision, 5 were head-on collision, 6 were sideswipe collisions, 3 were broadside, 6 were hit an object, 3 were overturn, and 2 were classified as others.

LCR - Zone 3 (Laguna Canyon Arts and Design to Stan Oaks Drive). This segment consists of one northbound lane, one southbound lane divided by a TWLTL.

Traffic accident data indicates 47 collisions occurred during this 60-month period with 13 collisions in 2016, 9 collisions in 2017, 11 collisions in 2018, 10 collisions in 2019, and 4 collisions in 2020.

For primary collision factors of the 47 collisions, 17 (i.e., $36 \%$ ) of the accidents was speeding, 10 (i.e., $21 \%$ ) were under influence of alcohol, 2 were following too close, 1 was failure to yield, 5 were improper turn, 10 (i.e., $21 \%$ ) were other violations, and 2 were other than driver. Also, 18 (i.e., $38 \%$ ) of the collisions were classified as rear end type collision, 6 were head-on collision, 5 were sideswipe collisions, 6 were broadside, 9 were hit an object, 1 was overturn, and 2 were auto-pedestrian collision.

LCR - Zone 4 (Stan Oaks Drive to Anneliese's School). This segment consists of one northbound lane, one southbound lane divided by a TWLTL.

Traffic accident data indicates 60 collisions occurred during this 60 -month period with 16 collisions in 2016, 8 collisions in 2017. 14 collisions in 2018, 14 collisions in 2019, and 8 collisions in 2020.

For primary collision factors of the 60 collisions, 33 (i.e., $55 \%$ ) of the accidents was speeding, 6 were under influence of alcohol, 3 were following too close, 3 were failure to yield, 7 were improper turn, 1 was other violations, 2 were other than driver, 5 were classified as unknown. 33 (i.e., $55 \%$ ) of the collisions were classified as rear end type collision, 4 were head-on collision, 5 were sideswipe collisions, 4 were broadside, 7 were hit an object, 4 were overturn, 1 was auto-pedestrian collision, and 2 were classified as others.

LCR - Zone 5 (Anneliese's School to El Toro Road). This segment consists of two northbound lanes, single northbound right turn lane, two southbound lanes and single southbound left turn lane.

Traffic accident data indicates 8 collisions occurred during this 60 -month period with 3 collisions in 2016, 0 collisions in 2017, 3 collisions in 2018, 0 collisions in 2019, and 2 collisions in 2020.

For primary collision factors of the 8 collisions, 3 (i.e., $37.5 \%$ ) of the accidents was speeding, 1 was failure to yield, 1 was improper turn, 1 was other violations, 1 was other than driver, and 1 was classified as unknown. Also, 2 of the collisions were classified as rear end type collision, 2 were sideswipe collisions, 1 was broadside, and 3 (i.e., $37.5 \%$ ) were hit an object.

### 3.4 Existing Deficiencies

The traffic demand for this corridor is expected to increase substantially in the near future. The existing poor operating conditions are expected to further worsen without any implementation of improvements.
This segment of LCR consists of a two-lane highway with 12-foot-wide travel lanes, a 10 -foot non-standard center TWLTL and limited on-street parking. Although no additional travel lanes are proposed with the project enhancing capacity, multimodal capacity of the corridor would improve due to the addition of bike, pedestrian and transit improvements.

Sidewalks or dedicated pedestrian paths do not exist along LCR within the project limits. The exception is a 0.2-mile-long sidewalk on the east side of LCR near the Laguna Beach Dog Park. Pedestrian access is limited to the paved shoulder next to the traffic lanes or in dirt areas adjacent to non-standard shoulders. A large number of bicyclists were observed during peak periods along the study corridor. Since this is a popular recreational route, it experiences high bike traffic on weekends and holidays. These bicyclists have limited access on fairly narrow, non-standard paved shoulders that are separated from traffic lanes only by a travel way edge stripe. The northbound LCR consists of residential and commercial land uses, many of which have direct driveway access to and from LCR. The southbound LCR includes several satellite parking lots. Vehicular congestion and queuing, and inadequate gaps during peak traffic periods create difficulty for left turning vehicles accessing these driveways and parking lots. This issue is compounded through the Big Bend area, where restricted sight distance through the horizontal curves can create difficulty for left turning vehicles to find adequate gaps for a safe left turn movement through the oncoming traffic stream.

The availability of public parking is highly constrained throughout the City. City transit and trolley services make a critical contribution in improving traffic circulation by removing additional motorists from utilizing the corridor, especially during the peak summer season. The Act V/City Maintenance Facility Yard parking lot located at the southern end of the project limits primarily serves as a park-and-ride location for the trolley service during summer months. Vehicular congestion and queuing in addition to the inadequate gaps during peak periods makes ingress and egress difficult for vehicles and the trolley service accessing this lot.

Overhead utilities exist along both sides of LCR through most of the corridor within the project limits. These overhead utility poles along the edge of the roadway in both directions are located within the clear recovery zone increasing the risk of collisions with errant vehicles.

## 4 Traffic Volume Forecasts

This chapter describes the assumptions and methodologies used to forecast traffic volumes at nine study intersections and driveways along LCR.

### 4.1 Traffic Forecasting Methodology and Assumptions

Future traffic forecasts at the study intersections and highway segments under the Opening Year (2030) and Horizon Year (2050) are developed using the assumptions contained in the Transportation Demand Forecasting (TDF) model OCTAM version 4.0. The Base Year (2012) and Future Year (2040) OCTAM models were used to calculate the annual growth volumes at the study facilities, which were applied to existing traffic counts using the difference method (Existing Counts + Model growth) or using the Furness method (using approach and departure growth to adjust intersection forecast) to generate 2050 and opening year volumes. The forecast volumes were balanced along the corridor to ensure conservation of flow. In average, the annual growth rate is approximately $2 \%$ for the year 2030 forecasts. The extrapolation growth rate is assumed to be $0.5 \%$ per year to develop the year 2050 forecasts. The $0.5 \%$ per year is based on the forecasted social and economic growth in the region.

A model post-processor was constructed to refine the "raw" model output link volumes. The post-processor was based on the methodologies delineated in the National Cooperative Highway Research Program Report (NCHRP) 255 published by the Transportation Research Board (TRB). The purpose of the post processor is to go beyond what can reasonably be achieved in terms of accuracy and detail from the OCTAM Regional Planning Model. Post-processing adjustments provide a greater level of consistency with available base year counts.

It should be noted that the vehicular forecast volumes for the No Build and Build alternatives are the same for Opening Year (2030) and Horizon Year (2050) since the traffic demands in the study area would not change between No Build and Build alternatives. Therefore, future forecast volumes between the scenarios would maintain consistency and potential benefits and impacts associated with each alternative can clearly be identified.

Traffic demand within this corridor already exceeds capacity during weekday AM and PM peak hours and during most summer weekends and holidays due to special events and the proximity to the Pacific Ocean as well as multiple adjacent recreational facilities and trails. A reversible lane alternative, Alternative 5, is being considered part of the overall corridor improvements evaluation in the PSR/PDS in order to handle the overcapacity traffic conditions. A technical memorandum on reversible lane operations concept memorandum, HDR, December 21, 2021, presents various aspects for Alternative 5 in detail. This technical memorandum is included in Appendix C. As described in the memorandum, reversible traffic lanes add peak-direction capacity to a two-way road and decrease congestion by borrowing available lane capacity from the other (off-peak) direction. Reversing lanes reduces congestion for handling special
event traffic, during morning and evening commutes, when an incident affects operation, or when construction or maintenance activity is present on the road. Roads that may be used as emergency evacuation routes or for special events also benefit from reversible lane strategies. Under the circumstance, peak season daily and corresponding peak hour traffic volumes were used to evaluate the traffic conditions for Alternative 5.

To develop the peak season traffic volume increase rate, the Caltrans Census counts on LCR between Canyon Acres Drive and El Toro Road were extracted from Caltrans website and evaluated. From year 1990 to 1996, the peak month ADT is about $18 \%$ to $19 \%$ higher than the average ADT for the off-peak months. But from year 1997 to 2018, the peak month ADT is about $11 \%$ to $12 \%$ higher than the average ADT for the off-peak months. The peak month ADT is about $1 \%$ higher for the years 2019 and 2020. On average between 1990 and 2020, the peak month ADT is assumed to be $12 \%$ higher than the average ADT for the off-peak months. The calculation worksheet is included in Appendix D.

To be consistent, the peak hour volumes along roadway segments and the through movement on LCR at the intersections are assumed to apply $12 \%$ increase.

Based on the existing peak hour directional flow, the reversible lane would be operational for southbound traffic during the AM peak period and northbound during the PM peak period. Hours of operations may occur between 7 am to 9 am during the AM peak period and 4 pm to 6 pm during the PM peak period. During off-peak periods, the reversible lane may operate as a TWLTL. With the center TWLTL reversible lane, left turn movements are prohibited between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits. The left turn traffic would proceed downstream until the end point intersection of the reversible lane to make a U-turn and then make the right turn onto the targeted access or driveway.
Based on the discussions in this section, the No Build and Build traffic volumes under Alternative 1 through Alternative 4 remain the same. The Alternative 5 traffic volumes are generally $12 \%$ higher than the Alternative 1 through 4 volumes.

### 4.2 Opening Year (2030) Traffic Volumes

Table 4-1 presents peak hour and daily volume forecast for study segments under Opening Year (2030) No Build and Build, Alternatives 1 to 4, conditions. Opening Year (2030) arterial segment volumes under Alternatives 1 to 4 are around $14 \%$ higher than the existing volumes. Table $4-2$ presents peak hour and daily volume forecast for study segments under Opening Year (2030) Build Alternative 5 conditions which is around $12 \%$ higher than the Alternatives 1 to 4 volumes as discussed in Section 4.1.

Table 4-3 and Table 4-5 present intersection volume forecast for the study intersections under Opening Year (2030) No Build and Build, Alternatives 1 to 4, conditions during AM and PM peak hours, respectively. Table 4-4 and Table 4-6 present intersection volume forecast for the study intersections under Opening Year (2030) Build Alternative 5 conditions during AM and PM peak hours, respectively.

Figure 4-1 presents intersection turning movement volumes under Opening Year (2030) No Build and Build, Alternatives 1 to 4, conditions. Figure 4-2 presents intersection turning movement volumes under Opening Year (2030) Build Alternative 5 conditions.

Table 4-1. Opening Year (2030) No Build and Build Arterial Segment Volumes Alternatives 1 to 4

| ID | Segment | Description | Direction | AM Peak Hour | PM <br> Peak <br> Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Laguna Canyon Rd/SR-133 | Btwn. El Toro Road \& Sun Valley Drive | Northbound | 1,310 | 1,920 | 44,600 |
|  |  |  | Southbound | 1,720 | 1,730 |  |
| 2 | Laguna Canyon Rd//SR-133 | Btwn. Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,300 | 1,960 | 45,100 |
|  |  |  | Southbound | 1,780 | 1,730 |  |
| 3 | Laguna Canyon <br> Rd//SR-133 | Btwn. Stan Oaks Drive \& LCAD Driveway | Northbound | 1,350 | 1,890 | 44,300 |
|  |  |  | Southbound | 1,770 | 1,790 |  |
| 4 | Laguna Canyon <br> Rd//SR-133 | Btwn. LCAD Driveway \& Canyon Acres Drive | Northbound | 1,370 | 1,890 | 44,800 |
|  |  |  | Southbound | 1,760 | 1,800 |  |

Table 4-2. Opening Year (2030) Build Arterial Segment Volumes - Alternative 5

| ID | Segment | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Laguna Canyon Rd/SR-133 | Btwn. El Toro Road \& Sun Valley Drive | Northbound | 1,470 | 2,150 | 50,000 |
|  |  |  | Southbound | 1,930 | 1,940 |  |
| 2 | Laguna Canyon Rd//SR-133 | Btwn. Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,460 | 2,200 | 50,500 |
|  |  |  | Southbound | 1,990 | 1,940 |  |
| 3 | Laguna Canyon Rd//SR-133 | Btwn. Stan Oaks Drive \& LCAD Driveway | Northbound | 1,510 | 2,120 | 49,600 |
|  |  |  | Southbound | 1,980 | 2,000 |  |
| 4 | Laguna Canyon <br> Rd//SR-133 | Btwn. LCAD Driveway \& Canyon Acres Drive | Northbound | 1,530 | 2,120 | 50,200 |
|  |  |  | Southbound | 1,970 | 2,020 |  |

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Table 4-3. 2030 No Build and Build AM Peak Hour Intersection Turning Movement Volumes - Alternatives 1 to 4

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 0 | 1045 | 711 | 28 | 1079 | 0 | 0 | 0 | 815 | 16 | 3694 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 1610 | 30 | 168 | 1726 | 0 | 0 | 0 | 20 | 146 | 3700 |
| 3 | SR-133 at Sun Valley Drive | 0 | 1444 | 1 | 2 | 1694 | 0 | 0 | 0 | 4 | 6 | 3151 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 1430 | 15 | 15 | 1683 | 0 | 0 | 0 | 10 | 15 | 3168 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 1439 | 1 | 2 | 1691 | 0 | 0 | 0 | 4 | 6 | 3143 |
| 6 | SR-133 at Castle Rock Road | 0 | 1432 | 2 | 3 | 1692 | 0 | 0 | 0 | 6 | 8 | 3143 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 52 | 1379 | 0 | 0 | 1656 | 42 | 55 | 45 | 0 | 0 | 3229 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 76 | 1351 | 0 | 0 | 1639 | 62 | 80 | 66 | 0 | 0 | 3274 |
| 9 | SR-133 at Canyon Acres Drive | 18 | 1555 | 15 | 16 | 1511 | 0 | 0 | 0 | 40 | 16 | 3171 |

Table 4-4. 2030 Build AM Peak Hour Intersection Turning Movement Volumes - Alternative 5

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at EI Toro Road | 76 | 1232 | 711 | 28 | 1208 | 0 | 0 | 0 | 815 | 16 | 4086 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 1873 | 30 | 168 | 1931 | 0 | 0 | 0 | 20 | 146 | 4168 |
| 3 | SR-133 at Sun Valley Drive | 0 | 1703 | 3 | 0 | 1901 | 0 | 0 | 0 | 0 | 10 | 3617 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 1681 | 30 | 0 | 1901 | 0 | 0 | 0 | 0 | 25 | 3637 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 1701 | 3 | 0 | 1901 | 0 | 0 | 0 | 0 | 10 | 3615 |
| 6 | SR-133 at Castle Rock Road | 0 | 1690 | 5 | 0 | 1901 | 0 | 0 | 0 | 0 | 14 | 3610 |
| 7 | SR-133 at Laguna College of Arts \& Design <br> Driveway | 0 | 1695 | 0 | 0 | 1807 | 94 | 0 | 100 | 0 | 0 | 3696 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility <br> Parking Lot Driveway | 76 | 1615 | 0 | 0 | 1845 | 62 | 80 | 66 | 0 | 0 | 3744 |
| 9 | SR-133 at Canyon Acres Drive | 18 | 1742 | 15 | 93 | 1640 | 0 | 0 | 0 | 40 | 16 | 3564 |

Table 4-5. 2030 No Build and Build PM Peak Hour Intersection Turning Movement Volumes - Alternatives 1 to 4

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 0 | 835 | 824 | 41 | 973 | 0 | 0 | 0 | 680 | 43 | 3396 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 1599 | 10 | 51 | 1602 | 0 | 0 | 0 | 11 | 60 | 3333 |
| 3 | SR-133 at Sun Valley Drive | 0 | 1644 | 6 | 2 | 1494 | 0 | 0 | 0 | 2 | 2 | 3150 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 1645 | 6 | 5 | 1491 | 0 | 0 | 0 | 5 | 5 | 3157 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 1649 | 6 | 2 | 1494 | 0 | 0 | 0 | 3 | 2 | 3156 |
| 6 | SR-133 at Castle Rock Road | 0 | 1652 | 8 | 3 | 1494 | 0 | 0 | 0 | 4 | 3 | 3164 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 4 | 1647 | 0 | 0 | 1488 | 10 | 13 | 19 | 0 | 0 | 3181 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 6 | 1632 | 0 | 0 | 1492 | 15 | 19 | 29 | 0 | 0 | 3193 |
| 9 | SR-133 at Canyon Acres Drive | 18 | 1473 | 30 | 20 | 1488 | 0 | 0 | 0 | 20 | 16 | 3065 |

Table 4-6. 2030 Build PM Peak Hour Intersection Turning Movement Volumes - Alternative 5

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 18 | 1012 | 824 | 41 | 1090 | 0 | 0 | 0 | 680 | 43 | 3708 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 1794 | 10 | 51 | 1737 | 0 | 0 | 0 | 11 | 60 | 3663 |
| 3 | SR-133 at Sun Valley Drive | 0 | 1837 | 8 | 0 | 1631 | 0 | 0 | 0 | 0 | 4 | 3480 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 1835 | 11 | 0 | 1631 | 0 | 0 | 0 | 0 | 10 | 3487 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 1841 | 8 | 0 | 1631 | 0 | 0 | 0 | 0 | 5 | 3485 |
| 6 | SR-133 at Castle Rock Road | 0 | 1842 | 11 | 0 | 1631 | 0 | 0 | 0 | 0 | 7 | 3491 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 0 | 1853 | 0 | 0 | 1617 | 14 | 0 | 32 | 0 | 0 | 3516 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 6 | 1834 | 0 | 0 | 1634 | 15 | 19 | 29 | 0 | 0 | 3537 |
| 9 | SR-133 at Canyon Acres Drive | 18 | 1650 | 30 | 45 | 1605 | 0 | 0 | 0 | 20 | 16 | 3384 |

Figure 4-1. Opening Year (2030) No Build and Build Intersection Peak Hour Volumes - Alternatives 1 to 4


Figure 4-2. Opening Year (2030) Build Intersection Peak Hour Volumes - Alternative 5


### 4.3 Horizon Year (2050) Traffic Volumes

Table 4-7 presents peak hour and daily volume forecast for study area highway segments under Horizon Year (2050) No Build and Build, Alternatives 1 to 4, conditions. Horizon Year (2050) arterial segment volumes under Alternatives 1 to 4 are around $50 \%$ higher than the existing volumes. Table 4-8 presents peak hour and daily volume forecast for Study Area highway segments under Horizon Year (2050) No Build and Build, Alternatives 1 to 4, conditions. Horizon Year (2050) arterial segment volumes under Alternative 5 are around 12\% higher than the Alternatives 1 to 4 volumes.

Table 4-9 and Table 4-11 present intersection volume forecast for the study intersections under Horizon Year (2050) No Build and Build, Alternatives 1 to 4, conditions during AM and PM peak hours, respectively. Table 4-10 and Table 4-12 present intersection volume forecast for the study intersections under Horizon Year (2050) Build Alternatives 5 conditions during AM and PM peak hours, respectively. Figure 4-3 presents intersection turning movement volumes under Horizon Year (2050) No Build and Build, Alternatives 1 to 4, conditions. Figure 4-4 presents intersection turning movement volumes under Horizon Year (2050) Build Alternative 5 conditions.

Table 4-7. Horizon Year (2050) No Build and Build Arterial Segment Volumes Alternatives 1 to 4

| ID | Segment | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Laguna Canyon <br> Rd//SR-133 | Btwn. El Toro Road \& Sun Valley Drive | Northbound | 1,680 | 2,625 | 54,800 |
|  |  |  | Southbound | 2,310 | 2,310 |  |
| 2 | Laguna Canyon Rd//SR-133 | Btwn. Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,680 | 2,730 | 55,900 |
|  |  |  | Southbound | 2,415 | 2,310 |  |
| 3 | Laguna Canyon Rd//SR-133 | Btwn. Stan Oaks Drive \& LCAD Driveway | Northbound | 1,785 | 2,625 | 54,800 |
|  |  |  | Southbound | 2,415 | 2,415 |  |
| 4 | Laguna Canyon <br> Rd//SR-133 | Btwn. LCAD Driveway \& Canyon Acres Drive | Northbound | 1,785 | 2,625 | 55,400 |
|  |  |  | Southbound | 2,415 | 2,415 |  |

Table 4-8. Horizon Year (2050) Build Arterial Segment Volumes - Alternative 5

| ID | Segment | Description | Direction | AM Peak Hour | PM Peak Hour | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Laguna Canyon Rd//SR-133 | Btwn. El Toro Road \& Sun Valley Drive | Northbound | 1,880 | 2,940 | 61,400 |
|  |  |  | Southbound | 2,590 | 2,590 |  |
| 2 | Laguna Canyon <br> Rd//SR-133 | Btwn. Sun Valley Drive \& Stan Oaks Drive | Northbound | 1,880 | 3,060 | 62,600 |
|  |  |  | Southbound | 2,700 | 2,590 |  |
| 3 | Laguna Canyon <br> Rd//SR-133 | Btwn. Stan Oaks Drive \& LCAD Driveway | Northbound | 2,000 | 2,940 | 61,400 |
|  |  |  | Southbound | 2,700 | 2,700 |  |
| 4 | Laguna Canyon <br> Rd//SR-133 | Btwn. LCAD Driveway \& Canyon Acres Drive | Northbound | 2,000 | 2,940 | 62,000 |
|  |  |  | Southbound | 2,700 | 2,700 |  |

Table 4-9. 2050 No Build and Build AM Peak Hour Intersection Turning Movement Volumes - Alternatives 1 to 4

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 0 | 1225 | 976 | 38 | 1334 | 0 | 0 | 0 | 1035 | 21 | 4629 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 2050 | 30 | 178 | 2191 | 0 | 0 | 0 | 20 | 151 | 4620 |
| 3 | SR-133 at Sun Valley Drive | 0 | 1784 | 1 | 2 | 2164 | 0 | 0 | 0 | 4 | 6 | 3961 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 1770 | 15 | 15 | 2153 | 0 | 0 | 0 | 10 | 15 | 3978 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 1779 | 1 | 2 | 2161 | 0 | 0 | 0 | 4 | 6 | 3953 |
| 6 | SR-133 at Castle Rock Road | 0 | 1772 | 2 | 3 | 2162 | 0 | 0 | 0 | 6 | 8 | 3953 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 52 | 1719 | 0 | 0 | 2126 | 42 | 55 | 45 | 0 | 0 | 4039 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 76 | 1691 | 0 | 0 | 2109 | 62 | 80 | 66 | 0 | 0 | 4084 |
| 9 | SR-133 at Canyon Acres Drive | 28 | 1895 | 15 | 21 | 1836 | 0 | 0 | 0 | 40 | 21 | 3856 |

Table 4-10. 2050 Build AM Peak Hour Intersection Turning Movement Volumes - Alternative 5

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 76 | 1452 | 976 | 38 | 1494 | 0 | 0 | 0 | 1035 | 21 | 5092 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 2353 | 30 | 178 | 2427 | 0 | 0 | 0 | 20 | 151 | 5159 |
| 3 | SR-133 at Sun Valley Drive | 0 | 2083 | 3 | 0 | 2402 | 0 | 0 | 0 | 0 | 10 | 4498 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 2061 | 30 | 0 | 2402 | 0 | 0 | 0 | 0 | 25 | 4518 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 2081 | 3 | 0 | 2402 | 0 | 0 | 0 | 0 | 10 | 4496 |
| 6 | SR-133 at Castle Rock Road | 0 | 2070 | 5 | 0 | 2402 | 0 | 0 | 0 | 0 | 14 | 4491 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 0 | 2075 | 0 | 0 | 2308 | 94 | 0 | 100 | 0 | 0 | 4577 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 76 | 1995 | 0 | 0 | 2346 | 62 | 80 | 66 | 0 | 0 | 4625 |
| 9 | SR-133 at Canyon Acres Drive | 28 | 2122 | 15 | 98 | 1996 | 0 | 0 | 0 | 40 | 21 | 4320 |

Table 4-11. 2050 No Build and Build PM Peak Hour Intersection Turning Movement Volumes - Alternatives 1 to 4

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 0 | 1095 | 999 | 46 | 1223 | 0 | 0 | 0 | 900 | 53 | 4316 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 2034 | 10 | 56 | 2067 | 0 | 0 | 0 | 16 | 60 | 4243 |
| 3 | SR-133 at Sun Valley Drive | 0 | 2084 | 6 | 2 | 1959 | 0 | 0 | 0 | 2 | 2 | 4055 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 2085 | 11 | 5 | 1956 | 0 | 0 | 0 | 5 | 5 | 4067 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 2094 | 6 | 2 | 1959 | 0 | 0 | 0 | 3 | 2 | 4066 |
| 6 | SR-133 at Castle Rock Road | 0 | 2097 | 8 | 3 | 1959 | 0 | 0 | 0 | 4 | 3 | 4074 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 4 | 2092 | 0 | 0 | 1953 | 10 | 13 | 19 | 0 | 0 | 4091 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 6 | 2077 | 0 | 0 | 1957 | 15 | 19 | 29 | 0 | 0 | 4103 |
| 9 | SR-133 at Canyon Acres Drive | 28 | 1843 | 30 | 20 | 1898 | 0 | 0 | 0 | 20 | 21 | 3860 |

Table 4-12. 2050 Build PM Peak Hour Intersection Turning Movement Volumes - Alternative 5

| ID | Description | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBR | WBL | WBR | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR-133 at El Toro Road | 18 | 1316 | 999 | 46 | 1370 | 0 | 0 | 0 | 900 | 53 | 4702 |
| 2 | SR-133 at Anneliese's School Driveway | 0 | 2273 | 10 | 56 | 2232 | 0 | 0 | 0 | 16 | 60 | 4647 |
| 3 | SR-133 at Sun Valley Drive | 0 | 2321 | 8 | 0 | 2126 | 0 | 0 | 0 | 0 | 4 | 4459 |
| 4 | SR-133 at Laguna Beach Dog Park Driveway | 0 | 2319 | 16 | 0 | 2126 | 0 | 0 | 0 | 0 | 10 | 4471 |
| 5 | SR-133 at Stan Oaks Drive | 0 | 2330 | 8 | 0 | 2126 | 0 | 0 | 0 | 0 | 5 | 4469 |
| 6 | SR-133 at Castle Rock Road | 0 | 2331 | 11 | 0 | 2126 | 0 | 0 | 0 | 0 | 7 | 4475 |
| 7 | SR-133 at Laguna College of Arts \& Design Driveway | 0 | 2342 | 0 | 0 | 2112 | 14 | 0 | 32 | 0 | 0 | 4500 |
| 8 | SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway | 6 | 2323 | 0 | 0 | 2129 | 15 | 19 | 29 | 0 | 0 | 4521 |
| 9 | SR-133 at Canyon Acres Drive | 28 | 2064 | 30 | 45 | 2045 | 0 | 0 | 0 | 20 | 21 | 4253 |

Figure 4-3. Horizon Year (2050) No Build and Build Intersection Peak Hour Volumes - Alternatives 1 to 4


Figure 4-4. Horizon Year (2050) Build Intersection Peak Hour Volumes - Alternative 5


## 5 Analysis Methodology

This section provides the methodology for the analysis of the existing, No Build and four (4) Build alternatives that include complete street elements such as bike, pedestrian facilities and transit services. As the Build alternatives do not provide additional lanes, the capacity enhancements provided by the proposed project are consistent from one alternative to another. Since traffic volumes do not change between No Build Alternative 1 and Build alternatives 2 to 4, the automobile LOS for highway segments is expected to remain the same for both No Build and Build alternatives 2 to 4 for Opening Year (2030) and Horizon Year (2050). However, the multimodal capacity of the corridor would improve due to the addition of bike, pedestrian and transit improvements. Therefore, the alternatives are evaluated in two ways: (1) the methodologies from Highway Capacity Manual (HCM) 2010 to analyze the level of service of the state highway facility as required by Caltrans policy including highway segments, and intersections and (2) the new multimodal LOS methodologies put forth by the recently released HCM 6 for bicycle, transit and pedestrians.

Standard evaluations for intersections, road segments and arterials are as valid for reversible lane system facilities as for any facility. The implementation of a reversal does not fundamentally change the expectations for roadway facilities. Therefore, the various methodologies, as described in the HCM, for example, are still valid for use by the City and Caltrans.

Based on the 2014 Transportation Concept Report for the SR-133 highway, the target concept level of service is LOS D for Year 2050. The concept LOS indicates the minimum level of service is LOS D that the District would allow on a route prior to proposing an alternative to improve operating conditions. However, based on the forecast 2050 traffic volumes, concurrence from Caltrans staff and Caltrans's approved methodology, the target level of service is LOS E.

### 5.1 Two-Lane Highways Level of Service Standards and Thresholds

The HCM 2010 Two-Lane Highway LOS methodology was used to assess the automobiles LOS performance along LCR. The HCM 2010 categorizes two-lane highways into three categories: Class I, II, and II. The LCR falls under Class I category. For Class I highways two measures of effectiveness below are used to determine automobile LOS:

- ATS (Average Travel Speed): Reflects mobility on a two-lane highway. It is defined as the highway segment length divided by the average travel time taken by vehicles to traverse it during a designated time interval.
- PTSF (Percent time spent following): Represents the freedom to maneuver and the comfort and convenience of travel. It is the average percentage of time that vehicles must travel in platoons behind slower vehicles due to the inability to pass.

Table 5-1 presents the automobile LOS criteria for Class I highways based on ATS and PTSF.

Table 5-1. Automobile LOS for Two-Lane Highways

| LOS | Percent time spent following (PTSF) | Average Travel Speed (MPH) | Description |
| :---: | :---: | :---: | :---: |
| A | <35.0 | >55.0 | Free-flow operations, motorists can travel at desired speed and passing demand is well below capacity |
| B | >35.0 and <50.0 | $>50.0$ and $<55.0$ | Stable flow, with speeds generally higher than 50 miles per hour. The passing demand to maintain desired speeds becomes significant |
| .C | >50.0 and < 80.0 | >45.0 and 50.0 | Stable flow at slower speeds. Individuals become noticeably affected by interactions with others, and percent time spent following drastically increases |
| D | >65.0 and <80.0 | $>40.0$ and $<45.0$ | Unstable flow with slower speeds and long platoons. Turning vehicles and roadside distractions cause major shock waves in the traffic stream. |
| E | >80.0 | $<40.0$ | Operating conditions at or near capacity. Speeds are slow and passing is virtually impossible. Platooning becomes intense. |
| F | N/A | N/A | Heavily congested flow. |

Source: 2010 Highway Capacity Manual, Chapter 15, Page 15-7. Exhibit 15-3

### 5.2 Multi-Lane Highways Level of Service Standards and Thresholds

The HCM 2010 Multi-Lane Highway LOS methodology was used to assess the automobiles LOS performance along LCR for the peak direction under Build Alternative 5 conditions. Because speeds are constant through a broad range of flow rates, LOS is defined on the basis of density, which is a measure of the proximity of vehicles to each other in the traffic stream. Table 5-2 summarizes the automobile LOS for multilane highway segments.

Table 5-2. Automobile LOS for Multilane Highway Segments

| LOS | FFS (mi/h) | Density $(\mathrm{pc} / \mathrm{mi} / \mathrm{ln})$ |
| :---: | :---: | :---: |
| A | All | $>0-11$ |
| B | All | $>11-18$ |
| C | All | $>18-26$ |
| D | All | $>26-35$ |
|  | 60 | $>35-40$ |
| E | 55 | $>35-41$ |
|  | 50 | $>35-43$ |


|  | Demand Exceeds Capacity |  |
| :--- | ---: | ---: |
|  |  |  |
| F | 60 | $>40$ |
|  | 55 | $>41$ |
|  | 50 | $>43$ |
|  | 45 |  |
|  |  |  |

Source: 2010 Highway Capacity Manual, Exhibit 14-4

### 5.3 Intersection Level of Service Standards and Thresholds

This section presents the methodologies used to perform peak hour intersection capacity analyses for signalized and unsignalized intersections.

### 5.3.1 Signalized Intersection Analysis

The analysis of signalized intersections utilized the operational analysis procedure as outlined in the HCM 2010. This method defines LOS in terms of delay, or more specifically, average stopped delay per vehicle. Delay is a measure of driver and/or passenger discomfort, frustration, fuel consumption and lost travel time. This technique uses 1,900 vehicles per hour per lane (VPHPL) as the maximum saturation volume of an intersection. This saturation volume was adjusted to account for lane width, on-street parking, pedestrians, traffic composition (i.e., percentage trucks) and shared lane movements (i.e., through and right-turn movements originating from the same lane). The LOS criteria used for this technique are described in Table 5-3.

Table 5-3. Signalized Intersection Level of Service

| Average Stopped <br> Delay Per Vehicle <br> (seconds) |  |
| :---: | :--- |
| <10.0 | LOS A describes operations with very low delay. This occurs when <br> progression is extremely favorable, and most vehicles do not stop at <br> all. Short cycle lengths may also contribute to low delay. |
| $10.1-20.0$ | LOS B describes operations with generally good progression and/or <br> short cycle lengths. More vehicles stop than for LOS A, causing higher <br> levels of average delay. |
| $20.1-35.0$ | LOS C describes operations with higher delays, which may result from <br> fair progression and/or longer cycle lengths. Individual cycle failures <br> may begin to appear at this level. The number of vehicles stopping is <br> significant at this level, although many still pass through the <br> intersection without stopping. |
| $35.1-55.0$ | LOS D describes operations with high delay, resulting from some <br> combination of unfavorable progression, long cycle lengths, or high <br> volumes. The influence of congestion becomes more noticeable, and <br> individual cycle failures are noticeable. |
| $55.1-80.0$ | LOS E is considered the limit of acceptable delay. Individual cycle <br> failures are frequent occurrences. |
| $>80.0$ | LOS F describes a condition of excessively high delay, considered <br> unacceptable to most drivers. This condition often occurs when arrival <br> flow rates exceed the LOS D capacity of the intersection. Poor <br> progression and long cycle lengths may also be major contributing <br> causes to such delay. |
| Source: Highway Capacity Manual 2010 |  |

### 5.3.2 Unsignalized Intersection Analysis

Unsignalized intersections, including two-way and all-way stop controlled intersections were analyzed using the HCM 2010 (Section 10) unsignalized intersection analysis methodology. The LOS for a two-way stop-controlled intersection is determined by the computed or measured control delay and is defined for each minor movement. Table 5-4 summarizes the LOS criteria utilized for unsignalized intersection analyses.

Table 5-4. Unsignalized Intersection Level of Service

| Average Control Delay (sec/veh) | LOS |
| :---: | :---: |
| $\leq 10$ | A |
| $>10$ and $\leq 15$ | B |
| $>15$ and $\leq 25$ | C |
| $>25$ and $\leq 35$ | D |
| $>35$ and $\leq 50$ | E |
| $>50$ | F |
| Source: Highway Capacity Manual 2010 |  |

### 5.4 Multimodal Level of Service Analysis

As previously mentioned, the methodologies put forth by HCM 6 were used to assess the LOS performance of bicycle, transit and pedestrian modes of transportation along LCR. Table 5-5 displays the LOS criteria and thresholds for bicycle, transit, and pedestrian facilities. Figure 5-1 displays the Integrated Multimodal Evaluation Framework underlying the methodology. The factors affecting the LOS of bicycle, transit, and pedestrian modes are:

- Bicycle LOS: Mainly affected by length of link between signalized intersections and number of access points the cyclist must cross along with level of comfort in traversing facility.
- Transit LOS: Based on number and spacing of transit stops and frequency of buses/hour or headway.
- Pedestrian LOS: Mainly affected by pedestrian traffic volume and speed. Also, conflicts with other modes and distance from vehicular traffic affects the LOS.
- Vehicle LOS: Mainly affected by length of link between signalized intersections and number of access points the motorist must travel along with level of comfort in traversing facility. The LOS is based on travel speed.

Table 5-5. Bicycle, Transit and Pedestrian LOS

| LOS | Los Score |
| :---: | :---: |
| A | $<=2.00$ |
| B | $>2.00-2.75$ |
| C | $>2.76-3.50$ |
| D | $>3.51-4.25$ |
| E | $>4.26-5.00$ |

Source: Mineta Transportation Institute (MTI)

Table 5-6 displays the inputs used to assess the LOS criteria for pedestrian facilities. LOS score is determined based on Pedestrian Exposure to Traffic at Signalized Intersections (PETSI) and modal conflicts. Table 5-7 shows the inputs used to assess the LOS criteria for Bicycle facilities. LOS score is determined based on Levels of Traffic Stress (LTS).

Table 5-6. Pedestrian Level of Service Inputs

| Segments | Intersections |
| :---: | :---: |
| Sidewalks and Parkway Widths | Crossing Width |
| Vehicle Volumes | Corner Radius |
| Vehicle Speeds | Potential Conflicts |
| Physical Separation | Visibility |
| - | Delay |
| Source: Mineta Transportation Institute (MTI) |  |

Table 5-7. Bicycle Level of Service Inputs

| Segments | Intersections |
| :---: | :---: |
| Facility Characteristics | Conflicts with turning vehicles |
| Street Width | Impediments/accommodations |
| Vehicle Speeds | Accessibility |
| Parking and Blockages | Parking Adjacent |
| - | Perceived Safety |
| Source: Mineta Transportation Institute (MTI) |  |

Figure 5-1. Multimodal Evaluation Framework

## Integrated Multimodal Evaluation Framework



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## 6 Traffic Engineering Performance Assessment Findings

This section discusses operational performance of study intersections and roadway segments along LCR under Existing, Opening Year (2030), and Horizon Year (2050).

### 6.1 Existing Year (2017) Conditions

This section presents the results of LOS analysis for study intersections and highway segments along LCR under existing conditions. The methodologies used to perform the analysis are previously described in Section 5.

### 6.1.1 Highway Analysis

Table 6-1 displays highway analysis results for segments along LCR under existing conditions. As shown, all the study segments currently operate at acceptable LOS E or better under existing conditions. HCM 2010 analysis worksheets are presented in Appendix E.

Table 6-1. Highway Analysis: Existing 2017 Conditions

| ID | Highway | From | To | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ATS (mph) / PTSF (\%) | LOS | ATS (mph) PTSF (\%) | LOS |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 28.9 / 88.9 | E | 26.0 / 94.5 | E |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 28.9 / 88.5 | E | 25.9 / 94.4 | E |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 29.0 / 88.4 | E | 26.1 / 93.9 | E |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 28.7 / 89.5 | E | 25.9 / 93.8 | E |

Laguna Canyon Road (Southbound)

| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | $28.7 / 92.9$ | E | $26.1 / 93.1$ | E |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | $28.6 / 93.6$ | E | $26.0 / 93.3$ | E |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | $28.8 / 93.2$ | E | $26.1 / 93.4$ | E |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $28.5 / 93.1$ | E | $26.0 / 93.6$ | E |

ATS = Average Travel Speed (miles per hour)
PTSF = Percent Time Spent Following
LOS = Level of Service

### 6.1.2 Intersection LOS Analysis

Table 6-2 displays intersection LOS and average vehicle delay results for study intersections under Existing Conditions. The LOS worksheets for the Existing Conditions analysis are presented in Appendix F. As shown in Table 6-2, all study area intersections currently operate at acceptable LOS of E or better under existing conditions, except the following which operate at LOS F:

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at Laguna College of Arts \& Design Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway, during AM and PM Peak Hours

Table 6-2. Intersection Analysis: Existing 2017 Conditions

| ID | Intersection | Existing Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 26.3 | C | 19.4 | B |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | >50 | F | 35.6 | E |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | 28.8 | D | 28.7 | D |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | 26.2 | D | 27.9 | D |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | 26.1 | D | 27.9 | D |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | 27.1 | D | 28.3 | D |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Stop-Controlled | 73.2 | F | 28.4 | D |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | >50 | F | >50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 3.8 | A | 3.3 | A |
| LOS = Level of Service <br> Intersection operation is expressed in average seconds of delay (sec/veh) for HCM methodology. <br> Bold: LOS F |  |  |  |  |  |  |

### 6.1.3 Intersection Control

Considering the high traffic volumes along LCR (SR-133) and inadequate Levels of Service at three of the study intersections, a preliminary peak hour warrant analysis was conducted. The results of warrant analysis indicated that three stop-controlled study intersections, listed below, meet the thresholds of peak hour warrant:

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at Laguna College of Arts \& Design Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway, during AM Peak Hour

It should be noted that the recommendation of a traffic signal at an intersection should not be merely based on peak hour warrant analysis. Satisfying the thresholds of peak hour warrant does however indicate the need for further warrant analysis. As described in Section 8, further warrant analysis such as the Eight-Hour and pedestrian volume warrants are required to be performed to have a better understanding of the need for a traffic signal at these intersections.

### 6.2 Opening Year (2030) Conditions

This section presents the results of LOS analysis for study intersections and roadway segments along LCR under Opening Year (2030) conditions. The methodologies used to perform the analysis are previously described in Section 5.

### 6.2.1 Highway Analysis

Table 6-3 and Table 6-4 display highway analysis results for segments along LCR under Opening Year (2030) No Build and Build conditions. The highway LOS worksheets are presented in Appendix G. As shown in Table 6-3 and Table 6-4, all the study area highway segments operate at LOS F under Opening Year (2030) No Build and Build, Alternatives 1 to 4, conditions. Under Build Alternative 5 conditions, southbound during AM peak and northbound during PM peak, the peak direction operate at LOS C with two-lane configuration utilizing the center reversible lane.

Table 6-3. Highway Analysis: Opening Year 2030 No Build and Build ConditionsAlternatives 1 to 4

| ID | Highway | From | To | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ATS (mph) / PTSF (\%) | LOS | ATS (mph) PTSF (\%) | LOS |
| Laguna Canyon Road (Northbound) |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 22.6 / 94.1 | F | 17.4 / 99.7 | F |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 22.2 / 94.1 | F | 17.0 / 100.0 | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 21.9/94.8 | F | 17.1 / 99.1 | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $21.8 / 94.9$ | F | 17.0 / 99.1 | F |
| Laguna Canyon Road (Southbound) |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 22.4 / 99.1 | F | 17.4 / 98.1 | F |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 22.0 / 99.9 | F | 17.1 / 98.2 | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 21.7 / 99.6 | F | 17.1 / 98.4 | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 21.5 / 99.5 | F | 17.0 / 98.4 | F |
| ATS = Average Travel Speed (miles per hour) PTSF = Percent Time Spent Following LOS = Level of Service, Bold = LOS F |  |  |  |  |  |  |  |

Table 6-4. Highway Analysis: Opening Year 2030 Build Conditions- Alternative 5

|  |  |  |  | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | Highway | From | To | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | LOS | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | LOS |

## Laguna Canyon Road (Northbound)

| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | $25.7 / 80.5$ | F | $50.0 / 23.6$ | C |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | $25.2 / 80.1$ | F | $50.0 / 24.1$ | C |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | $25.1 / 81.3$ | F | $50.0 / 23.3$ | C |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $25.1 / 81.6$ | F | $50.0 / 23.3$ | C |

Laguna Canyon Road (Southbound)

| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | $50.0 / 21.2$ | C | $21.9 / 88.3$ | F |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | $50.0 / 21.8$ | C | $21.4 / 88.2$ | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | $50.0 / 21.7$ | C | $21.9 / 89.1$ | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $50.0 / 22.2$ | C | $21.8 / 89.3$ | F |

### 6.2.2 Intersection LOS Analysis

### 6.2.2. Alternative 1 (No Build)

Under the No build alternative, the roadway network and lane configurations were assumed to remain the same as the existing conditions. Table 6-5 displays intersection LOS and average vehicle delay results for Study Area intersections under Opening Year (2030) No Build Conditions. The LOS worksheets for the Opening Year (2030) No Build Conditions analysis are presented in Appendix H. As shown in Table 6-5, all study area intersections operate at acceptable LOS of E or better under existing conditions, except the following which operate at LOS F.

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

Table 6-5. Intersection Analysis: Opening Year 2030 No Build Conditions

| ID | Intersection | Existing Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 34.6 | C | 23.2 | C |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | >50 | F | >50 | F |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | 44.0 | E | 49.1 | E |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | 45.6 | E | 47 | E |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | 43.6 | E | >50 | F |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | 45.9 | E | >50 | F |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Stop-Controlled | >50 | F | >50 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | >50 | F | >50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 4.5 | A | 3.9 | A |
| LOS = Level of Service <br> Intersection operation is expressed in average seconds of delay (sec/veh) for HCM methodology. <br> Bold: LOS F |  |  |  |  |  |  |

### 6.2.2.2 Alternatives 2, 3, 4 (Build)

Under Existing (2017) condition, the following three intersections met the peak hour warrant thresholds during AM peak hour:

- SR-133 at Anneliese's School Driveway
- SR-133 at Laguna College of Arts \& Design Driveway
- SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway

At the intersection of LCR with Anneliese's School driveway, the peak hour typically occurs before the school starts and after the school dismisses. Traffic entering and exiting Anneliese's School is expected to be minimal for the rest time periods. To avoid the interruption of the traffic flow along LCR, the intersection of SR-133 with Anneliese's School driveway remains stop-controlled intersection under the future build conditions. To reflect the worst-case scenario with low left turn movement volumes at this driveway, the driveway is analyzed with left turn movement allowed under Build Alternatives 2 to 4.

Installation of a traffic signal is not recommended at intersection of LCR with Act V/City Maintenance Yard Facility Parking Lot Driveway due to the close proximity to the Canyon Acres Road intersection located immediately to the south. Therefore, the intersection of LCR with Act V/City Maintenance Facility Yard Parking Lot Driveway was analyzed as a stop-controlled intersection under the future build conditions.

At the intersections of LCR with Laguna College of Arts \& Design driveway, traffic entering and exiting the driveway are expected to spread throughout the day. To provide adequate gaps for left turning traffic and safe access in and out of the driveway, the intersection was analyzed as signalized intersection under the future year Build Alternatives 2 to 4 conditions. This intersection was analyzed as a stopcontrolled intersection under the Build Alternative 5 with the worst-case peak season volumes. The existing signalized High-Intensity Activated Crosswalk Beacon (HAWK) is located 250 feet upstream of this intersection. Under Build Alternatives 2 to 4 conditions with the signalization at the intersection of LCR and Laguna College of Arts \& Design driveway, the HAWK signal is recommended to be removed and a pedestrian crossing walk at this signalized intersection is recommended to be added. Under Build Alternative 5, the HAWK signal is recommended to remain as is. Decisions on the signalization at the intersection of LCR with Laguna College of Arts \& Design driveway and removal of the HAWK signal is deferred to the PA/ED Phase for further evaluation.

The intersections at El Toro Road and Canyon Acres Drive would remain as a signalized intersection in all the Build scenarios.

Table 6-6 displays intersection LOS and average vehicle delay results for all study intersections under the Opening Year (2030) Build Alternatives 2 to 4 conditions. As shown, all study area intersections operate at acceptable LOS of E or better under Opening Year (2030) Build Alternatives 2 to 4 conditions, except the following which are expected to operate at LOS F.

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The LOS worksheets for the Opening Year (2030) Build Alternatives 2 to 4 analyses are presented in Appendix H .

Table 6-6. Intersection Analysis: Opening Year 2030 Build Conditions - Alternatives 1 to 4

| ID | Intersection | Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 34.6 | C | 23.2 | C |
| 2 | LCR/SR-133 at Anneliese's School Driveway | StopControlled | >50 | F | >50 | F |
| 3 | LCR/SR-133 at Sun Valley Drive | StopControlled | 44 | E | 49.1 | E |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | StopControlled | 45.6 | E | 47 | E |
| 5 | LCR/SR-133 at Stan Oaks Drive | StopControlled | 43.6 | E | >50 | F |
| 6 | LCR/SR-133 at Castle Rock Road | StopControlled | 45.9 | E | >50 | F |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Signalized* | >80 | F | 51 | D |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | StopControlled | >50 | F | >50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 4.5 | A | 3.9 | A |
| LOS <br> Inte <br> Bold <br> * Pr | Level of Service ection operation is expressed in average seconds of de LOS F <br> posed Traffic Control | (sec/veh) f | CM me | dolog |  |  |

### 6.2.2.3 Alternatives 5 (Build)

As discussed in Section 4.1, the reversible lane would be operational for southbound traffic during the AM peak period and northbound during the PM peak period. With the center TWLTL being a reversible lane during the peak hours, left turn movements are prohibited at all the intersections and driveways between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits. Therefore, the intersections of SR-133 with Laguna College of Arts \& Design driveway was analyzed as a stop-controlled intersection.

Table 6-7 displays intersection LOS and average vehicle delay results for all study intersections under the Opening Year (2030) Build Alternative 5 conditions. As shown, all study area intersections operate at acceptable LOS of E or better under Opening Year (2030) Build conditions, except the following which are expected to operate at LOS F.

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during PM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The LOS worksheets for the Opening Year (2030) Build Alternative 5 analysis are presented in Appendix H .

Table 6-7. Intersection Analysis: Opening Year 2030 Build Conditions - Alternative 5

| ID | Intersection | Existing Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 39.4 | D | 25.3 | C |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | >50 | F | 34.9 | D |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | 49.3 | E | 20.2 | C |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | 49.5 | E | 19.6 | C |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | 49.3 | E | 20.3 | C |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | >50 | E | 20.5 | C |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Stop-Controlled | 33.9 | D | >80 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | >50 | F | >50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 7.2 | A | 4.9 | A |
|  | evel of Service on operation is expressed in average seconds of delay S F | ec/veh) for HCM | thodolo |  |  |  |

### 6.2.3 Multimodal LOS Analysis

### 6.2.3.1 Alternative 1 (No Build)

Table 6-8 displays the results of multimodal analysis under the Opening Year (2030) Alternative 1 (No Build) conditions. As shown, transit and pedestrian modes operate at satisfactory LOS E or better, while vehicle and bicycle modes operate at LOS F.

Table 6-8. 2030 Alt 1 Multimodal LOS

| Mode | Score |  |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |
| Vehicle | 17 MPH | F |
| Transit | 4.5 | E |
| Bicycle | 5.5 | F |
| Pedestrian | 4.0 | D |
|  | Laguna Canyon Rd/SR-133 (Southbound) |  |
| Vehicle | 17 MPH | F |
| Transit | 4.5 | E |
| Bicycle | 5.5 | F |
| Pedestrian | 4.0 | D |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |

### 6.2.3.2 Alternative 2

Table 6-9 displays the results of multimodal analysis under the Opening Year (2030) Alternative 2 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-9. 2030 Alt 2 Multimodal LOS

| Mode | Score | LOS |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |
| Vehicle | 17 MPH | F |
| Transit | 2.6 | B |
| Bicycle | 1.0 | A |
| Pedestrian | 2.0 | A |
|  | Laguna Canyon Rd/SR-133 (Southbound) |  |
| Vehicle | 17 MPH | F |
| Transit | 2.3 | B |
| Bicycle | 1.0 | A |
| Pedestrian | N/A | N/A |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |

### 6.2.3.3 Alternative 3

Table 6-10 displays the results of multimodal analysis under the Opening Year (2030) Alternative 3 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-10. 2030 Alt 3 Multimodal LOS

| Mode | Score | LOS |
| :---: | :---: | :---: |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 17 MPH | F |
| Transit | 2.0 | A |
| Bicycle | 2.5 | B |
| Pedestrian | 1.5 | A |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |
| Vehicle | 17 MPH | F |
| Transit | 2.8 | C |
| Bicycle | 1.5 | A |
| Pedestrian | 1.5 | A |
| MPH: Miles per Hour - LOS = Level of Service - Bold: LOS F |  |  |

### 6.2.3.4 Alternative 4

Table 6-11 displays the results of multimodal analysis under the Opening Year (2030) Alternative 4 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-11. 2030 Alt 4 Multimodal LOS

| Mode | Score |  | LOS |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 17 MPH | F |  |
| Transit | 2.0 | A |  |
| Bicycle | 1.8 | A |  |
| Pedestrian | 1.5 | A |  |
|  | Laguna Canyon Rd/SR-133 (Southbound) |  |  |
| Vehicle | 17 MPH | F |  |
| Transit | 2.0 | A |  |
| Bicycle | 1.8 | A |  |
| Pedestrian | 1.5 | A |  |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |  |

### 6.2.3.5 Alternative 5

Table 6-12 displays the results of multimodal analysis under the Opening Year (2030) Alternative 5 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F for the off-peak direction which represents the worst-case scenario.

Table 6-12. 2030 Alt 5 Multimodal LOS

| Mode | Score | LOS |
| :--- | :---: | :---: | :---: |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 25.1 MPH | F |
| Transit | 2.2 | B |
| Bicycle | 2.0 | A |
| Pedestrian | 1.5 | A |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |
| Vehicle | 21.4 MPH | F |
| Transit | 2.2 | B |
| Bicycle | 2.0 | A |
| Pedestrian | 1.5 | A |
| MPH: Miles per Hour <br> LOS $=$ Level of Service <br> Bold: LOS F |  |  |

### 6.3 Horizon Year (2050) Conditions

This section presents the results of LOS analysis for study intersections and highway segments along LCR under Horizon Year (2050) conditions. The methodologies used to perform the analysis are previously described in Section 5.

### 6.3.1 Highway Analysis

Table 6-13 displays highway analysis results for segments along LCR under Horizon Year (2050) No Build and Build conditions. The highway LOS worksheets are presented in Appendix I. As shown in Table 6-13, all the study area highway segments operate at LOS F under Horizon Year (2050) No Build and Build, Alternatives 1 to 4, conditions. Under Build Alternative 5 conditions, the peak direction, southbound during AM peak and northbound during PM peak, operate at LOS D with two-lane lane configuration utilizing the center reversible lane.

Table 6-13. Highway Analysis: Horizon Year 2050 No Build and Build Conditions Alternatives 1 to 4

| ID | Highway | From | To | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ATS (mph) / PTSF (\%) | LOS | ATS (mph) PTSF (\%) | LOS |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 14.5 / 98.2 | F | 6.5 / 100 | F |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 13.6 / 98.3 | F | 5.6 / 100 | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 12.7 / 99.0 | F | 5.7 / 100 | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 12.7 / 99.0 | F | 5.7 / 100 | F |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 14.5 / 100 | F | 6.5 / 100 | F |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 13.6 / 100 | F | 5.7 / 100 | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 12.7 / 100 | F | 5.7 / 100 | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 12.5 / 100 | F | 5.7 / 100 | F |
| ```ATS = Average Travel Speed (miles per hour) PTSF = Percent Time Spent Following LOS = Level of Service Bold = LOS F``` |  |  |  |  |  |  |  |

Table 6-14. Highway Analysis: Horizon Year 2050 Build Conditions - Alternative 5

|  | Highway | From | To | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID |  |  |  | ATS (mph) PTSF (\%) or D (pc/mi/ln) | LOS | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | LOS |


| Laguna Canyon Rd/SR-133 (Northbound) |  |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | $18.4 / 86.7$ | F | $29.1 / 32.9$ | D |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | $17.5 / 86.5$ | F | $48.7 / 34.5$ | D |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | $17.0 / 88.3$ | F | $49.1 / 32.9$ | D |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $17.0 / 88.3$ | F | $49.1 / 32.9$ | D |

Laguna Canyon Rd/SR-133 (Southbound)

| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | $50.0 / 28.4$ | D | $12.4 / 94.5$ | F |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | $49.7 / 29.8$ | D | $11.4 / 94.4$ | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | $49.7 / 29.8$ | D | $12.0 / 96.9$ | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | $49.7 / 29.8$ | D | $12.0 / 96.9$ | F |

ATS = Average Travel Speed (miles per hour); LOS = Level of Service
PTSF = Percent Time Spent Following; D = Density
Bold = LOS F

* Density was applied to the southbound during the PM peak and northbound during the AM peak


### 6.3.2 Intersection LOS Analysis

### 6.3.2.1 Alternative 1 (No Build)

Under the No build alternative, the roadway network and lane configurations were assumed to remain the same as the Existing conditions. Table 6-15 displays intersection LOS and average vehicle delay results for Study Area intersections under Horizon Year (2050) Conditions. The LOS worksheets for the Horizon Year (2050) No build analysis are presented in Appendix J. As shown, study area intersections operate at acceptable LOS of E or better under Horizon Year (2050) No Build conditions, except the following which operate at LOS F during AM and PM peak hours:

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Sun Valley Drive, during AM and PM Peak Hours
- SR-133 at Laguna Beach Dog Park Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during AM and PM Peak Hours
- SR-133 at Castle Rock Road, during AM and PM Peak Hours
- SR-133 at Laguna College of Arts and Design Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway, during AM and PM Peak Hours

Table 6-15. Intersection Analysis: Horizon Year 2050 No Build Conditions

| ID | Intersection | Existing Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 67.3 | E | 43.5 | D |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | > 50 | F | >50 | F |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | >50 | F | $>50$ | F |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | >50 | F | >50 | F |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | >50 | F | >50 | F |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | >50 | F | >50 | F |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Stop-Controlled | >50 | F | >50 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | > 50 | F | > 50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 5.5 | A | 4.9 | A |
|  | LOS = Level of Service; Bold: LOS F |  |  |  |  |  |

### 6.3.2.2 Alternatives 2, 3, 4 (Build)

Table 6-16 displays intersection LOS and average vehicle delay results for all study intersections under the Horizon Year (2050) Build Alternatives 2 to 4 conditions. Intersection control assumptions for Horizon Year (2050) Build Alternatives 2 to 4 conditions remain the same as Opening Year (2030) Build Alternatives 2 to 4 conditions as described in Section 6.2.2.2. As shown, all study area intersections operate at LOS F under Horizon Year (2050) Build Alternatives 2 to 4 conditions during the AM and PM peak hours except the intersection of SR-133/El Toro Road which operates at LOS E and LOS D during the AM and the PM peak hour respectively and the intersection at Canyon Acres Drive which operates at LOS A during the AM and PM peak hours. The LOS worksheets for the Horizon Year (2050) Build Alternative analysis are presented in Appendix J.

Table 6-16. Intersection Analysis: Horizon Year 2050 Build Conditions - Alternatives 1 to 4

| ID | Intersection | Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 67.3 | E | 43.5 | D |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | > 50 | F | >50 | F |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | >50 | F | >50 | F |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | >50 | F | >50 | F |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | >50 | F | >50 | F |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | >50 | F | >50 | F |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Signalized* | >80 | F | >80 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | > 50 | F | > 50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 5.5 | A | 4.9 | A |
| LOS = Level of Service <br> Intersection operation is expressed in average seconds of delay (sec/veh) for HCM methodology. <br> Bold: LOS F <br> * Proposed Traffic Control |  |  |  |  |  |  |

### 6.3.2.3 Alternatives 5 (Build)

Table 6-17 displays intersection LOS and average vehicle delay results for all study intersections under the Horizon Year (2050) Build Alternative 5 conditions. Intersection control assumptions for Horizon Year (2050) Build Alternative 5 conditions remain the same as Opening Year (2030) Build Alternative 5 conditions as described in Section
6.2.2.2. As shown, all study area intersections operate at acceptable LOS of E or better under Horizon Year (2050) Build Alternative 5 conditions, except the following intersections which are expected to operate at LOS F.

- SR-133 at El Toro Road, during AM Peak Hour
- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Sun Valley Drive, during AM Peak Hour
- SR-133 at Laguna Beach Dog Park Driveway, during AM Peak Hour
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The LOS worksheets for the Horizon Year (2050) Build Alternative 5 analysis are presented in Appendix J.

Table 6-17. Intersection Analysis: Horizon Year 2050 Build Conditions - Alternative 5

| ID | Intersection | Traffic Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | >80 | F | 53.4 | D |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Stop-Controlled | > 50 | F | >50 | F |
| 3 | LCR/SR-133 at Sun Valley Drive | Stop-Controlled | >50 | F | 28 | D |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Stop-Controlled | >50 | F | 27 | D |
| 5 | LCR/SR-133 at Stan Oaks Drive | Stop-Controlled | >50 | F | 28.4 | D |
| 6 | LCR/SR-133 at Castle Rock Road | Stop-Controlled | >50 | F | 28.8 | D |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Stop-Controlled | >50 | F | >50 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Stop-Controlled | > 50 | F | > 50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 4.5 | A | 3.9 | A |
| LOS = Level of Service; Bold: LOS F; <br> Intersection operation is expressed in |  |  |  |  |  |  |

### 6.3.3 Multimodal LOS Analysis

### 6.3.3.1 Alternative 1 (No Build)

Table 6-18 displays the results of multimodal analysis under the Horizon Year (2050) Alternative 1 (No Build) conditions. As shown, transit and pedestrian modes operate at satisfactory LOS E or better, while vehicle and bicycle modes operate at LOS F.

Table 6-18. 2050 Alt 1 Multimodal LOS

| Mode | Score | LOS |
| :--- | :---: | :---: | :---: |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 5.6 MPH | F |
| Transit | 4.5 | E |
| Bicycle | 5.5 | F |
| Pedestrian | 4.0 | D |
|  | Laguna Canyon Rd/SR-133 (Southbound) |  |
| Vehicle | 5.6 MPH | F |
| Transit | 4.5 | E |
| Bicycle | 5.5 | F |
| Pedestrian | 4.0 | D |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |

### 6.3.3.2 Alternative 2

Table 6-19 displays the results of multimodal analysis under the Horizon Year (2050) Alternative 2 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-19. 2050 Alt 2 Multimodal LOS

| Mode | Score | LOS |  |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.6 | B |  |
| Bicycle | 1.0 | A |  |
| Pedestrian | 2.0 | A |  |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.3 | B |  |
| Bicycle | 1.0 | A |  |
| Pedestrian | N/A | N/A |  |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |  |

### 6.3.3.3 Alternative 3

Table 6-20 displays the results of multimodal analysis under the Horizon Year (2050) Alternative 3 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-20. 2050 Alt 3 Multimodal LOS

| Mode | Score |  | LOS |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.0 | A |  |
| Bicycle | 2.5 | B |  |
| Pedestrian | 1.5 | A |  |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.8 | C |  |
| Bicycle | 1.5 | A |  |
| Pedestrian | 1.5 | A |  |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |  |

### 6.3.3.4 Alternative 4

Table 6-21 displays the results of multimodal analysis under the Horizon Year (2050) Alternative 4 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F.

Table 6-21. 2050 Alt 4 Multimodal LOS

| Mode | Score | LOS |  |
| :--- | :---: | :---: | :---: |
|  | Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.0 | A |  |
| Bicycle | 1.8 | A |  |
| Pedestrian | 1.5 | A |  |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |
| Vehicle | 5.6 MPH | F |  |
| Transit | 2.0 | A |  |
| Bicycle | 1.8 | A |  |
| Pedestrian | 1.5 | A |  |
| MPH: Miles per Hour - LOS $=$ Level of Service - Bold: LOS F |  |  |  |

### 6.3.3.5 Alternative 5

Table 6-22 displays the results of multimodal analysis under the Horizon Year (2050) Alternative 5 conditions. As shown, transit, pedestrian, and bicycle modes operate at satisfactory LOS E or better, while vehicle mode operates at LOS F for the off-peak direction which represents the worst-case scenario.

Table 6-22. 2050 Alt 5 Multimodal LOS

| Mode | Score | LOS |
| :---: | :---: | :---: |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |
| Vehicle | 17 MPH | F |
| Transit | 2.2 | B |
| Bicycle | 2.0 | A |
| Pedestrian | 1.5 | A |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |
| Vehicle | 11 MPH | F |
| Transit | 2.2 | B |
| Bicycle | 2.0 | A |
| Pedestrian | 1.5 | A |
| MPH: Miles per Hour - LOS = Level of Service - Bold: LOS F |  |  |

### 6.4 Intersection Control Evaluation

The Intersection Control Evaluation (ICE) Review process is a fairly recent requirement for state highway modifications. This task requires that the Caltrans Design Coordinator, Design Reviewer, the Headquarter Traffic Liaison, and the FHWA Transportation Engineer (where applicable) review and approve the analysis of each interchange concept and provide input on the preferred traffic control configuration. The goal of this process is to make the decision to implement the most efficient intersection control system or strategy at each location along the state right of way. It is also meant to consider innovative traffic control measures such as roundabouts, single point urban interchanges, diverging diamond interchanges and other measures that reduce the number of signalized intersections being implemented. There also is an increased emphasis on pedestrian and bike access and safety.

The evaluation provided in this Traffic Engineering Performance Assessment report follows the latest Caltrans Intersection Control Evaluation (ICE) Process Informational Guide which follows a two-step process that includes a screening assessment (PSR) followed by design and analysis (PA/ED). The TEPA analysis addressed performance with respect to safety, mobility, and cost for a reasonable range of practical configuration and control alternatives. This process received input from the City regarding traffic control at various locations and the recommendations for several of the intersections ultimately developed along the state highway. Between 2014 and 2015, the City convened a SR-133/Laguna Canyon Road Task Force to review the

Assessment Report, conduct additional public outreach, and conduct technical studies to consider the corridor's issues and needs, and evaluate alternative improvement concepts. The City task force alternatives analysis and the most recent alternative screening was used as a starting point to identify the intersection control treatments. Finally, recommendations for two intersections were developed based on the analysis that would apply under any of the four Build Alternatives.
The intersection at Laguna College of Arts and Design Driveway is analyzed as a signalized intersection based on the Caltrans ICE Process Informational Guide and preliminary traffic signal warrants analysis under Build Alternatives 2 to 4 . With the signalization, it is recommended to remove the existing HAWK signal and add a pedestrian crossing across at the newly signalized intersection. Under Build Alternative 5, the intersection is analyzed as a right-in and right out access due to the reversible lane concept and the HAWK signal is recommended to remain as is. Decisions on the signalization at the intersection of LCR with Laguna College of Arts \& Design driveway and removal of the HAWK signal is deferred to the PA/ED Phase for further evaluation.

The intersection at Act V/City Maintenance Yard Facility Parking Lot Driveway meets the thresholds of peak hour signal warrant. Although the intersection was warranted for a traffic signal during the AM peak hour, a traffic signal is not recommended at this location due to the close proximity to the Canyon Acres Road intersection located immediately to the south. Furthermore, the intersection at the Act V Parking Lot Driveway was also considered for a roundabout. A roundabout at this location was determined to be unfeasible due to right-of-way constraints and operationally deficient per the high traffic volumes traversing LCR in contrast to the very low traffic volumes entering and existing the Lot in addition to potential vehicle queuing impacts from the Canyon Acres Road intersection. Therefore, this intersection is recommended to be maintained as a stop-controlled intersection.

## 7 Summary and Conclusion

This section summarizes the analysis results and findings presented in previous sections of this report. The analysis was performed for roadway segments and intersections within the study area under Existing (2017), Opening Year (2030) and Horizon Year (2050) No Build and Build conditions. The purpose of this analysis was to identify existing operational deficiencies and assess different alternatives and its traffic impacts.

### 7.1 Existing Conditions

Under Existing conditions all study area highway segments along LCR operate at satisfactory LOS E during both AM and PM peak hours.

The intersection capacity analysis under Existing conditions indicates that most study intersections operate at satisfactory LOS E or better. However, three intersections operate at LOS F.

The three intersections, which operate at LOS F are unsignalized intersections. The three intersections are warranted for a traffic signal based on the peak hour traffic warrant analysis but would require further warrant analysis. All three intersections that operate at LOS F and that are warranted for a traffic signal are listed below.

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway, during AM and PM Peak Hours


### 7.2 Opening Year (2030) Conditions

Under Opening Year conditions all study area highway segments along LCR operate at LOS F during both AM and PM peak hours. These results were expected given the traffic congestion under existing conditions.

The intersection capacity analysis under Opening Year (2030) No Build indicates that the study intersections operate at LOS E or better with the exception of the following intersections.

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The intersection capacity analysis under Opening Year (2030) Build Alternatives 2 to 4 indicates that the study intersections operate at LOS E or better with the exception of the following intersections.

- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

One more intersection was analyzed as signalized intersection in Opening Year (2030) Build Alternatives 2 to 4 scenarios:

- SR-133 at Laguna College of Arts and Design Driveway

The intersection capacity analysis under Opening Year (2030) Build Alternative 5 indicates that the study intersections operate at LOS E or better with the exception of the following intersections. Due to the reversible lane concept, the unsignalized intersections between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits including Laguna College of Arts and Design Driveway are analyzed as right-in and right-out accesses under Build Alternative 5.

- SR-133 at Anneliese's School Driveway, during AM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during PM Peak Hour
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The multimodal analysis results show improvement in pedestrian, transit and bicycle LOS for all Build alternatives as compared to the No Build due to the addition of bike, pedestrian and transit improvements along the corridor. The LOS results for each of the Build alternatives are similar and no alternative provides a significant advantage over the others. The vehicular LOS remains LOS F for Build Alternatives 2 to 4 since no addition of capacity was proposed for these alternatives. Under Build Alternative 5 conditions, the vehicular LOS are LOS F and C for the off-peak and peak direction, respectively. The peak direction vehicular LOS would improve resulting from the twolane configuration with the reversible lane conversion.

### 7.3 Horizon Year (2050) Conditions

Under Horizon Year conditions all study area highway segments along LCR operate at LOS F during both AM and PM peak hours. These results were expected given the traffic congestion under existing conditions.

The intersection capacity analysis under Horizon Year (2050) No Build indicates that most study intersections operate at LOS F. All the intersections operating at LOS F are unsignalized intersections.
One more intersection was analyzed as signalized intersection in Horizon Year (2050) Build Alternatives 2 to 4 scenarios:

- SR-133 at Laguna College of Arts and Design Driveway

The intersection analyzed with signal installation would operate at LOS F during the AM and PM peak hours. All the unsignalized intersections operate at LOS F during both peak periods.

The intersection capacity analysis under Horizon Year (2050) Build Alternative 5 indicates that the study intersections operate at LOS E or better with the exception of the following intersections. Similar to the Opening Year (2030) conditions, the unsignalized intersections between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits including Laguna College of Arts and Design Driveway are analyzed as right-in and right-out accesses under Build Alternative 5.

- SR-133 at El Toro Road, during AM Peak Hour
- SR-133 at Anneliese's School Driveway, during AM and PM Peak Hours
- SR-133 at Sun Valley Drive, during AM Peak Hour
- SR-133 at Laguna Beach Dog Park Driveway, during AM Peak Hour
- SR-133 at Stan Oaks Drive, during PM Peak Hour
- SR-133 at Castle Rock Road, during PM Peak Hour
- SR-133 at Laguna College of Arts and Design Driveway, during AM and PM Peak Hours
- SR-133 at Act V/City Maintenance Yard Facility Parking Lot Driveway, during AM and PM Peak Hours

The multimodal analysis results show improvement in pedestrian, transit and bicycle LOS for all Build alternatives as compared to the No Build due to the addition of bike, pedestrian and transit improvements along the corridor. The LOS results for each of the Build alternatives are similar and no alternative provides a significant advantage over the others. The vehicular LOS remains LOS F for Build Alternatives 2 to 4 since no addition of capacity was proposed for these alternatives. Under Build Alternative 5 conditions, the vehicular LOS are LOS F and D for the off-peak and peak direction, respectively. The peak direction vehicular LOS would improve resulting from the twolane configuration with the reversible lane conversion.

### 7.4 Comparative Analysis of Alternatives

The No Build and Build, Alternatives 1 to 4, provide one vehicular travel lane in each direction along LCR, thereby adding no capacity compared to existing conditions.

Therefore, vehicular traffic demand was forecast to be the same for No Build and Build, Alternatives 1 to 4, conditions. The No Build and Build, Alternatives 1 to 4, differ only from one another in number, classification, and configuration of pedestrian, bicycle, and transit facilities they provide. Alternative 5 was proposed to focus on the peak season with the worst-case traffic volumes. As mentioned in previous section, the peak direction configurations are proposed to have two lanes during the peak hours using the reversible lane concept. Table 7-1 compares the results of the highway analysis under 2030 and 2050 all scenarios. As shown in the table, the corridor operations for the peak direction under Build Alternative 5 would improve significantly with the reversible lane conversion.

Table 7-2 and Table 7-3 compare years 2030 and 2050 intersection analysis, respectively. As shown in the tables, the intersections service levels would improve at several stop-controlled intersections with the right-in and right-out configuration during the PM peak hour. The traffic operations at the Laguna College of Arts \& Design Driveway intersection are expected to improve during the AM and PM peak hours under Build Alternatives 2 to 4 and Build Alternative 5 conditions, respectively.

The multimodal analysis results were compared to evaluate the different alternatives. Table 7-4 compares the results of the multimodal analysis for Alternatives 1, 2, 3, 4, and 5 under Opening Year (2030) and Horizon Year (2050) conditions. The LOS results for each of the Build alternatives are similar and no alternative provides a significant advantage over the others.

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Table 7-1. 2030 and 2050 No Build and Build Highway Analysis Comparison

| ID | Highway | From | To | 2030 No Build/Build Alternatives 1-4 |  |  |  | 2030 Build Alternative 5 |  |  |  | 2050 No Build/Build Alternatives 1-4 |  |  |  | 2050 Build Alternative 5 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
|  |  |  |  | ATS (mph) / PTSF (\%) | LOS | $\begin{aligned} & \text { ATS (mph) / } \\ & \text { PTSF (\%) } \end{aligned}$ | LOS | ATS (mph) / PTSF (\%) or D (pc/mi/ln) ${ }^{\text { }}$ | LOS | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | LOS | ATS (mph) / PTSF (\%) | Los | ATS (mph) PTSF (\%) | LOS | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | Los | ATS (mph) / PTSF (\%) or D (pc/mi/ln)* | Los |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 22.6 / 94.1 | F | 17.4/99.7 | F | 25.7 / 80.5 | F | $50.0 / 23.6$ | c | 14.5/98.2 | F | $6.5 / 100$ | F | 18.4 / 86.7 | F | 29.1 / 32.9 | D |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 22.2 / 94.1 | F | 17.0/100.0 | F | 25.2 / 80.1 | F | 50.0 / 24.1 | c | 13.6/98.3 | F | $5.6 / 100$ | F | 17.5 / 86.5 | F | 48.7 / 34.5 | D |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 21.9/94.8 | F | 17.1 / 99.1 | F | 25.1 / 81.3 | F | $50.0 / 23.3$ | c | 12.7/99.0 | F | $5.7 / 100$ | F | $17.0 / 88.3$ | F | 49.1 / 32.9 | D |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 21.8/94.9 | F | 17.0 / 99.1 | F | 25.1 / 81.6 | $F$ | $50.0 / 23.3$ | c | 12.7/99.0 | F | $5.7 / 100$ | F | 17.0 / 88.3 | F | 49.1 / 32.9 | D |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | LCR/SR-133 | El Toro Road | Sun Valley Drive | 22.4 / 99.1 | F | 17.4/98.1 | F | 50.0 / 21.2 | c | 21.9/88.3 | F | 14.5 / 100 | F | $6.5 / 100$ | F | 50.0 / 28.4 | D | 12.4 / 94.5 | F |
| 2 | LCR/SR-133 | Sun Valley Drive | Stan Oaks Drive | 22.0 / 99.9 | F | 17.1 / 98.2 | F | 50.0 / 21.8 | c | 21.4 / 88.2 | F | 13.6 / 100 | F | 5.7 / 100 | F | 49.7 / 29.8 | D | 11.4/94.4 | F |
| 3 | LCR/SR-133 | Stan Oaks Drive | LCAD Driveway | 21.7/99.6 | F | 17.1/98.4 | F | $50.0 / 21.7$ | c | 21.9/89.1 | F | 12.7 / 100 | F | $5.7 / 100$ | F | 49.7 / 29.8 | D | 12.0/96.9 | F |
| 4 | LCR/SR-133 | LCAD Driveway | Canyon Acres Drive | 21.5/99.5 | F | 17.0 / 98.4 | F | 50.0 / 22.2 | c | 21.8 / 89.3 | F | 12.5 / 100 | F | $5.7 / 100$ | F | 49.7 / 29.8 | D | 12.0 / 96.9 | F |

ATS = Average Travel Speed (miles per hour); PTSF = Percent Time Spent Following; D = Density; LOS = Level of Service; Bold = LOS F

* Density was applied to the southbound results during the PM peak and northbound results during the AM peak

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Table 7-2. 2030 No Build and Build Intersection Analysis Comparison

| Int. \# | Intersection | Existing Traffic Control | 2030 No Build |  |  |  | 2030 Build Alternatives 2-4 |  |  |  | 2030 Build Alternative 5 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
|  |  |  | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1 | LCR/SR-133 at El Toro Road | Signalized | 34.6 | c | 23.2 | c | 34.6 | C | 23.2 | C | 39.4 | D | 25.3 | C |
| 2 | LCR/SR-133 at Anneliese's School Driveway | Minor Street Stop Controlled | >50 | F | >50 | F | >50 | F | >50 | F | >50 | F | 34.9 | D |
| 3 | LCR/SR-133 at Sun Valley Drive | Minor Street Stop Controlled | 44 | E | 49.1 | E | 44 | E | 49.1 | E | 49.3 | E | 20.2 | C |
| 4 | LCR/SR-133 at Laguna Beach Dog Park Driveway | Minor Street Stop Controlled | 45.6 | E | 47 | E | 45.6 | E | 47 | E | 49.5 | E | 19.6 | c |
| 5 | LCR/SR-133 at Stan Oaks Drive | Minor Street Stop Controlled | 43.6 | E | >50 | F | 43.6 | E | >50 | F | 49.3 | E | 20.3 | c |
| 6 | LCR/SR-133 at Castle Rock Road | Minor Street Stop Controlled | 45.9 | E | >50 | F | 45.9 | E | >50 | F | >50 | E | 20.5 | c |
| 7 | LCR/SR-133 at Laguna College of Arts \& Design Driveway | Minor Street Stop Controlled/Signalized* | >50 | F | >50 | F | >80 | F | 51 | D | 33.9 | D | >80 | F |
| 8 | LCR/SR-133 at Act V/City Maintenance Facility Yard Parking Lot Driveway | Minor Street Stop Controlled | >50 | F | >50 | F | >50 | F | >50 | F | >50 | F | >50 | F |
| 9 | LCR/SR-133 at Canyon Acres Drive | Signalized | 4.5 | A | 3.9 | A | 4.5 | A | 3.9 | A | 7.2 | A | 4.9 | A |

LOS = Level of Service
Intersection operation is expressed in average seconds of delay (del/veh) for HCM methodology.

* Minor Street Stop Controlled intersection under No Build and Build Alternative 5; Signalized intersection under Build Alternatives 2 to 4

Table 7-3. 2050 No Build and Build Intersection Analysis Comparison


LOS = Level of Service
Intersection operation is expressed in average seconds of delay (del/veh) for HCM methodology.

* Minor Street Stop Controlled intersection under No Build and Build Alternative 5; Signalized intersection under Build Alternatives 2 to 4

Table 7-4. 2030 and 2050 Build Multimodal Analysis Comparison

| Mode | Alternative 1 (No Build) |  | Alternative 2 |  | Alternative 3 |  | Alternative 4 |  | Alternative 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Score | LOS | Score | LOS | Score | LOS | Score | LOS | Score | LOS |
| Laguna Canyon Rd/SR-133 (Northbound) |  |  |  |  |  |  |  |  |  |  |
| Transit | 4.5 | E | 2.6 | B | 2.0 | A | 2.0 | A | 2.2 | B |
| Bicycle | 5.5 | F | 1.0 | A | 2.5 | B | 1.8 | A | 2.0 | A |
| Pedestrian | 4 | D | 2.0 | A | 1.5 | A | 1.5 | A | 1.5 | A |
| Laguna Canyon Rd/SR-133 (Southbound) |  |  |  |  |  |  |  |  |  |  |
| Transit | 4.5 | E | 2.3 | B | 2.8 | C | 2.0 | A | 2.2 | B |
| Bicycle | 5.5 | F | 1.0 | A | 1.5 | A | 1.8 | A | 2.0 | A |
| Pedestrian | 4 | D | N/A | N/A | 1.5 | A | 1.5 | A | 1.5 | A |

As evident above in Table 7-4, the LOS performance for Transit, Bicycle, and Pedestrian modes improves for all four Build alternatives compared to the No Build alternative.

### 7.5 Key Findings and Conclusions

The study intersections and roadway segments along the LCR operate at satisfactory LOS in the existing conditions with the exception of intersections at Anneliese's School Driveway, Laguna College of Arts and Design Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway. Due to heavy traffic during the period of weekdays, summer weekends and holidays, several operational constraints such as vehicular queuing, inadequate gaps for left turning traffic from driveways, conflicts between vehicles and pedestrian and bicycles due to inadequate bike lanes and sidewalks are observed along the corridor. The proposed alternatives accommodate innovative safety improvements and improvements for active and transit transportation modes for improving the safety and circulation for all modes of transportation. In the proposed Build alternatives, the constraints related to pedestrians, bicycles and transit are addressed. There is a significant improvement in multimodal LOS along the corridor for all the proposed Build alternatives in the Year 2050. The corridor is expected to be safer for pedestrians, and bicycles under the proposed alternatives due to reduction in conflicts with vehicles.

For Alternatives 1 to 4, since none of the alternatives have proposed any addition in number of lanes, there was no significant improvement in vehicular operations along the corridor. All the unsignalized intersections and roadway segments operate at LOS F during the Year 2050 No Build and Build, Alternatives 1 to 4, conditions. One of the key vehicular safety issues along the corridor is the lack of traffic breaks for left turning vehicles in and out of driveways. Therefore, signalization of intersections is recommended at the stop-controlled locations with high turning volumes as roundabouts were infeasible. The signalization of intersections would result in formation of vehicle platoons which would increase traffic breaks along the corridor
resulting in safer conditions for left turning vehicles in and out of the driveways. Based on preliminary peak hour warrant analysis, three unsignalized study intersections meet the thresholds of the peak hour signal warrant. However, only one of those intersections is analyzed as signalized intersections as explained earlier in Section 6.2 .2 and Section 6.4 under Build Alternatives 2 to 4 . This signalized intersection would continue to operate at LOS F in the Year 2050 conditions. However, it would contribute to enhance safety for left turning vehicles in and out of driveway along the corridor. The signalized intersection is listed below:

- SR-133 at Laguna College of Arts \& Design Driveway

For Alternative 5, the peak direction is proposed to have two lanes. Left turn at the two-way stop-controlled intersections/driveways are prohibited between Anneliese's School Driveway and Act V/City Maintenance Facility Yard Parking Lot Driveway within the project limits. The driveways have right-in and right-out accesses, which include the intersection at Laguna College of Arts \& Design Driveway. The peak direction vehicular operations along the corridor have significant improvements during the directional peak hours. The intersection service levels have significant improvements at several intersections during the PM peak hours.

The proposed Build alternatives are a combination of complete streets improvements, and safety enhancements which would serve the future multimodal user needs of the corridor.

## 8 Scope of Future Traffic Engineering Studies

The Traffic Engineering Performance Assessment (TEPA) report provided the details of the existing deficiencies along the Laguna Canyon Road (LCR) (SR-133) corridor. The possible alternatives were discussed and analyzed to determine the operational feasibility of each alternative. TEPA document is generally used to estimate the scope and magnitude of the Project Approval and Environmental Document (PA\&ED) phase. The detailed operational analysis is required as part of the PA\&ED phase.

### 8.1 Study Intersections and Data Collection

As part of the future detailed traffic operational analysis, it is recommended that the intersection LCR at Willow Canyon Road/Willow Staging Area be included in the analysis to assess and address potential operational and safety concerns that Caltrans has been receiving from the public. The data collection efforts are required to be conducted during the seasonal peak period (summer) on a typical weekday (Tuesday, Wednesday, or Thursday) and weekend to document the peak seasonal recreational traffic conditions along the corridor. Peak period turning movement counts are recommended to be collected at all study intersections (including its minor streets) along with pedestrian and bicycle counts. Additionally, arterial counts must be collected over a 24 -hour period for all study segments along LCR and minor streets of all study intersections.

### 8.2 Signal Warrant Analysis

A full set of traffic warrant analysis (Warrants 1-9) is required to be considered as per the latest version of California Manual on Uniform Traffic Control Devices (CA MUTCD), Chapter 4C. The warrant analysis needs to be conducted using the actual counts data. The analysis for all the applicable warrants should be conducted to justify the need for a traffic signal at intersections.

### 8.3 Accident Analysis

Any future study must obtain accident data from Caltrans' Traffic Accident and Surveillance Analysis Systems (TASAS) for the latest 36-month period. The accident analysis must be performed and compiled similar to Section 3.3 of this study.

### 8.4 Forecasting

As part of the detailed operational analysis, the future traffic volume forecasts at the study intersections and highway segments for the future year conditions should be developed using the assumptions contained in the latest version of Transportation Demand Forecasting (TDF) model OCTAM. The existing counts, base year and future year OCTAM models should be used to calculate the annual growth at the study facilities, which should be applied to existing traffic counts using the difference method
(Existing Counts + Model growth) or using the Furness method (using approach and departure growth to adjust intersection forecast) to generate the future year volumes.

The future model output link volumes should be converted to the future year peak hour turning movement volumes by post-processing. The post-processing shall be based on the methodologies delineated in the National Cooperative Highway Research Program Report (NCHRP) 255 published by the Transportation Research Board (TRB). The purpose of the post-processing is to go beyond what can reasonably be achieved in terms of accuracy and detail from the OCTAM Regional Planning Model. Post-processing adjustments provide a greater level of consistency with available base year counts.

The forecasting years for analysis of the project include:

- Opening Year
- Horizon Year (2050 or later)


### 8.5 Operational/Capacity Analysis and Evaluation

The future year peak hour turn volumes and the ADT link volumes obtained from the volume forecasting would be used for the operational analysis at study intersections and roadway segments respectively. The operational and capacity analysis should be conducted for all the future No Build and Build scenarios to estimate the level of operational improvements along the corridor with recommended improvements. All the alternatives should be analyzed with the future volumes to determine the feasibility and operational performance of each alternative. The proposed alternatives along the LCR corridor included improvements for alternative transportation modes for improving the safety and circulation for all modes of transportation. Therefore, it is recommended to evaluate the operations of all study intersections and roadway segments using the Multimodal Level of Service based on the methodology in the latest Highway Capacity Manual (HCM). The LOS standards for the operational analysis should be LOS E for all the study intersections and roadway segments unless alternative direction is provided by the governing jurisdictions.

### 8.6 Safety Analysis and Evaluation

Safety is a key concern for the City along the LCR corridor. A traffic safety analysis should be completed as part of the study to evaluate the existing safety concerns along the corridor. A safety analysis for all the proposed alternatives would help determine the most feasible alternative improvement for the corridor.

## Appendix A. Traffic Counts

National Data \& Surveying ServicesIntersection Turning Movement Count

National Data \& Surveying ServicesIntersection Turning Movement Count

| Location: SR-133 \& Canyon Acres Dr <br> City: Laguna Beach <br> Control: Signalized |  |  |  |  |  |  |  |  |  |  |  |  |  | ject ID: Date: | $\begin{aligned} & 7-01254-0 \\ & 1 / 30 / 2017 \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bikes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NS/ EW Streets: | SR-133 |  |  |  | SR-133 |  |  |  | Canyon Acres Dr |  |  |  | Canyon Acres Dr |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 1$N L$ |  | 1 | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | $\begin{aligned} & 1 \\ & \mathrm{SL} \\ & \hline \end{aligned}$ | $\begin{gathered} 2 \\ \mathrm{ST} \end{gathered}$ | 0 |  | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | 0 0 |  | $\begin{gathered} 1 \\ \text { WL } \end{gathered}$ | 0$W T$ | 1WR | WU | TOTAL |
|  |  |  | NR |  |  |  | SR | SU |  |  | ER | EU |  |  |  |  |  |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 7:00 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:15 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:45 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 11 | 1 | 0 | 1 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 27 |
| APPROACH \% 's : | 0.00\% | 91.67\% | 8.33\% | 0.00\% | 7.14\% | 92.86\% | 0.00\% | 0.00\% |  |  |  |  | 100.00\% | 0.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : |  | 7:45 AM - | 8:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 1 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| PEAK HR FACTOR : | 0.000 | 0.250 | 0.250 | 0.000 | 0.000 | 0.750 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.625 |
|  |  | 0.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | NORTH | OUND |  |  | SOUT | OUND |  |  | EAS | UND |  |  | WEST | OUND |  |  |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 4:15 PM | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 6 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 15 |
| APPROACH \% 's : | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 12.50\% | 87.50\% | 0.00\% | 0.00\% |  |  |  |  | 100.00\% | 0.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : |  | 04:30 PM - | 5:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| PEAK HR FACTOR : | 0.00 | 0.250 | 0.000 | 0.000 | 0.000 | 0.625 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |
|  |  | 0.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.500 |

National Data \& Surveying ServicesIntersection Turning Movement Count
Location: SR-133 \& Canyon Acres Dr City: Laguna Beach

Date:
Pedestrians (Crosswalks)

| NS/ EW Streets: | SR-133 |  | SR-133 |  | Canyon Acres Dr |  | Canyon Acres Dr |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 3 |
| 8:30 AM | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| TOTAL VOLUMES : APPROACH \% 's : | $\begin{gathered} \hline \mathrm{EB} \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { WB } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { EB } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { WB } \\ 0 \end{gathered}$ | $\begin{gathered} \hline N B \\ 5 \\ 45.45 \% \end{gathered}$ | $\begin{gathered} \hline \text { SB } \\ 6 \\ 54.55 \% \end{gathered}$ | $\begin{gathered} \hline \mathrm{NB} \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { SB } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { TOTAL } \\ 11 \end{gathered}$ |
| PEAK HR : | 07:45 | 45 AM | 0 | 0 | $\begin{gathered} 4 \\ 0.500 \end{gathered}$ |  | 0 | 0 | TOTAL |
| PEAK HR VOL: PEAK HR FACTOR : | 0 | 0 |  |  |  | $\begin{gathered} 3 \\ 0.375 \end{gathered}$ |  |  | $\begin{gathered} 7 \\ 0.583 \end{gathered}$ |



## SR-133 \& Canyon Acres Dr

## Peak Hour Turning Movement Count

ID: 17-01254-001
City: Laguna Beach


Total Vehicles (Noon)


Total Vehicles (PM)


| SR-133 |
| :---: |
| SOUTHBOUND |

Day: Thursday
Date: 11/30/2017


Bikes (NOON)


Bikes (PM)


National Data \& Surveying ServicesIntersection Turning Movement Count


## National Data \& Surveying ServicesIntersection Turning Movement Count

| Location: SR-133 \& Laguna Dog Park intersection <br> City: Laguna Beach <br> Control: No Control |  |  |  |  |  |  |  |  |  |  |  |  |  | ject ID Date | $\begin{aligned} & 7-01254 \\ & 1 / 30 / 201 \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bikes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NS/ EW Streets: | SR-133 |  |  |  | SR-133 |  |  |  | Laguna Dog Park intersection |  |  |  | Laguna Dog Park intersection |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
|  | $\begin{gathered} 0 \\ \mathrm{NL} \end{gathered}$ |  | 1 | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | $\begin{aligned} & 1 \\ & \mathrm{SL} \end{aligned}$ | $\begin{aligned} & 1 \\ & \mathrm{ST} \end{aligned}$ | 00 |  | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 0 \\ E T \end{gathered}$ | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | 1$W T$ | 0 | WU |  |
|  |  |  | NR |  |  |  | SR | SU |  |  |  |  |  |  | WR |  |  |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:30 AM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:45 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 8 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| APPROACH \% 's : | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |  |  |  |  |  |  |  |  |
| PEAK HR : |  | 8:00 AM - | 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| PEAK HR FACTOR : | 0.000 | 0.500 | 0.000 | 0.000 | 0.000 | 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |
|  |  | 0.5 |  |  |  | 0.5 |  |  |  |  |  |  |  |  |  |  | 0.500 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | NORTH | OUND |  |  | SOUTH | OUND |  |  | EAS | UND |  |  | WES | OUND |  |  |
| PM | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 4:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 4:45 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 6:15 PM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 5 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| APPROACH \% 's : | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 33.33\% | 66.67\% | 0.00\% | 0.00\% |  |  |  |  |  |  |  |  |  |
| PEAK HR : |  | 4:30 PM - | 5:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| PEAK HR FACTOR : | 0.00 | 0.500 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |
|  |  | 0.5 |  |  |  | 0.2 |  |  |  |  |  |  |  |  |  |  | 0.375 |

National Data \& Surveying ServicesIntersection Turning Movement Count
Location: SR-133 \& Laguna Dog Park intersection Project ID: 17-01254-002 City: Laguna Beach

Date: 11/30/2017
Pedestrians (Crosswalks)

| NS/ EW Streets: | SR-133 |  | SR-133 |  | Laguna Dog Park intersection |  | Laguna Dog Park intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 4 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES: APPROACH \% 's: | EB | WB | EB | WB | NB |  | NB | SB | TOTAL |
|  | 0 | 0 | 0 | 0 | $\begin{gathered} 3 \\ 3 \\ 50.00 \% \end{gathered}$ | $\begin{gathered} 0 \\ 3 \\ 50.00 \% \end{gathered}$ | 0 | 0 | 6 |
| PEAK HR : | 08:00 AM - 09:00 AM |  | 0 | 0 | $\begin{gathered} 3 \\ 0.250 \end{gathered}$ |  | 0 | 0 | TOTAL |
| PEAK HR VOL: | 0 | 0 |  |  |  | 2 |  |  | 5 |
| PEAK HR FACTOR : |  |  |  |  |  | $0.500$ |  |  | 0.313 |


| PM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 2 | ${ }^{6}$ | 0 | 0 | 8 |
| APPROACH \% 's : |  |  |  |  | 25.00\% | 75.00\% |  |  |  |
| PEAK HR : | 04:30 | :30 PM |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 |
| PEAK HR FACTOR : |  |  |  |  | 0.250 | 0.500 |  |  | 0.750 |

SR-133 \& Laguna Dog Park intersection
Peak Hour Turning Movement Count

ID: 17-01254-002
City: Laguna Beach


Total Vehicles (Noon)


Total Vehicles (PM)


SR-133
SOUTHBOUND

Day: Thursday
Date: 11/30/2017

National Data \& Surveying ServicesIntersection Turning Movement Count


## National Data \& Surveying ServicesIntersection Turning Movement Count



# National Data \& Surveying ServicesIntersection Turning Movement Count <br> Location: SR-133 \& El Toro Rd and The Anneliese School Entrance Project ID: 18-01018-001 

 City: Laguna BeachDate: $1 / 25 / 2018$


| PM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH \%'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 04:45 | :45 PM |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## SR-133 \& E1 Toro Rd and The Anneliese School Entrance

Peak Hour Turning Movement Count


National Data \& Surveying ServicesIntersection Turning Movement Count


National Data \& Surveying ServicesIntersection Turning Movement Count


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 0 | NU | 1SL | $\stackrel{1}{\text { ST }}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |  |
|  | NL | NT | NR |  |  |  | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU |  |
| 4:00 PM | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 4:45 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES: APPROACH \%'s | NL | NT | NR | NU | SL | ST | SR | SU | EL | $\begin{gathered} \hline \mathrm{ET} \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \mathrm{EU} \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { WT } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WU } \\ 0 \end{gathered}$ | $\begin{gathered} \hline \text { TOTAL } \\ 16 \end{gathered}$ |
|  | 0 | 10 | 0 | 0 | 0 | 6 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |
|  | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |  |  |  |  |  |  |  |  |
| PEAK HR : | 04:30 PM - 05:30 PM |  |  |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 3 \\ 0.375 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 5 | 0 | 0 |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| PEAK HR FACTOR : | 0.00 | 0.625 | 0.000 | $0.000$ |  |  |  |  |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |
|  |  | 0.625 |  |  |  |  | 0.375 |  |  |  |  |  |  |  |  |  | 0.500 |

# National Data \& Surveying ServicesIntersection Turning Movement Count <br> Location: SR-133 \& Anneliese School Entrance $\quad$ Project ID: 18-01018-002 

 City: Laguna BeachDate: $1 / 25 / 2018$
Pedestrians (Crosswalks)

| NS/EW Streets: | SR-133 |  | SR-133 |  | Anneliese School Entrance |  | Anneliese School Entrance |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : <br> APPROACH \%'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 08:00 | 00 AM | 0 | 0 | 0 | 0 | 0 | 0 | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 |  |  |  |  |  |  | 0 |


| PM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH \%'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 04:30 | 30 PM |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL: PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

SR-133 \& Anneliese School Entrance
Peak Hour Turning Movement Count

ID: 18-01018-002
City: Laguna Beach

| $\begin{aligned} & \infty \\ & \stackrel{n}{3} \\ & \text { 혿 } \\ & \frac{x}{4} \\ & \underset{\alpha}{2} \end{aligned}$ | 08:00 AM - 09:00 AM |
| :---: | :---: |
|  | NONE |
|  | 04:30 PM - 05:30 PM |



Day: Thursday
Date: 01/25/2018

| AM | 0 | 1383 | 165 | 0 | 1435 | AM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOON | 0 | 0 | 0 | 0 | 0 | NOON |
|  | PM | 0 | 1257 | 49 | 0 | 1338 |$\quad$ PM $\quad 0$

06:00 AM - 09:00 AM
NONE

04:00 PM - 07:00 PM


## Prepared by NDS/ATD

VOLUME
SR 133 \& Vicinity of the ACT V Parking Lot
Day: Thursday
City: Laguna Beach
Date: 11/30/2017
Project \#: CA17_1253_001

| DAILY TOTALS |  |  |  |  |  | $\frac{\mathrm{NB}}{17,469}$ | SB |  | EB |  | WB |  |  |  | Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 17,668 |  | 0 |  | 0 |  |  |  |  | 137 |
| AM Period | NB |  | SB |  | EB | WB | TOTAL |  | PM Period | NB |  | SB | EB | WB | TOTAL |  |
| 00:00 | 0 |  | 39 |  |  |  | 39 |  | 12:00 | 337 |  | 286 |  |  | 623 |  |
| 00:15 | 3 |  | 33 |  |  |  | 36 |  | 12:15 | 282 |  | 267 |  |  | 549 |  |
| 00:30 | 24 |  | 28 |  |  |  | 52 |  | 12:30 | 299 |  | 249 |  |  | 548 |  |
| 00:45 | 17 | 44 | 13 | 113 |  |  | 30 | 157 | 12:45 | 287 | 1205 | 257 | 1059 |  | 544 | 2264 |
| 01:00 | 25 |  | 12 |  |  |  | 37 |  | 13:00 | 294 |  | 286 |  |  | 580 |  |
| 01:15 | 11 |  | 8 |  |  |  | 19 |  | 13:15 | 288 |  | 261 |  |  | 549 |  |
| 01:30 | 18 |  | 7 |  |  |  | 25 |  | 13:30 | 280 |  | 278 |  |  | 558 |  |
| 01:45 | 13 | 67 | 9 | 36 |  |  | 22 | 103 | 13:45 | 314 | 1176 | 257 | 1082 |  | 571 | 2258 |
| 02:00 | 6 |  | 5 |  |  |  | 11 |  | 14:00 | 325 |  | 253 |  |  | 578 |  |
| 02:15 | 8 |  | 2 |  |  |  | 10 |  | 14:15 | 311 |  | 277 |  |  | 588 |  |
| 02:30 | 9 |  | 3 |  |  |  | 12 |  | 14:30 | 327 |  | 321 |  |  | 648 |  |
| 02:45 | 3 | 26 | 6 | 16 |  |  | 9 | 42 | 14:45 | 350 | 1313 | 296 | 1147 |  | 646 | 2460 |
| 03:00 | 4 |  | 11 |  |  |  | 15 |  | 15:00 | 316 |  | 255 |  |  | 571 |  |
| 03:15 | 6 |  | 6 |  |  |  | 12 |  | 15:15 | 338 |  | 257 |  |  | 595 |  |
| 03:30 | 9 |  | 9 |  |  |  | 18 |  | 15:30 | 291 |  | 284 |  |  | 575 |  |
| 03:45 | 7 | 26 | 18 | 44 |  |  | 25 | 70 | 15:45 | 283 | 1228 | 305 | 1101 |  | 588 | 2329 |
| 04:00 | 7 |  | 12 |  |  |  | 19 |  | 16:00 | 324 |  | 317 |  |  | 641 |  |
| 04:15 | 10 |  | 17 |  |  |  | 27 |  | 16:15 | 301 |  | 305 |  |  | 606 |  |
| 04:30 | 18 |  | 26 |  |  |  | 44 |  | 16:30 | 320 |  | 335 |  |  | 655 |  |
| 04:45 | 21 | 56 | 43 | 98 |  |  | 64 | 154 | 16:45 | 308 | 1253 | 274 | 1231 |  | 582 | 2484 |
| 05:00 | 36 |  | 38 |  |  |  | 74 |  | 17:00 | 303 |  | 283 |  |  | 586 |  |
| 05:15 | 56 |  | 48 |  |  |  | 104 |  | 17:15 | 346 |  | 295 |  |  | 641 |  |
| 05:30 | 68 |  | 66 |  |  |  | 134 |  | 17:30 | 318 |  | 263 |  |  | 581 |  |
| 05:45 | 81 | 241 | 95 | 247 |  |  | 176 | 488 | 17:45 | 289 | 1256 | 285 | 1126 |  | 574 | 2382 |
| 06:00 | 75 |  | 107 |  |  |  | 182 |  | 18:00 | 239 |  | 292 |  |  | 531 |  |
| 06:15 | 97 |  | 159 |  |  |  | 256 |  | 18:15 | 203 |  | 247 |  |  | 450 |  |
| 06:30 | 176 |  | 213 |  |  |  | 389 |  | 18:30 | 210 |  | 287 |  |  | 497 |  |
| 06:45 | 224 | 572 | 304 | 783 |  |  | 528 | 1355 | 18:45 | 175 | 827 | 261 | 1087 |  | 436 | 1914 |
| 07:00 | 218 |  | 348 |  |  |  | 566 |  | 19:00 | 194 |  | 230 |  |  | 424 |  |
| 07:15 | 240 |  | 344 |  |  |  | 584 |  | 19:15 | 156 |  | 203 |  |  | 359 |  |
| 07:30 | 323 |  | 353 |  |  |  | 676 |  | 19:30 | 165 |  | 179 |  |  | 344 |  |
| 07:45 | 307 | 1088 | 337 | 1382 |  |  | 644 | 2470 | 19:45 | 165 | 680 | 179 | 791 |  | 344 | 1471 |
| 08:00 | 324 |  | 296 |  |  |  | 620 |  | 20:00 | 149 |  | 157 |  |  | 306 |  |
| 08:15 | 322 |  | 317 |  |  |  | 639 |  | 20:15 | 152 |  | 147 |  |  | 299 |  |
| 08:30 | 340 |  | 304 |  |  |  | 644 |  | 20:30 | 126 |  | 141 |  |  | 267 |  |
| 08:45 | 336 | 1322 | 305 | 1222 |  |  | 641 | 2544 | 20:45 | 111 | 538 | 143 | 588 |  | 254 | 1126 |
| 09:00 | 329 |  | 346 |  |  |  | 675 |  | 21:00 | 146 |  | 126 |  |  | 272 |  |
| 09:15 | 266 |  | 340 |  |  |  | 606 |  | 21:15 | 168 |  | 121 |  |  | 289 |  |
| 09:30 | 330 |  | 346 |  |  |  | 676 |  | 21:30 | 132 |  | 130 |  |  | 262 |  |
| 09:45 | 258 | 1183 | 299 | 1331 |  |  | 557 | 2514 | 21:45 | 136 | 582 | 100 | 477 |  | 236 | 1059 |
| 10:00 | 281 |  | 248 |  |  |  | 529 |  | 22:00 | 118 |  | 92 |  |  | 210 |  |
| 10:15 | 241 |  | 281 |  |  |  | 522 |  | 22:15 | 112 |  | 89 |  |  | 201 |  |
| 10:30 | 272 |  | 242 |  |  |  | 514 |  | 22:30 | 111 |  | 95 |  |  | 206 |  |
| 10:45 | 292 | 1086 | 265 | 1036 |  |  | 557 | 2122 | 22:45 | 84 | 425 | 62 | 338 |  | 146 | 763 |
| 11:00 | 235 |  | 292 |  |  |  | 527 |  | 23:00 | 74 |  | 66 |  |  | 140 |  |
| 11:15 | 247 |  | 293 |  |  |  | 540 |  | 23:15 | 58 |  | 47 |  |  | 105 |  |
| 11:30 | 264 |  | 280 |  |  |  | 544 |  | 23:30 | 62 |  | 42 |  |  | 104 |  |
| 11:45 | 297 | 1043 | 280 | 1145 |  |  | 577 | 2188 | 23:45 | 38 | 232 | 33 | 188 |  | 71 | 420 |
| TOTALS |  | 6754 |  | 7453 |  |  |  | 14207 | TOTALS |  | 10715 |  | 10215 |  |  | 20930 |
| SPLIT \% |  | 47.5\% |  | 52.5\% |  |  |  | 40.4\% | SPLIT \% |  | 51.2\% |  | 48.8\% |  |  | 59.6\% |
|  | DAILY TOTALS |  |  |  |  | NB SB |  |  | EB |  | WB |  |  |  |  | tal |
|  |  |  |  |  |  | 17,469 | 17,668 |  | 0 |  | 0 |  |  |  | 35,137 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour |  | 08:15 |  | 07:00 |  |  |  | 08:15 | PM Peak Hour |  | 14:30 |  | 15:45 |  |  | 15:45 |
| AM Pk Volume |  | 1327 |  | 1382 |  |  |  | 2599 | PM Pk Volume |  | 1331 |  | 1262 |  |  | 2490 |
| Pk Hr Factor |  | 0.976 |  | 0.979 |  |  |  | 0.963 | Pk Hr Factor |  | 0.951 |  | 0.942 |  |  | 0.950 |
| 7-9 Volume |  | 2410 |  | 2604 |  |  |  | 5014 | 4-6 Volume |  | 2509 |  | 2357 |  |  | 4866 |
| 7-9 Peak Hour |  | 08:00 |  | 07:00 |  |  |  | 07:30 | 4-6 Peak Hour |  | 16:30 |  | 16:00 |  |  | 16:00 |
| 7-9 Pk Volume |  | 1322 |  | 1382 |  |  |  | 2579 | 4-6 Pk Volume |  | 1277 |  | 1231 |  |  | 2484 |
| Pk Hr Factor |  | 0.972 |  | 0.979 |  |  |  | 0.954 | Pk Hr Factor |  | 0.923 |  | 0.919 |  |  | 0.948 |

SR 133 \& Vicinity of the ACT V Parking Lot
Day: Saturday
City: Laguna Beach
Date: 12/2/2017
Project \#: CA17_1253_001


VOLUME
SR 133 \& Laguna College of Art and Design

Day: Thursday
Date: 11/30/2017

City: Laguna Beach
Project \#: CA17_1253_002


SR 133 \& Laguna College of Art and Design

Day: Saturday
Date: 12/2/2017

City: Laguna Beach
Project \#: CA17_1253_002


SR 133 \& Stan Oaks Dr

Day: Thursday
Date: 11/30/2017

City: Laguna Beach
Project \#: CA17_1253_003


SR 133 \& Stan Oaks Dr
Day: Saturday
Date: 12/2/2017
City: Laguna Beach
Project \#: CA17_1253_003


VOLUME
SR 133 Bet. Dog Park \& Willow Canyon Rd
Day: Thursday
City: Laguna Beach
Date: 11/30/2017
Project \#: CA17_1253_004


SR 133 Bet. Dog Park \& Willow Canyon Rd
Day: Saturday
City: Laguna Beach
Date: 12/2/2017
Project \#: CA17_1253_004


## Appendix B. Accident Data

## Page\#

1

| Location Description |  |  | Rate Group (RUS) |  |  | No. of Accidents / Significance |  |  |  |  |  |  | Pers Kld Inj | ADT <br> Main <br> X-St | Total MV+ or MVM | Accident Rates |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tot | Fat | Inj | F+I | Veh | Wet | Dark | Fat | F+I | Tot |  |  |  | Fat | F+I | Tot |
| 12 ORA 133 000.940-12 ORA 133001.573 |  |  |  | . 634 | MI H | 35 | 0 | 14 | 14 | 30 | 2 | 5 | 0 | 17.8 | 20.64 | 0.000 | . 68 | 1.70 | 0.012 | . 40 | . 83 |
| 0001-0001 | 2016-01-01 | 2020-12-31 |  |  |  | 60 mo. | NOR | TH U | H99 |  | H95 | H95 |  |  |  | 15 |  |  |  |  |  |  |  |  |
| 12 ORA 133000.940 -12 ORA 133001.573 |  |  |  | . 634 | Mı H | 16 | 0 | 7 | 7 | 10 | 0 | 3 | 0 | 17.8 | 20.64 | 0.000 | . 34 | . 78 | 0.012 | . 40 | . 83 |
| 0001-0002 | 2016-01-01 | 2020-12-31 | 60 mo. | SOU | TH U |  |  |  |  |  |  |  | 17 |  |  |  |  |  |  |  |  |

## Accident Rates expressed as: \# of accidents / Million vehicle miles

+ denotes that Million Vehicles (MV) used in accident rates instead (for intersections and ramps).
For Ramps RUS only considers R(Rural) U(Urban)


## Page\#

1


## Accident Rates expressed as: \# of accidents / Million vehicle miles

+ denotes that Million Vehicles (MV) used in accident rates instead (for intersections and ramps).
For Ramps RUS only considers R(Rural) U(Urban)


## Page\#

1

| Location Description |  |  | Rate Group (RUS) |  | No. of Accidents / Significance |  |  |  |  |  |  | Pers Kld Inj | $\begin{aligned} & \text { ADT } \\ & \text { Main } \\ & \text { X-St } \end{aligned}$ | Total MV+ or MVM | Accident Rates |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Tot | Fat | Inj | F+l | Veh | Wet | Dark |  |  |  | Fat | F+I | Tot | Fat | F+l | Tot |
| 12 ORA 133002.446 -12 ORA 133003.330 |  |  |  | . 885 MIH 11 | 36 | 0 | 20 | 20 | 26 | 2 | 10 | 0 | 18.8 | 30.37 | 0.000 | . 66 | 1.19 | 0.013 | . 40 | . 82 |
| 0001-0001 | 2016-01-01 | 2020-12-31 | 60 mo. | NORTH U | H97 |  | H97 | H97 |  |  |  | 23 |  |  |  |  |  |  |  |  |
| 12 ORA 133002.446 -12 ORA 133003.330 |  |  |  | . 885 MI H 11 | 24 | 0 | 17 | 17 | 14 | 2 | 5 | 0 | 18.8 | 30.37 | 0.000 | . 56 | . 79 | 0.013 | . 40 | . 82 |
| 0001-0002 | 2016-01-01 | 2020-12-31 | 60 mo . | SOUTH U |  |  | H90 |  |  |  |  | 21 |  |  |  |  |  |  |  |  |

## Accident Rates expressed as: \# of accidents / Million vehicle miles

+ denotes that Million Vehicles (MV) used in accident rates instead (for intersections and ramps).
For Ramps RUS only considers R(Rural) U(Urban)

California Department of Transportation Table B - Selective Accident Rate Calculation

Page\#
1
Event ID: 4380080

| Location Description |  |  | Rate Group (RUS) |  | No. of Accidents / Significance Multi |  |  |  |  |  |  | Pers Kld Inj | ADT <br> Main <br> X-St | $\begin{aligned} & \text { Total } \\ & \text { MV+ or } \\ & \text { MVM } \end{aligned}$ | Accident Rates |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tot | Fat | Inj | F+I | Veh | Wet | Dark | Fat | F+I |  |  |  | Tot | Fat | $F+1$ | Tot |
| 12 ORA 133 | .330-12 ORA | 03.415 |  |  |  | . 086 MI H 11 | 2 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 17.1 | 2.69 | 0.000 | . 00 | . 74 | 0.013 | . 40 | . 82 |
| 0001-0001 | 2016-01-01 | 2020-12-31 | 60 mo. | NORTH U |  |  |  |  |  |  |  | 0 |  |  |  |  |  |  |  |  |
| 12 ORA 133 | 3.330-12 ORA | 3.415 |  | . 086 MIH 11 | 6 | 0 | 2 | 2 | 4 | 0 | 1 | 0 | 17.1 | 2.69 | 0.000 | . 74 | 2.23 | 0.013 | . 40 | . 82 |
| 0001-0002 | 2016-01-01 | 2020-12-31 | 60 mo . | SOUTH U | H95 |  |  |  |  |  |  | 4 |  |  |  |  |  |  |  |  |

+ denotes that Million Vehicles (MV) used in accident rates instead (for intersections and ramps).
For Ramps RUS only considers R(Rural) U(Urban)

+ denotes MV used in rates.
Req $=$ investigation required (9, 6 or 3 or more accs. \& significant in 36, 24 or 12 months, resp.)

| $\begin{aligned} & \text { OTM22140 } \\ & \text { 15-08-18 } \\ & \text { 10:45 AM } \end{aligned}$ <br> Location Description | California Department of Transportation <br> Table C - Potential Investigation Locations |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Page\# 1 <br> Event ID: 3737047 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Confidence Level |  |  |  | District99.5$01-\mathrm{OCT}$ |  |  | 12 ALL A <br> Interval thru 30-S |  |  | $\begin{aligned} & \text { Accidents } \\ & .2 \quad \mathrm{M} \\ & \mathrm{EP}-13 \end{aligned}$ |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { SCL } \\ & \text { RMP } \\ & \text { LNS } \end{aligned}$ | R | Rate Grp | $\begin{aligned} & 36 \mathrm{mo} \\ & \text { ACCS } \end{aligned}$ | Total ACCS |  | $\begin{aligned} & \text { Accidents I } \\ & 12 \text { mo. } \\ & \text { ACCS } \end{aligned}$ |  | / Si | ificance ACCS |  | $\begin{array}{r} 3 \mathrm{mo} \\ \text { ACCS } \end{array}$ | AVE ADT <br> 1000 VEH |  |  | 12 MOS RATE ACCS/MV-MVMACTUALAVERAGE |  |  |  | Req |
|  |  |  |  |  |  |  |  | Main |  |  |  | X-St. | F+I | тот | F+I | TOT |  |
| 005 ORA 15.028 005/SB ON FROM EB OSO PKWY | OF | U | R 20 | 13 | Y | 12 |  |  | Y |  | Y |  | 3 | N |  | N | 5.8 | - | 1.89 | 3.31 | 0.18 | 0.57 + | Req |
| 005 ORA 030.866 TO 031.066 SOUTH | 06D | U | H67 | 168 | Y | 117 | Y | 47 | Y | 17 | Y |  | N | 173.3 | - | 0.95 | 3.71 | 0.33 | 1.15 | Req |
| 005 ORA $35.684005 /$ SBOFF STCOLL/THECITY DR | FD | $u$ | R 10 | 32 | Y | 19 | Y | 10 | Y | 8 | Y |  | Y | 7.8 | - | 3.16 | 3.51 | 0.35 | 1.01 + | Req |
| 005 ORA 35.718 005/SEGNB OFFHOV TO DISNEY | FC | U | R 06 |  | Y | 4 | Y |  | Y | 3 | Y |  | N | 1.5 | - | 5.48 | 7.31 | 0.16 | 0.49 + | Req |
| 005 ORA 41.745 005/SB ON FROM MAGNOLIA AVE | OD | U | R 12 | 19 | $Y$ | 18 | $Y$ |  | $Y$ | 2 | N |  | N | 11.1 | - | 0.99 | 1.97 | 0.22 | 0.63 + | Req |
| 022 ORA R007.738 TO R007.938 EAST | 05D | U | H66 | 49 | Y | 31 | Y | 16 | Y | 12 | Y |  | N | 109.5 | - | 1.13 | 2.00 | 0.28 | 0.94 | Req |
| 039 ORA 3.611 TALBERT AVE | xxx | U | 114 | - |  | 35 | Y | 16 | Y | 6 | N |  | N | 65.4 | 4 | 0.36 | 0.63 | 0.11 | 0.27 + | Req |
| 055 ORA T002.349 TO R002.549 SOUTH | 03D | U | H65 | 22 | Y | 15 | Y |  | Y | 4 | N |  | N | 45.1 | - | 0.61 | 2.13 | 0.18 | 0.58 | Req |
| 057 ORA 019.641 TO 019.841 NORTH | 05D | $u$ | H66 | 115 | Y | 85 | Y | 37 | Y | 9 | N |  | N | 122.1 | - | 0.90 | 4.15 | 0.31 | 1.01 | Req |
| 073 ORA 21.798 073/NB ON FR NB NEWPORT COAST | OL | U | R 40 | 6 | N | 5 | $N$ |  | N | 4 | Y |  | N | 4.6 | - | 1.19 | 2.37 | 0.21 | 0.73 + | Req |
| 091 ORA R001.500 TO R001.700 EAST | 05D | U | H66 | 25 | N | 22 | N | 16 | N | 13 | Y |  | N | 129.4 | - | 0.11 | 1.69 | 0.32 | 1.06 | Req |
| 091 ORA R001.700 TO R001.900 WEST | 05D | $u$ | H66 | 34 | N | 25 | N | 19 | N | 13 | Y |  | N | 130.2 | - | 0.42 | 2.00 | 0.32 | 1.06 | Req |
| 091 ORA 004.347 TO 004.747 WEST | 03D | $u$ | H65 | 93 |  | 66 |  | 41 |  | 26 |  | 19 |  | 128.9 | - | 0.90 | 2.18 | 0.37 | 1.16 | C1 |
| 133 ORA 001.050 TO 001.250 NORTH | 01D | U | H11 | 16 | Y | 13 | Y |  | N | 5 | Y | 4 | Y | 18.8 | - | 2.92 | 3.65 | 0.54 | 1.29 | Req |
| 133 ORA 001.270 TO 001.470 NORTH | 01D |  | H11 | 19 | Y | 16 | Y |  | Y |  | N | 4 | Y | 22.5 | - | 1.22 | 5.48 | 0.54 | 1.29 | Req |
| 241 ORA 033.848 TO 034.048 SOUTH | 03D | S | H61 | 8 | Y | 8 | Y | 7 | Y | 5 | Y |  | Y | 23.8 | - | 0.58 | 4.03 | 0.11 | 0.35 | Req |
| 405 ORA 011.520 TO 011.720 NORTH | 06D | U | H67 | 71 | Y | 50 | Y | 23 | Y |  | N |  | N | 156.4 | - | 0.88 | 2.02 | 0.30 | 1.06 | Req |
| 405 ORA 22.705 405/SB OFF SEAL BEACH BLVD | F G | U | R 22 | 24 | Y | 18 | Y | 6 | Y | 2 | N | 2 | $N$ | 3.9 | - | 2.09 | 4.18 | 0.33 | $1.00+$ | Req |

+ denotes MV used in rates.
Req $=$ investigation required (4 or more accs. \& significant in 12 , 6 , or 3 months)

| $\begin{aligned} & \text { OTM22140 } \\ & \text { 16-09-08 } \\ & \text { 12:06 PM } \end{aligned}$ <br> Location Description | California Department of Transportation Table C - Potential Investigation Locations |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Page\# 3 <br> Event ID: 3849861 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Confidence Level |  |  |  |  | $\begin{gathered} \text { District } \\ 99.5 \\ 01-\mathrm{OCT} \end{gathered}$ |  | $12$ |  | ALL erval | Acci |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { SCL } \\ & \text { RMP } \\ & \text { LNS } \end{aligned}$ | U | $\begin{aligned} & \text { Rate } \\ & \text { Grp } \end{aligned}$ | 36 mo. ACCS | Total 24 mo. ACCS |  | $\begin{gathered} \text { Accidents / } \\ 12 \mathrm{mo} \\ \text { ACCS } \end{gathered}$ |  |  | ificance ACCS |  | $\begin{aligned} & 3 \mathrm{mo} \\ & \text { ACCS } \end{aligned}$ |  | AVE ADT 1000 VEH |  | 12 MOS RATE ACCS/MV-MVMACTUALAVERAGE |  |  |  |  |
|  |  |  |  |  |  |  |  | Main |  |  |  | X-St. | F+I | TOT | F+I | TOT | Req |
| 091 ORA 001.029 TO 001.229 WEST | 03D | $u$ | H65 | 51 | $Y$ | 38 |  |  | Y | 22 | $Y$ |  | 12 | N | 6 | N | 124.5 | - | 0.44 | 2.42 | 0.35 | 1.13 | Req |
| 091 ORA 003.627 TO 003.827 WEST | 03D | U | H65 | 46 | N | 34 | N | 22 | Y | 9 | N | 6 | N | 133.0 | - | 0.62 | 2.27 | 0.36 | 1.19 | Req |
| 091 ORA 004.287 TO 004.487 WEST | 03D | U | H65 | 50 | Y | 40 | Y | 22 | Y | 8 | N | 6 | N | 129.3 | - | 0.42 | 2.33 | 0.35 | 1.16 | Req |
| 091 ORA 005.383 TO 005.583 WEST | 05D | U | H67 | 45 | Y | 30 | Y | 20 | Y | 11 | Y | 7 | N | 126.9 | - | 0.54 | 2.16 | 0.26 | 0.91 | Req |
| 091 ORA 3.502 091/SEGWB CONN FRONTAGE RD | Z A | U | R 02 | 22 | Y | 17 | Y | 9 | $Y$ | 8 | Y | 6 | Y | 10.5 | - | 1.83 | 2.35 | 0.19 | $0.72+$ | Req |
| 091 ORA R009.810 TO R010.010 WEST | 05D | U | H 67 | 50 | N | 35 | N | 20 | N | 13 | N | 10 | Y | 161.0 | - | 0.34 | 1.70 | 0.31 | 1.09 | Req |
| 091 ORA R015.964 TO R016.164 EAST | 06D | U | H67 | 29 | N | 24 | N | 18 | Y | 9 | N | 4 | N | 129.8 | - | 0.42 | 1.90 | 0.27 | 0.93 | Req |
| 133 ORA R 4.173 ON/OFF RAMPS(RTE 73) RT | XXX |  | 129 | 14 | $Y$ | 12 | Y | 7 | $Y$ | 5 | Y | 3 | N | 21.4 | . 1 | 0.38 | 0.89 | 0.09 | 0.21 + | Req |
| 405 ORA 002.655 TO 002.855 NORTH | 06D | U | H 67 | 38 | N | 25 | N | 14 | N | 11 | Y | 7 | N | 124.9 | - | 0.44 | 1.54 | 0.26 | 0.90 | Req |
| 405 ORA 010.660 TO 010.860 NORTH | 08D | U | H 67 | 31 | N | 22 | N | 17 | N | 12 | N | 9 | Y | 146.1 | - | 0.47 | 1.59 | 0.29 | 1.01 | Req |
| 405 ORA 011.520 TO 011.720 NORTH | 06D | U | H67 | 79 | Y | 52 | Y | 27 | Y | 14 | Y | 6 | N | 156.1 | - | 0.44 | 2.37 | 0.30 | 1.06 | Req |
| 405 ORA 20.277 405/NB OFF GARDEN GROVE/22 | FD | $u$ | R 10 | 43 | Y | 26 | Y | 15 | Y | 13 | Y | 9 | Y | 11.6 | - | 1.42 | 3.55 | 0.35 | 1.01 + | Req |
| 405 ORA 22.705 405/SB OFF SEAL BEACH BLVD | FG | $u$ | R 22 | 25 | Y | 13 | Y |  | Y | 3 | N | 2 | N | 3.9 | - | 2.79 | 4.88 | 0.33 | $1.00+$ | Req |
| 405 ORA 013.626 TO 013.826 NORTH | 05D | U | H66 | 61 | Y | 38 | Y | 20 | N | 12 | N | 10 | Y | 143.0 | - | 0.48 | 1.92 | 0.34 | 1.14 | Req |
| 405 ORA 021.088 TO 021.288 SOUTH | 05D | $u$ | H67 | 64 | N | 45 | N | 27 | N | 18 | Y | 9 | N | 188.5 | - | 0.51 | 1.96 | 0.35 | 1.22 | Req |
| 605 ORA R001.175 TO R001.375 SOUTH | 04D |  | H66 | 53 | Y | 37 |  | 17 |  |  | N |  | N | 80.5 | - | 0.51 | 2.89 | 0.23 | 0.76 | Req |

+ denotes MV used in rates.
Req $=$ investigation required ( 4 or more accs. \& significant in 12 , 6 , or 3 months)

| $\begin{aligned} & \text { OTM22140 } \\ & 14-12-17 \end{aligned}$ | California Department of Transportation Table C - Potential Investigation Locations |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{ll} \text { Page\# } & 2 \\ \text { Event ID: } & 3682267 \end{array}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Confidence Level |  |  |  |  | District 99.5 <br> 01-JAN- |  | $12$ |  | Inte ru | ALL <br> erval | Acc <br> DEC | $\begin{gathered} \text { cidents } \\ .2 \\ c-12 \end{gathered}$ | MI |  |  |  |  |  |  |  |
| Location Description | $\begin{aligned} & \text { SCL } \\ & \text { RMP } \\ & \text { LNS } \end{aligned}$ | R | Rate Grp | $\begin{aligned} & 36 \mathrm{mo} \\ & \text { ACCS } \end{aligned}$ | Total24 mo ACCS |  | $\begin{aligned} & \text { Accidents } / \begin{array}{c} 12 \mathrm{mo} \end{array} \\ & \text { ACS } \end{aligned}$ |  |  | / Sia | ificance 6 mo. ACCS |  | $\begin{aligned} & 3 \mathrm{mo} . \\ & \text { ACCS } \end{aligned}$ |  | $\begin{aligned} & \text { AVE ADT } \\ & 1000 \text { VEH } \end{aligned}$ |  | 12 MOS RATE ACCS/MV-MVM |  |  |  | Req |
|  |  |  |  |  |  |  |  | Main | X-St. |  |  |  | F+I | тот | F+I | тот |  |
| 057 ORA 014.771 TO 014.971 NORTH | 05D | U | H67 | 46 | Y | 27 |  |  |  | N |  | 18 Y |  | Y | 14 | Y |  | Y | 125.0 | - | 0.55 | 1.97 | 0.26 | 0.91 | Req |
| 057 ORA 017.366 TO 017.566 SOUTH | 05D | U | H66 | 46 | N | 34 | Y |  | 20 Y | Y | 12 | N | 5 | N | 131.6 | - | 0.31 | 2.08 | 0.32 | 1.07 | Req |
| 057 ORA 018.661 TO 018.861 SOUTH | 05D | U | H66 | 41 | N | 29 | N |  | 18 N | N | 12 | $Y$ | 9 | Y | 122.0 | - | 0.79 | 2.02 | 0.31 | 1.01 | Req |
| 057 ORA 019.681 TO 019.881 SOUTH | 05D | U | H66 | 50 | Y | 37 | Y |  | 23 Y | Y |  | N |  | N | 121.6 | - | 0.90 | 2.59 | 0.31 | 1.01 | Req |
| 074 ORA 013.468 TO 013.868 | 02 U | R | H05 | 24 |  | 16 |  |  | 13 |  | 10 |  | 8 |  | 10.2 | - | 2.01 | 8.69 | 0.72 | 1.45 | C2 |
| 091 ORA R002.485 TO R002.685 EAST | 05D | U | H66 | 60 | $Y$ | 35 | Y |  | 20 Y |  | 12 | N | 6 | N | 131.8 | - | 0.62 | 2.08 | 0.32 | 1.07 | Req |
| 091 ORA R 4.031 091/WB OFF TO MAGNOLIA AVE | F D | U | R 10 | 28 | Y | 20 | Y |  |  | Y |  | Y | 2 | N | 8.9 | - | 1.23 | 3.08 | 0.35 | 1.01 + | Req |
| 133 ORA 002.928 TO 003.128 NORTH | 01D | $u$ | H 11 | 13 | $Y$ | 12 | $Y$ |  | 7 Y |  | 1 | N | 1 | N | 18.8 | - | 1.46 | 5.11 | 0.54 | 1.29 | Req |
| 133 ORA 008.607 TO 008.807 SOUTH | 02D |  | H64 |  | N | 5 | N |  | $4 Y$ |  |  | Y | 3 | Y | 17.0 | - | 0.81 | 3.22 | 0.13 | 0.43 | Req |
| 142 ORA 005.247 TO 005.447 | 02 U | $u$ | H 11 | 10 | N |  | $N$ |  |  | $Y$ |  | N | 2 | N | 16.1 | - | 1.70 | 5.97 | 0.54 | 1.29 | Req |
| 405 ORA 5.733 405/NB ON SB CULVER DR | OF | U | R 20 | 13 | Y | 10 | Y |  | 8 Y | Y | 6 | Y | 3 | N | 8.3 | - | 0.66 | 2.64 | 0.18 | 0.57 + | Req |
| 405 ORA 15.199 405/SEG NB ON FR WB WARNER | O Z | U | R 50 | 11 | N | 8 | N |  |  | $Y$ | 6 | Y | 3 | N | 8.1 | - | 1.01 | 2.71 | 0.25 | 0.75 + | Req |
| 405 ORA 20.277 405/NB OFF GARDEN GROVE/22 | F D | U | R 10 | 38 | Y | 26 | Y |  | 13 Y | Y |  | N | 3 | N | 11.6 | - | 0.71 | 3.08 | 0.35 | 1.01 + | Req |
| 405 ORA 012.470 TO 012.670 NORTH | 06D | U | H67 | 78 | Y | 58 | Y |  | 37 Y | Y | 14 | Y | 7 | N | 146.0 | - | 0.94 | 3.47 | 0.29 | 1.01 | Req |
| 405 ORA 23.828 405/NB OFF TO NB RTE 605 | FF | U | R 62 | 28 | N | 27 | Y |  | 17 Y | Y | 10 | N | 4 | N | 53.1 | - | 0.26 | 0.88 | 0.12 | 0.38 + | Req |
| 405 ORA 013.626 TO 013.826 NORTH | 05D | U | H66 | 67 | Y | 44 | Y |  | 28 Y |  | 15 | Y | 6 | N | 143.5 | - | 0.67 | 2.67 | 0.34 | 1.14 | Req |
| 405 ORA 022.528 TO 022.728 SOUTH | 07D | U | H67 | 99 | Y | 66 | Y |  | 34 Y |  | 16 | N | 10 | N | 187.2 | - | 0.51 | 2.49 | 0.35 | 1.22 | Req |

+ denotes MV used in rates.
Req $=$ investigation required (4 or more accs. \& significant in 12 , 6 , or 3 months)

+ denotes MV used in rates.
Req $=$ investigation required (9, 6 or 3 or more accs. \& significant in 36 , 24 or 12 months, resp.)


## Appendix C. Reversible Lane Operations Concept Memorandum

# Technical Memorandum 

Date: Tuesday, December 21, 2021
Project: SR-133 Laguna Canyon Road PSR/PDS
To: City of Laguna Beach
From: Doug Smith, PE
Kent Ko, PE, TE

Subject: Reversible Lane Operations Concept Memorandum

## 1 Introduction

The City of Laguna Beach (City), in cooperation with the California Department of Transportation (Caltrans) District 12, is proposing to construct improvements along the State Route 133 (SR133) corridor extending approximately 2.5 miles from Canyon Acres Drive (Post Mile [PM] 0.96) to El Toro Road (PM 3.41) in the City of Laguna Beach, Orange County (the Project).

SR-133, also known as Laguna Canyon Road (LCR) in this area, extends further south of Canyon Acres Drive, terminating at Pacific Coast Highway (SR-1) and transitions into unincorporated Orange County (County) north of the junction with El Toro Road. LCR is one of three gateways into the City and provides critical access to adjacent recreational spaces as well as key destinations and activities in the City. As such, ensuring that LCR provides efficient, safe access to the area is vital both to the region and to the City itself.

### 1.1 Location and Background

The Transportation, Circulation and Growth Management Element of the City's General Plan identifies LCR as a Primary Arterial, serving as a regional access to and from the City, as well as a critical evacuation route. Due to the topographic constraints with the roadway located within an existing canyon and the proximity of the Pacific Ocean to the south, LCR serves as one of only three routes in and out of the City. Pacific Coast Highway (PCH or SR-1) accommodates travelers north and south along the coast, and LCR is oriented inland. As part of the State Highway System, LCR connects SR-1 and the coastal areas within the County to three of the key inland highways including Interstate 5 (I-5), I-405, and the SR-73 toll road.

### 1.2 Purpose and Need

The purpose and need of the Project are defined below.
The purpose of the Project is to:

- Improve traffic safety and provide room for bicycle and pedestrian facilities by undergrounding the existing overhead utilities located within the Clear Recovery Zone ( CRZ)
- Encourage the use of active transportation modes through infrastructure improvements that increase the use of public transit, walking, and biking, and allow for greater connectivity to adjacent residential and commercial land uses, recreational trails and parks within the City of Laguna Beach
- Improve pedestrian and bicycle mobility and safety by separating vehicles, cyclists and pedestrians by incorporating dedicated pedestrian and bicycle paths, sidewalks, Americans with Disabilities Act (ADA) access, and improved shoulders along the corridor

Traffic demand within this corridor already exceeds capacity during weekday AM and PM peak hours and during most summer weekends and holidays due to special events and the proximity to the Pacific Ocean as well as multiple adjacent recreational facilities and trails. The high traffic demand and resulting vehicle queuing, and the lack of traffic breaks, protected left-turn movements and inadequate shoulders contribute to a high concentration of accidents in various locations within the Project limits. In addition, the corridor lacks adequate shoulders and pedestrian and bicycle facilities within the Project limits Without the implementation of traffic improvements and the provision for alternative transportation modes such as bike and pedestrian facilities, quality and level of service of this multi-modal corridor will continue to degrade.

The corridor has multiple constraints including overhead SCE transmission and distribution lines on both sides of the corridor within the CRZ and in close proximity to the edge of travel way. The right-of-way is further constrained by residential and light commercial developments as well as various environmental constraints along the route.

## Purpose of this Document:

A reversible lane is being considered part of the overall corridor improvements evaluation in the PSR/PDS. This document presents how a reversible lane would operate. The document also provides a high-level review of traffic volumes and discusses how the reversible lane would serve residents and visitors.

## 2 Reversible Lane Background

Reversible traffic lanes add peak-direction capacity to a two-way road and decrease congestion by borrowing available lane capacity from the other (off-peak) direction. Reversing lanes reduces congestion for handling special event traffic, during morning and evening commutes, when an incident affects operation, or when construction or maintenance activity is present on the road. Reversible lanes make sense for roadways that experience regular, significant imbalances in traffic demand by direction during peak periods. Roads that may be used as emergency evacuation routes or for special events also benefit from reversible lane strategies.

This section describes the criteria used to develop the reversible lane system (RLS) concept operations along the SR-133 corridor.

### 2.1 Risk / Safety

Safety concerns are related to a several factors, including conflicts between opposing mainline vehicles, through and turning vehicles, entering of side-street and driveway traffic and general driver confusion associated with unfamiliarity with reversible lane operations, control systems, and movements. Also, in general, as collisions generally occur infrequently, the sound evaluation of safety performance of reversible lane systems requires a long evaluation periods (at least three years after the implementation of the treatment).

There are three primary types of collisions are typically associated with reversible operations; leftturning traffic from reversible lanes, left-turning traffic to reversible lanes, and left-turn from lanes immediately adjacent to reversible lanes. The number of collisions involving a left-turning vehicle would be a critical safety performance of the reversible lane system. The following risk / safety factor should be considered during the design phase.

- Minimize entering traffic from side streets or from reversible lanes
- Provide standard merge / diverge transition zones
- Minimize potential head-on collision


### 2.2 City / State Policy

Policies on the use of reversible facilities are those associated with the eligibility requirements for particular vehicles. These policies assign reversible lane usage priority to certain vehicle classifications or restrict the RLS usage to others. One of the most common policies used to manage the accessibility of reversible facilities is to limit their use to transit and high occupancy vehicles (HOV). These policies have been in use on freeways in several urban centers in Florida and Texas. The proposed reversible lane along the State Route 133 (SR-133) corridor will have no restriction and operate as a general-purpose lane.

Local businesses and communities may be impacted with the implementation of a reversible lane. A reversible lane may require parking restrictions, limit access to the business, or limit freight access and movements. Access to local communities can also be affected through turning restrictions. Due to the potential impact to local businesses and communities, policies should consider time of day operation of the reversible lane and turn restrictions.

The hours or time period of operations will need reviewed and implemented by the City. Based on the existing peak hour directional flow, the reversible lane would be operational for southbound traffic during the AM peak period and northbound during the PM peak period. Hours of operations may occur between 7 am to 9 am during the AM peak period and 4 pm to 6 pm during the PM peak period. During off-peak periods, the reversible lane may operate as a two-way left turn lane.

## 3 Proposed Reversible Lane Design \& Operations

### 3.1 Geometric Design

### 3.1.1 Cross-section

The existing cross-section generally consists of a typical width of 64 feet for the majority of the route including the vehicle, pedestrian, and bicycle facilities. With a reversible lane, the crosssection would include 12 -foot travel lanes, and a 12- to 14-foot center reversible lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5 -foot Class II buffered bike lane/shoulder on both sides of the roadway. During emergencies, the configuration could provide for four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes.

A constrained segment existing near the 'Big Bend' where the bike lane widths would be reduced to five feet and the travel lanes reduced to 11 feet. At this pinch point of 53 feet available ROW width, the pedestrian paths and bike lane buffers on either side of the roadway would be reduced within this short segment. See Figure 1 for typical cross-section.

Figure 1. Typical Cross-Section


Limited areas of the constrained conditions


F?

### 3.1.2 Approach, Departure and Transition Areas

At the southern terminus, the RLS will begin just north of the driveway to the existing Maintenance Yard/Municipal Parking Lot (ACT V Parking Lot). Since the RLS will begin just north of the driveway, access/driveways to ACT V Parking Lot will not be modified from the current configuration and will not be limited to the RLS "time of day" (TOD) operation. The RLS will operate where northbound traffic will transition from the number one lane and merge left onto the center reversible lane. Southbound traffic will transition from the center reversible lane onto the southbound number one through lane. Southbound traffic will not be required to merge and/or maneuver out of the center reversible lane.

At the northern terminus, the RLS will begin at the intersection of El Toro Road. The RLS will operate where southbound traffic will transition from the number one lane and merge left onto the center reversible lane. Northbound traffic will transition from the center reversible lane onto the southbound number one through lane. Northbound traffic will not be required to merge and/or maneuver out of the center reversible lane. Note that further coordination will be required to implement any future projects including the improvements at the Anneliese School driveway.

Ingress and egress will be controlled by traffic control devices that include overhead signage and signals. The subsequent section provides additional information and details on the various traffic control devices.

### 3.1.3 Intersections

Two signalized intersections at Canyon Acres Drive and El Toro Road are located within the Project limits. In addition, an existing midblock HAWK (High-Intensity Activated crossWalK) signal is located between the Main Campus and East Campus of the Laguna College of Art and Design (LCAD). Signal timing strategies should be reviewed and implemented at these signalized intersections, especially at the north and south terminus of the RLS.

### 3.2 Operational Assessment

Standard evaluations for intersections, road segments and arterials are as valid for RLS facilities as for any facility. The implementation of a reversal does not fundamentally change the expectations for roadway facilities. Therefore, the various methodologies, as described in the Highway Capacity Manual (HCM), for example, are still valid for use by the City and Caltrans.

The Traffic Engineering Performance Assessment (TEPA) prepared for this Project includes both vehicle traffic demand and operational analysis along the corridor as well as an assessment of complete street elements, such as bike and pedestrian facilities, and transit services. A general comparison of capacity and operations along the roadway are provided in this section. See the TEPA for additional detail and information on the operational assessment.

Under existing conditions, the AM peak direction was determined to occur in the southbound direction with a weighted average of 55 percent. The PM peak direction was determined to occur in the northbound direction with a weighted average of 51 percent. Reversible traffic lanes add peak-direction capacity to a two-way road and decrease congestion by borrowing available lane
capacity from the other (off-peak) direction; therefore, reversible lane might be a viable option to help alleviate congestion through the corridor.

Under existing conditions, the Volume-to-capacity ratios (V/C) exceeds capacity with segments to be nearly 50 percent over capacity. With the implementation of the reversible lane configuration for southbound AM peak direction and northbound PM peak direction, there would be nearly a 30 percent reduction in V/C. Table 1 and 2 provide a summary of the $V / C$ for existing and reversible lane configurations, respectively. The RLS facility would provide operational benefits and is considered a viable alternative.

Table 1. Existing Configuration

| ID | Segment | Description | Direction | Existing AM Peak Hour | V/C | Existing PM Peak Hour | V/C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LCR/SR-133 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,006 | 1.12 | 1,348 | 1.50 |
|  |  |  | Southbound | 1,239 | 1.38 | 1,251 | 1.39 |
| 2 | LCR/SR-133 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 988 | 1.10 | 1,350 | 1.50 |
|  |  |  | Southbound | 1,267 | 1.41 | 1,264 | 1.40 |
| 3 | LCR/SR-133 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 989 | 1.10 | 1,306 | 1.45 |
|  |  |  | Southbound | 1,249 | 1.39 | 1,282 | 1.42 |
| 4 | LCR/SR-133 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,032 | 1.15 | 1,307 | 1.45 |
|  |  |  | Southbound | 1,235 | 1.37 | 1,301 | 1.45 |

Capacity for existing (1 lane - 900 vehicle per hour)

## Table 2. Reversible Lane Configuration

| ID | Segment | Description | Direction | Existing AM Peak Hour | V/C | Existing PM Peak Hour | V/C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LCR/SR-133 | Between El Toro Road \& Sun Valley Drive | Northbound | 1,006 | 1.12 | 1,348 | 0.75 |
|  |  |  | Southbound | 1,239 | 0.69 | 1,251 | 1.39 |
| 2 | LCR/SR-133 | Between Sun Valley Drive \& Stan Oaks Drive | Northbound | 988 | 1.10 | 1,350 | 0.75 |
|  |  |  | Southbound | 1,267 | 0.70 | 1,264 | 1.40 |
| 3 | LCR/SR-133 | Between Stan Oaks Drive \& LCAD Driveway | Northbound | 989 | 1.10 | 1,306 | 0.73 |
|  |  |  | Southbound | 1,249 | 0.69 | 1,282 | 1.42 |
| 4 | LCR/SR-133 | Between LCAD Driveway \& Canyon Acres Drive | Northbound | 1,032 | 1.15 | 1,307 | 0.73 |
|  |  |  | Southbound | 1,235 | 0.69 | 1,301 | 1.45 |

Capacity for reversible lane (2 lane - 1,800 vehicle per hour)

### 3.3 Traffic Control Devices

The predominant means of guiding and controlling traffic moving into, out of, and along reversible lane segments are standard roadway signs, signals, and pavement markings per CA MUTCD. Signs for reversible lane segments may be placed either overhead above the lanes or along the roadside. There are a number of other signs as shown in Figure 2, to indicate the actual number of lanes in each direction during the associated peak hours. These types of signs are used where the RLS control is TOD. TOD operation is proposed for the reversible lane system (RLS) operations along the State Route 133 (SR-133) corridor.

Figure 2. Typical Reversible Lane Signs


Lane control signals are used to indicate which lanes of a reversible roadway are available (or not available) for use in a particular direction. Lane control signals must feature two types of displays: a downward pointing green arrow, and a red " $X$ ", both on a black background. The red " $X$ " must be capable of both flashing and solid operation. See Figure 3 for typical lane control signals.

Figure 3. Typical Lane Control Signals


In reversible flow lane applications, the face must be visible to both directions of intended travel. The system must not permit simultaneous display of green down arrow to both directions in any lane. All lanes of an RLS should have a lane control signal to give positive guidance to the driver.

In a reversible lane system, pavement markings are used to guide traffic into and out of the reversible lane. Pavement markings for arterial and freeway RLS are typically permanent markings.

In general, the design of the pavement markings should comply with design standards, the CA MUTCD, and other appropriate published standards. Double yellow broken lines should be used to delineate the directional dividing line for traffic flow at different times of the lane reversal. Markings for reversible lanes should be as per the latest CA MUTCD recommendation of normal broken double yellow line to delineate the edge of a lane. See Figure 4 for typical lane marking.
Figure 4. Typical Lane Marking
Figure 3B-6. Example of Reversible Lane Marking Application


Other reversible lane traffic control devices may include automated barrier gate and swing gates at the terminal areas, traffic cameras, vehicle detectors, permanent and movable barriers, dynamic message signs (DMS), changeable lane designation signs and temporary traffic cones and tubular markers. See Figure 5 for an example of an existing reversible lane traffic control devices located along $4^{\text {th }}$ in the City of Los Angeles.

Figure 5. City of Los Angeles - $4^{\text {th }}$ Street Reversible Lane Control Signal


### 3.4 System Detection

If required, detection devices can be the traditional inductive loop detectors, micro-wave detectors or video detectors. In addition to the detectors for RLS operations, CCTV camera may also be used to provide a video link and incident management.
In arterial RLS installations, detection zones are typically mid-block where they can best monitor traffic speed and density (least affected by upstream or downstream intersections). They should be installed in each lane separately to help identify individual lane flows and incidents.

### 3.5 Reversible Lane System Management

Reversible lane systems need to be planned, designed, and operated as a managed lane system. There are components of the system that are standard traffic control devices noted above, and there are more specialized components that are utilized in specific situations to provide information and guidance to the driver. Intelligent transportation systems (ITS) can be utilized in order to improve efficiency and performance of reversible lanes in an urban area by using technology to engage changeable message signs and to automate the reversal process. The RLS can be monitored and controlled within the City traffic management center (TMC) to provide overall management of the system.

### 3.6 Transit Operations

Transit operation is allowed for the RLS operations along the State Route 133 (SR-133) corridor which would affect transit routing, headways and stop locations. The RLS may increase the complexity of weaving for transit vehicles, depending on their routing. Transit travel time may serve as a transit related measure of performance for the RLS.

### 3.7 Monitoring and Enforcement

Traditional enforcement on RLS lanes requires the specific design treatment known as dedicated enforcement areas. These areas are usually located immediately adjacent to the reversible lanes facility and allow enforcement personnel to monitor the facility, pursue and apprehend violators to issue appropriate citations.

The RLS can be monitored and controlled within the City TMC to provide overall management of the system. The ongoing monitoring of system performance measures will help to justify the system in the long term, and also help to identify when changes are required. If the RLS is a fixed time system based on morning and afternoon weekday peak hours, then ongoing traffic flow monitoring will help identify when the system needs to start and stop. Typical performance measures include:

- 15 minute directional traffic flow counts;
- Peak hour directional level of service; and
- Peak hour directional vehicle (person) delay.


## Appendix D. Peak Season Traffic Growth Development

| Years | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 | 2018 | 2019 | 2020 | $\begin{array}{\|c\|} \hline \text { Average } \\ \text { Peak } \\ \text { AD } \\ \text { Growth } \\ \hline 100 \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average ADT | 35,000 | 35,000 | 35,000 | 36,000 | 45,000 | 36,000 | 36,000 | 40,000 | 38,000 | 35,500 | 36,000 | 36,000 | 36,000 | 36,000 | 36,000 | 35,000 | 35,000 | 36,000 | 36,000 | 36,000 | 36,000 | 37,000 | 37,500 | 37,600 | 37,700 | 37,500 | 37,500 | 37,500 | 35,000 | 38,700 | 38,700 |  |
| Peak Month ADT | 41,500 | 41,500 | 41,500 | 42,500 | 53,000 | 42,500 | 42,500 | 44,500 | 42,500 | 39,500 | 40,000 | 40,000 | 40,000 | 40,000 | 40,000 | 39,000 | 39,000 | 40,000 | 40,000 | 40,000 | 40,000 | 41,000 | 41,500 | 42,000 | 42,000 | 42,000 | 42,000 | 42,000 | 39,000 | 39,000 | 39,000 |  |
| Peak Month ADT/Average ADT | 19\% | 19\% | 19\% | 18\% | 18\% | 18\% | 18\% | 11\% | 12\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 11\% | 12\% | 11\% | 12\% | 12\% | 12\% | 11\% | 1\% | 1\% | 12\% |

## Appendix E. Existing Highway LOS Worksheets

| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To E/ Toro/Sun Valley Dr <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: $\operatorname{SR-133}$ PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1093 1347 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $\left.=\mathrm{BFFS}-\mathrm{f}_{\mathrm{Ls}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $28.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $59.4 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1093 1347 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 83.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 12.3 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 88.9 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.64 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To E/ Toro/Sun Valley Dr <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: $\operatorname{SR-133}$ PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1465 1360 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1465 1360 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 9.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 94.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.86 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To E/ Toro/Sun Valley Dr <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: $\operatorname{SR-133}$ PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1347 1093 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1347 1093 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 86.1 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 12.3 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 92.9 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.79 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To E/ Toro/Sun Valley Dr <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: $\operatorname{SR-133}$ PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1360 1465 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $26.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $53.6 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1360 1465 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 88.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 9.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.80 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To  <br> Fun Valley Dr/Stan Oaks Dr  <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1074 1377 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1074 1377 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 83.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 12.1 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 88.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.63 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To  <br> Fun Valley Dr/Stan Oaks Dr  <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1467 1374 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1467 \| 1374 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 8.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 94.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.86 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To Sun Valley Dr/Stan Oaks Dr <br> Jromisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1377 1074 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $28.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $58.8 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1377 \| 1074 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 86.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 12.1 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.81 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To Sun Valley Dr/Stan Oaks Dr <br> Jromisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1374 1467 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $26.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $53.3 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1374 1467 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 8.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.81 |





| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To Stan Oaks Dr/LCAD dwy <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1420 1393 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $\left.=\mathrm{BFFS}-\mathrm{f}_{\mathrm{Ls}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $26.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $53.6 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1420 1393 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 8.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.9 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.84 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To Stan Oaks Dr/LCAD dwy <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1358 1075 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1358 1075 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 86.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 12.4 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.80 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/SB <br> From/To Stan Oaks Dr/LCAD dwy <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1393 1420 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $26.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $53.6 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1393 1420 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 8.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.82 |





| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $1 / 23 / 2018$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR-133/NB <br> From/To LCAD dwy/Canyon Acres Dr <br> Jurisdiction Caltrans <br> Analysis Year Existing 2017 |
| Project Description: SR-133 PSR/PDS |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1421 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $50.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $1.3 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.0 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $25.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $53.3 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 1421 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 89.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 8.7 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 93.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | E |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.84 |







## Appendix F. Existing Intersection LOS Worksheets



HCM Unsignalized Intersection Capacity Analysis
2: Laguna Cyn Rd \& Anneliese Dwy


| Direction, Lane \# WB 1 | NB 1 | SB 1 | SB 2 |  |
| :---: | :---: | :---: | :---: | :---: |
| Volume Total 165 | 1360 | 170 | 1426 |  |
| Volume Left 18 | 0 | 170 | 0 |  |
| Volume Right 147 | 28 | 0 | 0 |  |
| cSH 154 | 1700 | 505 | 1700 |  |
| Volume to Capacity 1.07 | 0.80 | 0.34 | 0.84 |  |
| Queue Length 95th (ft) 215 | 0 | 37 | 0 |  |
| Control Delay (s) 152.2 | 0.0 | 15.7 | 0.0 |  |
| Lane LOS F |  | C |  |  |
| Approach Delay (s) 152.2 | 0.0 | 1.7 |  |  |
| Approach LOS F |  |  |  |  |
| Intersection Summary |  |  |  |  |
| Average Delay |  | 8.9 |  |  |
| Intersection Capacity Utilization |  | 98.6\% | ICU Level of Service | F |
| Analysis Period (min) |  | 15 |  |  |





HCM Unsignalized Intersection Capacity Analysis
6: Laguna Cyn Rd \& Castle Rock Rd




| Direction, Lane \# | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | SB 2 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Volume Total | 87 | 72 | 83 | 1197 | 1409 | 67 |  |
| Volume Left | 87 | 0 | 83 | 0 | 0 | 0 |  |
| Volume Right | 0 | 72 | 0 | 0 | 0 | 67 |  |
| cSH | 65 | 170 | 456 | 1700 | 1700 | 1700 |  |
| Volume to Capacity | 1.33 | 0.42 | 0.18 | 0.70 | 0.83 | 0.04 |  |
| Queue Length 95th (ft) | 181 | 48 | 16 | 0 | 0 | 0 |  |
| Control Delay (s) | 330.8 | 41.0 | 14.6 | 0.0 | 0.0 | 0.0 |  |
| Lane LOS | F | E | B |  | 0.0 |  |  |
| Approach Delay (s) | 199.5 |  | 0.9 |  | 0.0 |  |  |
| Approach LOS | F |  |  |  |  |  |  |
| Intersection Summary |  |  | 11.3 |  |  |  |  |
| Average Delay |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  | $79.3 \%$ | ICU Level of Service |  |  |  |  |
| Analysis Period (min) |  | 15 |  |  |  |  |  |


|  | $\dagger$ | 4 | $\dagger$ | $\dagger$ | $p$ | - | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% | F | ด | 个4 | F | \% | 个4 |  |
| Traffic Volume (veh/h) | 37 | 14 | 7 | 1307 | 13 | 11 | 1280 |  |
| Future Volume (veh/h) | 37 | 14 | 7 | 1307 | 13 | 11 | 1280 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial Q (Qb), veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 39 | 15 |  | 1361 | 14 | 11 | 1333 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 72 | 64 |  | 2835 | 1237 | 24 | 3054 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.80 | 0.80 | 0.01 | 0.86 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 39 | 15 |  | 1361 | 14 | 11 | 1333 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 2.0 | 0.9 |  | 11.6 | 0.2 | 0.6 | 7.7 |  |
| Cycle Q Clear(g_c), s | 2.0 | 0.9 |  | 11.6 | 0.2 | 0.6 | 7.7 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 72 | 64 |  | 2835 | 1237 | 24 | 3054 |  |
| V/C Ratio(X) | 0.54 | 0.23 |  | 0.48 | 0.01 | 0.47 | 0.44 |  |
| Avail Cap(c_a), veh/h | 486 | 434 |  | 2835 | 1237 | 124 | 3054 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 43.8 | 43.2 |  | 3.0 | 1.9 | 45.6 | 1.4 |  |
| Incr Delay (d2), s/veh | 6.3 | 1.8 |  | 0.6 | 0.0 | 13.6 | 0.5 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 1.1 | 0.4 |  | 5.7 | 0.1 | 0.4 | 3.7 |  |
| LnGrp Delay(d),s/veh | 50.0 | 45.1 |  | 3.6 | 1.9 | 59.2 | 1.9 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 54 |  |  | 1375 |  |  | 1344 |  |
| Approach Delay, s/veh | 48.7 |  |  | 3.6 |  |  | 2.3 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R c$ ), s | 5.7 | 79.0 |  |  |  | 84.7 |  | 8.3 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 6.5 | 74.5 |  |  |  | 74.5 |  | 25.5 |
| Max Q Clear Time (g_c+l1), s | 2.6 | 13.6 |  |  |  | 9.7 |  | 4.0 |
| Green Ext Time (p_c), s | 0.0 | 16.0 |  |  |  | 13.1 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 3.8 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |
| User approved ignoring U-Turning movement. |  |  |  |  |  |  |  |  |



HCM Unsignalized Intersection Capacity Analysis
2: Laguna Cyn Rd \& Anneliese Dwy


| Direction, Lane \# | WB 1 | NB 1 | SB 1 | SB 2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 67 | 1316 | 50 | 1283 |  |
| Volume Left | 10 | 0 | 50 | 0 |  |
| Volume Right | 57 | 8 | 0 | 0 |  |
| cSH | 183 | 1700 | 525 | 1700 |  |
| Volume to Capacity | 0.37 | 0.77 | 0.10 | 0.75 |  |
| Queue Length 95th (ft) | 39 | 0 | 8 | 0 |  |
| Control Delay (s) | 35.6 | 0.0 | 12.6 | 0.0 |  |
| Lane LOS | E |  | B |  |  |
| Approach Delay (s) | 35.6 | 0.0 | 0.5 |  |  |
| Approach LOS | E |  |  |  |  |
| Intersection Summary |  |  |  |  |  |
| Average Delay |  |  | 1.1 |  |  |
| Intersection Capacity Utilization |  |  | 78.6\% | ICU Level of Service | D |
| Analysis Period (min) |  |  | 15 |  |  |





HCM Unsignalized Intersection Capacity Analysis
6: Laguna Cyn Rd \& Castle Rock Rd




|  | $\dagger$ | 4 | $\dagger$ | $\dagger$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 「 | 日 | 性 | 「 | \％ | 性 |  |
| Traffic Volume（veh／h） | 18 | 13 | 11 | 1201 | 28 | 14 | 1191 |  |
| Future Volume（veh／h） | 18 | 13 | 11 | 1201 | 28 | 14 | 1191 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial Q（Qb），veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus，Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate，veh／h | 19 | 14 |  | 1278 | 30 | 15 | 1267 |  |
| Adj No．of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.94 | 0.94 |  | 0.94 | 0.94 | 0.94 | 0.94 |  |
| Percent Heavy Veh，\％ | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap，veh／h | 55 | 49 |  | 2845 | 1241 | 31 | 3081 |  |
| Arrive On Green | 0.03 | 0.03 |  | 0.80 | 0.80 | 0.02 | 0.87 |  |
| Sat Flow，veh／h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume（v），veh／h | 19 | 14 |  | 1278 | 30 | 15 | 1267 |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve（g＿s），s | 1.0 | 0.8 |  | 10.1 | 0.4 | 0.8 | 6.6 |  |
| Cycle Q Clear（g＿c），s | 1.0 | 0.8 |  | 10.1 | 0.4 | 0.8 | 6.6 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap（c），veh／h | 55 | 49 |  | 2845 | 1241 | 31 | 3081 |  |
| V／C Ratio（X） | 0.35 | 0.28 |  | 0.45 | 0.02 | 0.49 | 0.41 |  |
| Avail Cap（c＿a），veh／h | 495 | 442 |  | 2845 | 1241 | 146 | 3081 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter（I） | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay（d），s／veh | 43.4 | 43.3 |  | 2.7 | 1.8 | 44.5 | 1.2 |  |
| Incr Delay（d2），s／veh | 3.7 | 3.1 |  | 0.5 | 0.0 | 11.5 | 0.4 |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \％ile BackOfQ（50\％），veh／ln | 0.5 | 0.4 |  | 5.0 | 0.2 | 0.5 | 3.2 |  |
| LnGrp Delay（d），s／veh | 47.1 | 46.4 |  | 3.3 | 1.8 | 56.0 | 1.6 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol，veh／h | 33 |  |  | 1308 |  |  | 1282 |  |
| Approach Delay，s／veh | 46.8 |  |  | 3.2 |  |  | 2.2 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $G+Y+R c$ ），s | 6.1 | 78.0 |  |  |  | 84.1 |  | 7.3 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 7.5 | 73.5 |  |  |  | 74.5 |  | 25.5 |
| Max Q Clear Time（g＿c＋11），s | 2.8 | 12.1 |  |  |  | 8.6 |  | 3.0 |
| Green Ext Time（p＿c），s | 0.0 | 14.4 |  |  |  | 12.0 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 3.3 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |
| User approved ignoring U－Turning movement． |  |  |  |  |  |  |  |  |

## Appendix G. Opening Year (2030) Highway LOS Worksheets

| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB <br> oro/Sun Valley Dr trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1424 | 1870 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{g}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{* f} \mathrm{HV}, \mathrm{PTSF}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1424 | 1870 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 90.3 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 8.9 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 94.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $v / c$ | 0.84 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 46.4 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1423.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.50 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Toro/Sun Valley Dr trans <br> 3 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2087 | 1880 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2087 | 1880 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 95.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 7.2 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+\mathrm{f}_{\mathrm{np,PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{\mathrm{d}, \mathrm{PTSF}}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.7 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.23 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.7 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2087.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.69 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Toro/Sun Valley Dr trans <br> 30 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1870 | 1424 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br>  $1.3 \mathrm{mi} / \mathrm{h}$ <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>   <br>  $22.4 \mathrm{mi} / \mathrm{h}$ <br>  46.0 ATS |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1870 | 1424 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 94.0 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 8.9 |  |
| Percent time-spent-following, PTSF ${ }_{\text {d }}(\%)=$ BPTSF ${ }_{\mathrm{d}}+\mathrm{f}_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{\text {d,PTSF }} / \mathrm{v}_{\text {d, PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.10 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 46.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1869.6 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.64 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Toro/Sun Valley Dr trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1880 | 2087 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1880 | 2087 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right)$ | 94.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 7.2 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{\mathrm{d}, \mathrm{PTSF}}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.11 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
|  |  |  |
|  |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1880.4 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.64 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB Toro/Sun Valley Dr trans 30 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 801 | 2098 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{vl} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 799 | 2098 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 76.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.6 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 80.5 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
|  | 0.47 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 52.7 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 798.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.21 |  |
| Bicycle level of service (Exhibit 15-4) | c |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $03 / 14 / 22$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Toro/Sun Valley Dr trans <br> 30 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1054 | 2337 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1054 | 2337 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 83.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 14.0 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 88.3 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 0.62 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 44.9 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1054.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.35 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst BM <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Valley Dr/Stan Oaks Dr Itrans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1413 | 1935 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br>  $1.3 \mathrm{mi} / \mathrm{h}$ <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $22.2 \mathrm{mi} / \mathrm{h}$ <br>  45.6 ATS |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\right.$ PHF $\left.^{\star} \mathrm{F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1413 | 1935 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right)$ | 90.2 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 9.3 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 94.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 0.83 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 45.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1413.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.50 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as leve <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | R-133/NB <br> un Valley Dr/Stan Oaks Dr altrans <br> 030 No Build/Alt1-Alt |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | $\square$ <br> Terrain $\square$ Level Grade Length 0.25 mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2135 | 1880 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(v / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | ```Base free-flow speed \({ }^{4}\), BFFS Adj. for lane and shoulder width, \({ }^{4}{ }_{\mathrm{LS}}\) (Exhibit 15-7) Adj. for access points \({ }^{4}\), \(\mathrm{f}_{\mathrm{A}}\) (Exhibit 15-8) Free-flow speed, FFS (FSS=BFFS- Ls \(^{-f_{A}}\) ) Average travel speed, ATS \({ }_{d}=\) FFS- \(0.00776\left(v_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}\) Percent free flow speed, PFFS``` |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} / \mathrm{h}$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>   <br>  $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> $34.0 \mathrm{mi} / \mathrm{h}$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 0.92 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2316 | 1880 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 96.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 7.4 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.36 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1697 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1564 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 34.9 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2130.4 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.70 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1935 | 1413 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1935 | 1413 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 94.5 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 9.3 |  |
| Percent time-spent-following, PTSF ${ }_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.9 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.14 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 45.1 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1934.8 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.66 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1880 | 2130 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1880 | 2130 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\mathrm{d}}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right.$ ) | 94.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 7.4 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.2 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.11 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1880.4 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.64 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as leve <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst BM <br> Agency or Company HDR <br> Date Performed $03 / 14 / 22$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel SR <br> From/To S <br> Jurisdiction C <br> Analysis Year 2030 | -133/NB <br> Valley Dr/Stan Oaks Dr Itrans <br> 30 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | $\square$ <br> Terrain Level Grade Length Peak-hour factor, mi No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 795 | 2163 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ LS (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f_{A}}$ ) <br> Average travel speed, ATS ${ }_{d}=F F S-0.00776\left(v_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br>  $1.3 \mathrm{~m} / \mathrm{h}$ <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ $-\mathrm{f}_{\mathrm{np}, \text { ATS }}$ <br>  $25.2 \mathrm{mi} / \mathrm{h}$ <br> $51.8 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 793 | 2163 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\left.\mathrm{av}_{\mathrm{d}}{ }^{\text {b }}\right)}\right.$ | 76.5 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.3 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{\text {np,PTSF }} *\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+v_{o, \text { PTSF }}\right)$ | 80.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 0.47 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 51.8 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 793.5 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.20 |  |
| Bicycle level of service (Exhibit 15-4) | c |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $03 / 14 / 22$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1054 | 2391 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br>  $1.3 \mathrm{~m} / \mathrm{h}$ <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $21.4 \mathrm{mi} / \mathrm{h}$ <br>  44.0 ATS |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1054 | 2391 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 83.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 14.2 |  |
| Percent time-spent-following, PTSF ${ }_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 88.2 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) <br> Volume to capacity ratio, $v / c$ | F |  |
|  | 0.62 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {( }}$ (Equation 15-11 - Class III only) | 44.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1054.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.35 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit $15-14$ if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Oaks DrLLCAD dwy trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1467 | 1924 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(v / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1467 | 1924 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 90.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 8.9 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 94.8 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 0.86 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 44.9 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1467.4 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.52 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as leve <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Oaks DrLLCAD dwy trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2054 | 1946 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $17.1 \mathrm{mi} / \mathrm{h}$ <br>  $35.2 \%$ |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2054 | 1946 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 95.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 6.7 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.21 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.2 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2054.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.69 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Oaks Dr/LCAD dwy trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1924 | 1467 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(v / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $21.7 \mathrm{mi} / \mathrm{h}$ <br>  44.5 ATS |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1924 | 1467 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 94.6 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 8.9 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.6 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
|  | 1.13 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 44.5 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1923.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.65 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as leve <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Oaks Dr/LCAD dwy trans <br> 30 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1946 | 2054 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $17.1 \mathrm{mi} / \mathrm{h}$ <br>  $35.2 \%$ |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1946 | 2054 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 95.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 6.7 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.4 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.14 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.2 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1945.7 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.66 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $03 / 14 / 22$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Oaks DrLLCAD dwy trans <br> 0 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 822 | 2152 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $25.1 \mathrm{mi} / \mathrm{h}$ <br>  51.5 ATS |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 821 | 2152 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 77.5 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 13.6 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 81.3 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 0.48 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 51.5 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 820.7 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.22 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed O3/14/22 <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To Jurisdiction Analysis Year | 133/SB <br> Oaks Dr/LCAD dwy rans <br> Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi <br> Peak-hour factor, PHF No-passing zone <br> \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ <br> Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1087 | 2304 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{vl} / \mathrm{fHV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls $($ Exhibit 15-7) <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f_{A}}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $\left.\begin{array}{l}50.0 \mathrm{mi} / \mathrm{h} \\ 1.3 \mathrm{mi} / \mathrm{h} \\ 0.0 \mathrm{mi} / \mathrm{h} \\ \\ \\ \\ \\ 0 . A T S\end{array}\right)-\mathrm{f}_{\mathrm{np,ATS}}$ <br> $21.9 \mathrm{mi} / \mathrm{h}$  <br> $44.9 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| $\text { Grade adjustment factor }{ }^{1} \text {, } \mathrm{f}_{\mathrm{g}, \text { PTSF }} \text { (Exhibit 15-16 or Ex 15-17) }$ | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1087 | 2304 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right.$ ) | 84.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.6 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n \mathrm{f}, \mathrm{PTSF}}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 89.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) <br> Volume to capacity ratio, v/c | $F$ |  |
|  | 0.64 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Bicycle Level of Service |  |  |
|  |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1087.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.36 |  |
| Bicycle level of service (Exhibit 15-4) | c |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $\mathrm{v}>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |


| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> AD dwy/Canyon Acres Dr trans <br> 30 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1489 | 1913 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1489 | 1913 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 91.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 8.7 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\mathrm{np,PTSF}}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 94.9 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.88 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 44.7 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1489.1 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.52 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> AD dwy/Canyon Acres Dr trans <br> 30 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width <br>  Segment length, L |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2054 | 1957 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} / \mathrm{h}$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $17.0 \mathrm{mi} / \mathrm{h}$ <br> 35.0 ATS  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2054 | 1957 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 95.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 6.6 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f} \mathrm{n}_{\mathrm{p}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\text {d,PTSF }} / \mathrm{v}_{\text {d,PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.21 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2054.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.69 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> AD dwy/Canyon Acres Dr trans <br> 30 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 | 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.1 | 1.1 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.994 | 0.994 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1925 | 1498 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1913 | 1489 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 94.6 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 8.7 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f} \mathrm{n}_{\mathrm{p}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\text {d,PTSF }} / \mathrm{v}_{\text {d,PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.5 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.13 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1690 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 44.1 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1913.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.65 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> AD dwy/Canyon Acres Dr trans <br> 30 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1957 | 2054 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} / \mathrm{h}$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $17.0 \mathrm{mi} / \mathrm{h}$ <br> 35.0 ATS  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{g}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{* f} \mathrm{HV}, \mathrm{PTSF}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1957 | 2054 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 95.2 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 6.6 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.4 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.15 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1956.5 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.66 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $03 / 14 / 22$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To Jurisdiction Analysis Year | 133/NB <br> D dwy/Canyon Acres Dr rans <br> Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi <br> Peak-hour factor, PHF No-passing zone <br> \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ <br> Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 833 | 2141 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{vl} / \mathrm{fHV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls $($ Exhibit 15-7) <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f_{A}}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} / \mathrm{h}$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $25.1 \mathrm{mi} / \mathrm{h}$ <br> $51.5 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| $\text { Grade adjustment factor }{ }^{1} \text {, } \mathrm{f}_{\mathrm{g}, \text { PTSF }} \text { (Exhibit 15-16 or Ex 15-17) }$ | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 832 | 2141 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right)$ | 77.8 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.7 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+v_{o, \text { PTSF }}\right)$ | 81.6 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) <br> Volume to capacity ratio, v/c | F |  |
|  | 0.49 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Bicycle Level of Service |  |  |
|  |  |  |
| Directional demand flow rate in outside lane, $\mathrm{v}_{\mathrm{OL}}$ (Eq. 15-24) veh/h | 831.5 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.23 |  |
| Bicycle level of service (Exhibit 15-4) | c |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $\mathrm{v}>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |




| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed O3/14/22 <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To Jurisdiction Analysis Year | 133/SB <br> D dwy/Canyon Acres Dr rans <br> Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi <br> Peak-hour factor, PHF No-passing zone <br> \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ <br> Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1098 | 2304 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{vl} / \mathrm{fHV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls $($ Exhibit 15-7) <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f_{A}}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1098 | 2304 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right)$ | 84.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.5 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n \mathrm{f}, \mathrm{PTSF}}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 89.3 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) <br> Volume to capacity ratio, $v / c$ | $F$ |  |
|  | 0.65 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Bicycle Level of Service |  |  |
|  |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1097.8 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.37 |  |
| Bicycle level of service (Exhibit 15-4) | c |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $\mathrm{v}>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |

## Appendix H. Opening Year (2030) Intersection LOS Worksheets

|  | 7 | 4 | 4 | $p$ |  | $\dagger$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | \％ | F | 个个 | F | ${ }^{7}$ | 个个 |  |  |
| Traffic Volume（veh／h） | 815 | 16 | 1045 | 711 | 28 | 1079 |  |  |
| Future Volume（veh／h） | 815 | 16 | 1045 | 711 | 28 | 1079 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow，veh／h／n | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate，veh／h | 858 | 17 | 1100 | 748 | 29 | 1136 |  |  |
| Adj No．of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap，veh／h | 875 | 781 | 1304 | 1364 | 46 | 1528 |  |  |
| Arrive On Green | 0.49 | 0.49 | 0.37 | 0.37 | 0.03 | 0.43 |  |  |
| Sat Flow，veh／h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume（v），veh／h | 858 | 17 | 1100 | 748 | 29 | 1136 |  |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| $Q$ Serve（g＿s），s | 57.0 | 0.7 | 34.2 | 14.9 | 1.9 | 32.2 |  |  |
| Cycle Q Clear（g＿c），s | 57.0 | 0.7 | 34.2 | 14.9 | 1.9 | 32.2 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 875 | 781 | 1304 | 1364 | 46 | 1528 |  |  |
| V／C Ratio（ X ） | 0.98 | 0.02 | 0.84 | 0.55 | 0.63 | 0.74 |  |  |
| Avail Cap（c＿a），veh／h | 880 | 785 | 1304 | 1364 | 74 | 1528 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay（d），s／veh | 29.8 | 15.6 | 34.7 | 2.2 | 57.9 | 28.5 |  |  |
| Incr Delay（d2），s／veh | 25.5 | 0.0 | 6.8 | 1.6 | 13.5 | 3.3 |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \％ile BackOfQ（50\％），veh／ln | 34.1 | 0.3 | 17.9 | 25.3 | 1.1 | 16.3 |  |  |
| LnGrp Delay（d），s／veh | 55.3 | 15.6 | 41.5 | 3.8 | 71.4 | 31.9 |  |  |
| LnGrp LOS | E | B | D | A | E | C |  |  |
| Approach Vol，veh／h | 875 |  | 1848 |  |  | 1165 |  |  |
| Approach Delay，s／veh | 54.5 |  | 26.2 |  |  | 32.8 |  |  |
| Approach LOS | D |  | C |  |  | C |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 7.6 | 48.7 |  |  |  | 56.3 |  | 63.7 |
| Change Period（ $Y+R \mathrm{Rc}$ ），$s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.0 | 42.0 |  |  |  | 51.5 |  | 59.5 |
| Max Q Clear Time（g＿ct1），s | 3.9 | 36.2 |  |  |  | 34.2 |  | 59.0 |
| Green Ext Time（p＿c），s | 0.0 | 4.3 |  |  |  | 7.1 |  | 0.2 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 34.6 |  |  |  |  |  |
| HCM 2010 Ctrl DelayHCM 2010 LOS |  |  | C |  |  |  |  |  |



|  |  | $4$ |  |  | $\pm$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | ${ }^{7}$ | F' | 44 | 「' | ${ }^{1}$ | 44 |  |  |
| Traffic Volume (veh/h) | 815 | 16 | 1232 | 711 | 28 | 1208 |  |  |
| Future Volume (veh/h) | 815 | 16 | 1232 | 711 | 28 | 1208 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial Q $(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate, veh/h | 858 | 17 | 1297 | 748 | 29 | 1272 |  |  |
| Adj No. of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap, veh/h | 832 | 743 | 1389 | 1364 | 46 | 1613 |  |  |
| Arrive On Green | 0.47 | 0.47 | 0.39 | 0.39 | 0.03 | 0.46 |  |  |
| Sat Flow, veh/h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume(v), veh/h | 858 | 17 | 1297 | 748 | 29 | 1272 |  |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| Q Serve(g_s), $s$ | 56.3 | 0.7 | 42.2 | 14.9 | 1.9 | 36.6 |  |  |
| Cycle Q Clear(g_c), s | 56.3 | 0.7 | 42.2 | 14.9 | 1.9 | 36.6 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap(c), veh/h | 832 | 743 | 1389 | 1364 | 46 | 1613 |  |  |
| V/C Ratio(X) | 1.03 | 0.02 | 0.93 | 0.55 | 0.63 | 0.79 |  |  |
| Avail Cap(c_a), veh/h | 832 | 743 | 1389 | 1364 | 74 | 1613 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 31.9 | 17.1 | 35.0 | 2.2 | 57.9 | 27.7 |  |  |
| Incr Delay (d2), s/veh | 39.4 | 0.0 | 11.7 | 0.5 | 13.5 | 4.0 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/In | 36.6 | 0.3 | 22.8 | 24.9 | 1.1 | 18.7 |  |  |
| LnGrp Delay(d),s/veh | 71.2 | 17.1 | 46.7 | 2.6 | 71.4 | 31.7 |  |  |
| LnGrp LOS | F | B | D | A | E | C |  |  |
| Approach Vol, veh/h | 875 |  | 2045 |  |  | 1301 |  |  |
| Approach Delay, s/veh | 70.2 |  | 30.6 |  |  | 32.6 |  |  |
| Approach LOS | E |  | C |  |  | C |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 7.6 | 51.6 |  |  |  | 59.2 |  | 60.8 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 5.0 | 45.2 |  |  |  | 54.7 |  | 56.3 |
| Max Q Clear Time (g_c+l1), s | 3.9 | 44.2 |  |  |  | 38.6 |  | 58.3 |
| Green Ext Time (p_c), s | 0.0 | 0.9 |  |  |  | 8.5 |  | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 39.4 |  |  |  |  |  |
| $\text { HCM } 2010 \text { LOS }$ |  |  | D |  |  |  |  |  |


|  |  | $4$ |  |  | $\pm$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | ${ }^{7}$ | F゙ | 44 | F゙ | ${ }^{7}$ | 中4 |  |  |
| Traffic Volume（veh／h） | 680 | 43 | 1012 | 824 | 41 | 1090 |  |  |
| Future Volume（veh／h） | 680 | 43 | 1012 | 824 | 41 | 1090 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate，veh／h | 716 | 45 | 1065 | 867 | 43 | 1147 |  |  |
| Adj No．of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap，veh／h | 757 | 676 | 1480 | 1338 | 59 | 1741 |  |  |
| Arrive On Green | 0.43 | 0.43 | 0.42 | 0.42 | 0.03 | 0.49 |  |  |
| Sat Flow，veh／h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume（v），veh／h | 716 | 45 | 1065 | 867 | 43 | 1147 |  |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| Q Serve（g＿s），s | 43.0 | 1.9 | 27.7 | 20.8 | 2.7 | 27.0 |  |  |
| Cycle Q Clear（g＿c），s | 43.0 | 1.9 | 27.7 | 20.8 | 2.7 | 27.0 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 757 | 676 | 1480 | 1338 | 59 | 1741 |  |  |
| V／C Ratio（X） | 0.95 | 0.07 | 0.72 | 0.65 | 0.73 | 0.66 |  |  |
| Avail Cap（c＿a），veh／h | 905 | 808 | 1480 | 1338 | 82 | 1741 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay（d），s／veh | 30.5 | 18.7 | 26.8 | 2.9 | 53.1 | 21.1 |  |  |
| Incr Delay（d2），s／veh | 16.6 | 0.0 | 1.7 | 1.1 | 18.7 | 2.0 |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \％ile BackOfQ（50\％），veh／ln | 24.4 | 0.8 | 13.8 | 26.7 | 1.6 | 13.5 |  |  |
| LnGrp Delay（d），s／veh | 47.1 | 18.8 | 28.5 | 4.0 | 71.7 | 23.1 |  |  |
| LnGrp LOS | D | B | C | A | E | C |  |  |
| Approach Vol，veh／h | 761 |  | 1932 |  |  | 1190 |  |  |
| Approach Delay，s／veh | 45.4 |  | 17.5 |  |  | 24.9 |  |  |
| Approach LOS | D |  | B |  |  | C |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 8.2 | 50.8 |  |  |  | 59.0 |  | 51.8 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.1 | 44.9 |  |  |  | 54.5 |  | 56.5 |
| Max Q Clear Time（g＿c＋11），s | 4.7 | 29.7 |  |  |  | 29.0 |  | 45.0 |
| Green Ext Time（p＿c），s | 0.0 | 10.0 |  |  |  | 9.6 |  | 2.3 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 25.3 |  |  |  |  |  |
| $\text { HCM } 2010 \text { LOS }$ |  |  | C |  |  |  |  |  |

HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 22.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\mathbf{T}$ |  | l | 个 |
| Traffic Vol, veh/h | 20 | 146 | 1610 | 30 | 168 | 1726 |
| Future Vol, veh/h | 20 | 146 | 1610 | 30 | 168 | 1726 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 151 | 1660 | 31 | 173 | 1779 |



## Notes

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy



HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 30 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\mathbf{T}$ |  | A | 4中 |
| Traffic Vol, veh/h | 20 | 146 | 1873 | 30 | 168 | 1931 |
| Future Vol, veh/h | 20 | 146 | 1873 | 30 | 168 | 1931 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 151 | 1931 | 31 | 173 | 1991 |



HCMLOS F

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -74 | 294 | - |
| HCM Lane V/C Ratio | - | -2.313 | 0.589 | - |
| HCM Control Delay (s) | - | $\$ 720.3$ | 33.4 | - |
| HCM Lane LOS | - | - | F | D |
| HCM 95th \%tile Q(veh) | - | - | 16.1 | 3.5 |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+:$ Computation Not Defined $\quad *:$ All major volume in platoon

HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0.9 |  |  |  |  |  |  |
| Movement V | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * ${ }^{\prime}$ |  | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 中4 |
| Traffic Vol, veh/h | 11 | 60 | 1794 | 10 | 51 | 1737 |
| Future Vol, veh/h | 11 | 60 | 1794 | 10 | 51 | 1737 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 62 | 1849 | 10 | 53 | 1791 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 4 | 6 | 1444 | 1 | 2 | 1694 |
| Future Vol, veh/h | 4 | 6 | 1444 | 1 | 2 | 1694 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 7 | 1570 | 1 | 2 | 1841 |


| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3416 | 1571 | 0 | 0 | 1571 | 0 |  |
| Stage 1 | 1571 | - | - | - | - | - |  |
| Stage 2 | 1845 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - |  | 2.218 | - |  |
| Pot Cap-1 Maneuver | 8 | 136 | - | - | 420 | - |  |
| Stage 1 | 188 | - | - | - | - | - |  |
| Stage 2 | 137 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 8 | 136 | - | - | 420 | - |  |
| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |  |
| Stage 1 | 188 | - | - | - | - | - |  |
| Stage 2 | 136 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 44 |  | 0 |  | 0 |  |  |
| HCM LOS | E |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBT | NBR | BLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 103 | 420 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.106 | 0.005 | - |  |
| HCM Control Delay (s) |  | - | - | 44 | 13.6 | - |  |
| HCM Lane LOS |  | - | - | E | B | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 2 | 2 | 1644 | 6 | 2 | 1494 |
| Future Vol, veh/h | 2 | 2 | 1644 | 6 | 2 | 1494 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 2 | 1787 | 7 | 2 | 1624 |


| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3419 | 1791 | 0 | 0 | 1794 | 0 |  |
| Stage 1 | 1791 | - | - | - | - | - |  |
| Stage 2 | 1628 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - |  | 2.218 | - |  |
| Pot Cap-1 Maneuver | 8 | 100 | - | - | 344 | - |  |
| Stage 1 | 146 | - | - | - | - | - |  |
| Stage 2 | 176 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 8 | 100 | - | - | 344 | - |  |
| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |  |
| Stage 1 | 146 | - | - | - | - | - |  |
| Stage 2 | 175 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 49.1 |  | 0 |  | 0 |  |  |
| HCM LOS | E |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBT | NBRV | BLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 86 | 344 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.051 | 0.006 | - |  |
| HCM Control Delay (s) |  | - | - | 49.1 | 15.5 | - |  |
| HCM Lane LOS |  | - | - | E | C | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\mathbf{T}$ | $\boldsymbol{f}$ |  |  | 个中 |
| Traffic Vol, veh/h | 0 | 10 | 1703 | 3 | 0 | 1901 |
| Future Vol, veh/h | 0 | 10 | 1703 | 3 | 0 | 1901 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 11 | 1851 | 3 | 0 | 2066 |



|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection |  |  |  |  |  |  |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | $\mathbf{r}$ |  | $\mathbf{4}$ | $\mathbf{r}$ | a | 4 |
| Traffic Vol, veh/h | 5 | 5 | 1645 | 6 | 5 | 1491 |
| Future Vol, veh/h | 5 | 5 | 1645 | 6 | 5 | 1491 |
| Conflicting Peds, \#/hr | 0 | 5 | 0 | 5 | 5 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 165 | 205 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 5 | 1696 | 6 | 5 | 1537 |


| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3248 | 1706 | 0 | 0 | 1707 | 0 |  |
| Stage 1 | 1701 | - | - | - | - | - |  |
| Stage 2 | 1547 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 10 | 113 | - | - | 372 | - |  |
| Stage 1 | 162 | - | - | - | - | - |  |
| Stage 2 | 193 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 10 | 112 | - | - | 370 | - |  |
| Mov Cap-2 Maneuver | 84 | - | - | - | - | - |  |
| Stage 1 | 161 | - | - | - | - | - |  |
| Stage 2 | 190 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 47 |  | 0 |  | 0 |  |  |
| HCM LOS | E |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBT | NBRV | BLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 96 | 370 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.107 | 0.014 | - |  |
| HCM Control Delay (s) |  | - | - | 47 | 14.9 | - |  |
| HCM Lane LOS |  | - | - | E | B | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\mathbf{7}$ | 个 | $\mathbf{F}$ |  | 个中 |
| Traffic Vol，veh／h | 0 | 25 | 1681 | 30 | 0 | 1901 |
| Future Vol，veh／h | 0 | 25 | 1681 | 30 | 0 | 1901 |
| Conflicting Peds，\＃／hr | 0 | 5 | 0 | 5 | 5 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | 165 | - | - |
| Veh in Median Storage，\＃ | 0 | - | 0 | - | - | 0 |
| Grade，\％ | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 26 | 1733 | 31 | 0 | 1960 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



HCM 2010 TWSC
5: Laguna Cyn Rd \& Stan Oaks Dr

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\uparrow$ |  | 1 | 个 |
| Traffic Vol, veh/h | 4 | 6 | 1439 | 1 | 2 | 1691 |
| Future Vol, veh/h | 4 | 6 | 1439 | 1 | 2 | 1691 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 7 | 1564 | 1 | 2 | 1838 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3407 | 1565 | 0 | 0 | 1565 | 0 |
| Stage 1 | 1565 | - | - | - | - | - |
| Stage 2 | 1842 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 |  | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 8 | 137 | - | - | 422 | - |
| Stage 1 | 189 | - | - | - | - | - |
| Stage 2 | 138 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 8 | 137 | - | - | 422 | - |
| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |
| Stage 1 | 189 | - | - | - | - | - |
| Stage 2 | 137 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 43.6 |  | 0 |  | 0 |  |
| HCM LOS | E |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NB | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 104 | 422 | - |
| HCM Lane V/C Ratio |  | - | - | 0.105 | 0.005 | - |
| HCM Control Delay (s) |  | - | - | 43.6 | 13.6 | - |
| HCM Lane LOS |  | - | - | E | B | - |
| HCM 95th \%tile Q(veh) |  | - |  | 0.3 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y |  | $\boldsymbol{F}$ |  | 7 | 4 |
| Traffic Vol, veh/h | 3 | 2 | 1649 | 6 | 2 | 1494 |
| Future Vol, veh/h | 3 | 2 | 1649 | 6 | 2 | 1494 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 2 | 1792 | 7 | 2 | 1624 |


| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3424 | 1796 | 0 | 0 | 1799 | 0 |  |
| Stage 1 | 1796 | - | - | - | - | - |  |
| Stage 2 | 1628 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - |  | 2.218 | - |  |
| Pot Cap-1 Maneuver | 8 | 100 | - | - | 343 | - |  |
| Stage 1 | 145 | - | - | - | - | - |  |
| Stage 2 | 176 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 8 | 100 | - | - | 343 | - |  |
| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |  |
| Stage 1 | 145 | - | - | - | - | - |  |
| Stage 2 | 175 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 50.8 |  | 0 |  | 0 |  |  |
| HCM LOS | F |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBT | NBR | BLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 84 | 343 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.065 | 0.006 | - |  |
| HCM Control Delay (s) |  | - | - | 50.8 | 15.6 | - |  |
| HCM Lane LOS |  | - | - | F | C | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\mathbf{r}$ | $\mathbf{T}$ |  |  | 个中 |
| Traffic Vol, veh/h | 0 | 10 | 1701 | 3 | 0 | 1901 |
| Future Vol, veh/h | 0 | 10 | 1701 | 3 | 0 | 1901 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 11 | 1849 | 3 | 0 | 2066 |



|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection |  |  |  |  |  |  |




| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 3403 | 1558 | 0 | 0 | 1559 | 0 |  |
| Stage 1 | 1558 | - | - | - | - | - |  |
| Stage 2 | 1845 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - |  | 2.218 | - |  |
| Pot Cap-1 Maneuver | 8 | 139 | - | - | 424 | - |  |
| Stage 1 | 191 | - | - | - | - | - |  |
| Stage 2 | 137 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 8 | 139 | - | - | 424 | - |  |
| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |  |
| Stage 1 | 191 | - | - | - | - | - |  |
| Stage 2 | 136 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 45.9 |  | 0 |  | 0 |  |  |
| HCM LOS | E |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBT | NBRL | VBLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 103 | 424 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.148 | 0.008 | - |  |
| HCM Control Delay (s) |  | - | - | 45.9 | 13.6 | - |  |
| HCM Lane LOS |  | - | - | E | B | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.5 | 0 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |







|  | 4 |  | 4 |  | $\dagger$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | ${ }^{7}$ | 4 | $\uparrow$ |  |  |  |
| Traffic Volume (veh/h) | 55 | 45 | 52 | 1379 | 1656 | 42 |  |  |
| Future Volume (veh/h) | 55 | 45 | 52 | 1379 | 1656 | 42 |  |  |
| Number | 7 | 14 | 5 | 2 | 6 | 16 |  |  |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |  |  | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1900 | 1863 | 1863 | 1863 | 1900 |  |  |
| Adj Flow Rate, veh/h | 60 | 49 | 57 | 1499 | 1800 | 46 |  |  |
| Adj No. of Lanes | 0 | 0 | 1 | 1 | 1 | 0 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Percent Heavy Veh, \% | 0 | 0 | 2 | 2 | 2 | 2 |  |  |
| Cap, veh/h | 74 | 60 | 198 | 1574 | 1258 | 32 |  |  |
| Arrive On Green | 0.08 | 0.08 | 0.11 | 0.84 | 0.70 | 0.70 |  |  |
| Sat Flow, veh/h | 919 | 750 | 1774 | 1863 | 1808 | 46 |  |  |
| Grp Volume(v), veh/h | 110 | 0 | 57 | 1499 | 0 | 1846 |  |  |
| Grp Sat Flow(s),veh/h/ln | 1684 | 0 | 1774 | 1863 | 0 | 1855 |  |  |
| Q Serve(g_s), s | 7.7 | 0.0 | 3.5 | 76.7 | 0.0 | 83.5 |  |  |
| Cycle Q Clear(g_c), s | 7.7 | 0.0 | 3.5 | 76.7 | 0.0 | 83.5 |  |  |
| Prop In Lane | 0.55 | 0.45 | 1.00 |  |  | 0.02 |  |  |
| Lane Grp Cap(c), veh/h | 135 | 0 | 198 | 1574 | 0 | 1290 |  |  |
| V/C Ratio(X) | 0.82 | 0.00 | 0.29 | 0.95 | 0.00 | 1.43 |  |  |
| Avail Cap(c_a), veh/h | 253 | 0 | 198 | 1574 | 0 | 1290 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 54.3 | 0.0 | 48.9 | 7.4 | 0.0 | 18.3 |  |  |
| Incr Delay (d2), s/veh | 11.2 | 0.0 | 0.8 | 13.9 | 0.0 | 198.2 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 4.0 | 0.0 | 1.8 | 44.0 | 0.0 | 113.0 |  |  |
| LnGrp Delay(d),s/veh | 65.6 | 0.0 | 49.7 | 21.3 | 0.0 | 216.5 |  |  |
| LnGrp LOS | E |  | D | C |  | F |  |  |
| Approach Vol, veh/h | 110 |  |  | 1556 | 1846 |  |  |  |
| Approach Delay, s/veh | 65.6 |  |  | 22.3 | 216.5 |  |  |  |
| Approach LOS | E |  |  | C | F |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 105.9 |  | 14.1 | 17.9 | 88.0 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 4.5 |  | 4.5 | 4.5 | 4.5 |  |  |
| Max Green Setting (Gmax), s |  | 93.0 |  | 18.0 | 5.0 | 83.5 |  |  |
| Max Q Clear Time (g_c+11), s |  | 78.7 |  | 9.7 | 5.5 | 85.5 |  |  |
| Green Ext Time (p_c), s |  | 11.4 |  | 0.1 | 0.0 | 0.0 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 125.7 |  |  |  |  |  |
| HCM 2010 LOS |  |  | F |  |  |  |  |  |


|  | 4 |  | 4 |  | $\frac{1}{1}$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | * |  | ${ }^{7}$ | 4 | $\uparrow$ |  |  |  |
| Traffic Volume (veh/h) | 13 | 19 | 4 | 1647 | 1488 | 10 |  |  |
| Future Volume (veh/h) | 13 | 19 | 4 | 1647 | 1488 | 10 |  |  |
| Number | 7 | 14 | 5 | 2 | 6 | 16 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |  |  | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1900 | 1863 | 1863 | 1863 | 1900 |  |  |
| Adj Flow Rate, veh/h | 14 | 21 | 4 | 1790 | 1617 | 11 |  |  |
| Adj No. of Lanes | 0 | 0 | 1 | 1 | 1 | 0 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Percent Heavy Veh, \% | 0 | 0 | 2 | 2 | 2 | 2 |  |  |
| Cap, veh/h | 20 | 30 | 9 | 1646 | 1544 | 11 |  |  |
| Arrive On Green | 0.03 | 0.03 | 0.01 | 0.88 | 0.84 | 0.84 |  |  |
| Sat Flow, veh/h | 645 | 968 | 1774 | 1863 | 1848 | 13 |  |  |
| Grp Volume(v), veh/h | 36 | 0 | 4 | 1790 | 0 | 1628 |  |  |
| Grp Sat Flow(s),veh/h/ln | 1660 | 0 | 1774 | 1863 | 0 | 1861 |  |  |
| Q Serve(g_s), s | 2.3 | 0.0 | 0.2 | 93.0 | 0.0 | 87.9 |  |  |
| Cycle Q Clear(g_c), s | 2.3 | 0.0 | 0.2 | 93.0 | 0.0 | 87.9 |  |  |
| Prop In Lane | 0.39 | 0.58 | 1.00 |  |  | 0.01 |  |  |
| Lane Grp Cap(c), veh/h | 51 | 0 | 9 | 1646 | 0 | 1555 |  |  |
| V/C Ratio(X) | 0.70 | 0.00 | 0.43 | 1.09 | 0.00 | 1.05 |  |  |
| Avail Cap(c_a), veh/h | 284 | 0 | 84 | 1646 | 0 | 1555 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 50.5 | 0.0 | 52.2 | 6.1 | 0.0 | 8.7 |  |  |
| Incr Delay (d2), s/veh | 15.9 | 0.0 | 28.4 | 50.1 | 0.0 | 36.3 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/In | 1.3 | 0.0 | 0.2 | 67.7 | 0.0 | 58.9 |  |  |
| LnGrp Delay(d),s/veh | 66.4 | 0.0 | 80.6 | 56.2 | 0.0 | 44.9 |  |  |
| LnGrp LOS | E |  | F | F |  | F |  |  |
| Approach Vol, veh/h | 36 |  |  | 1794 | 1628 |  |  |  |
| Approach Delay, s/veh | 66.4 |  |  | 56.3 | 44.9 |  |  |  |
| Approach LOS | E |  |  | E | D |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 97.5 |  | 7.8 | 5.1 | 92.4 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ |  | 4.5 |  | 4.5 | 4.5 | 4.5 |  |  |
| Max Green Setting (Gmax), s |  | 93.0 |  | 18.0 | 5.0 | 83.5 |  |  |
| Max Q Clear Time (g_c+l1), s |  | 95.0 |  | 4.3 | 2.2 | 89.9 |  |  |
| Green Ext Time (p_c), s |  | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 51.0 |  |  |  |  |  |
| HCM 2010 LOS |  |  | D |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | - | 1033 | - | 0 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.93 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.319 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 230 | 0 | - | - | - |
| $\quad$ Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | - | 230 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 33.9 | 0 | 0 |
| HCM LOS | D |  |  |
|  |  |  |  |
|  |  |  |  |
| Minor Lane/Major Mvmt | NBT EBLn 1 | SBT | SBR |
| Capacity (veh/h) | -230 | - | - |
| HCM Lane V/C Ratio | -0.473 | - | - |
| HCM Control Delay (s) | - | 33.9 | - |
| HCM Lane LOS | - | - |  |
| HCM 95th \%tile Q(veh) | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | - | 1766 | - | 0 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.23 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.319 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 103 | 0 | - | - | - |
| $\quad$ Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | - | 103 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


|  | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Approach | 0 | 0 |  |
| HCM Control Delay, s | 56.8 |  | 0 |
|  |  |  |  |
| HCM LOS |  |  |  |
|  |  |  |  |
| Minor Lane/Major Mvmt | NBT EBLn | SBT | SBR |
| Capacity (veh/h) | -103 | - | - |
| HCM Lane V/C Ratio | -0.338 | - | - |
| HCM Control Delay (s) | -56.8 | - | - |
| HCM Lane LOS | - | F | - |
| HCM 95th \%tile Q(veh) | - | - |  |

HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 10.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | T | $\mathbf{T}$ |  | $\mathbf{4}$ | 4 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 80 | 66 | 76 | 1351 | 1639 | 62 |
| Future Vol, veh/h | 80 | 66 | 76 | 1351 | 1639 | 62 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 100 | - | - | 300 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 87 | 72 | 83 | 1468 | 1782 | 67 |



HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot



HCM 2010 TWSC
8：Laguna Cyn Rd \＆Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 17.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{4}$ | 4 | 中4 | 「 |
| Traffic Vol，veh／h | 80 | 66 | 76 | 1615 | 1845 | 62 |
| Future Vol，veh／h | 80 | 66 | 76 | 1615 | 1845 | 62 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Star | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | － | None | － | None | － | None |
| Storage Length | 0 | 0 | 100 | － | － | 300 |
| Veh in Median Storage，\＃ | \＃ 0 | － | － | 0 | 0 | － |
| Grade，\％ | 0 | － | － | 0 | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 87 | 72 | 83 | 1755 | 2005 | 67 |



HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 | $\mathbf{T}$ | $\mathbf{1}$ | 个 | 个 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 19 | 29 | 6 | 1834 | 1634 | 15 |
| Future Vol, veh/h | 19 | 29 | 6 | 1834 | 1634 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | 100 | - | - | 300 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 32 | 7 | 1993 | 1776 | 16 |



|  |  | $4$ | $\dagger 1$ |  |  |  | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 7 | $\square$ | 44 | 「 | ${ }^{1 /}$ | 蚛 |  |
| Traffic Volume (veh/h) | 40 | 16 | 18 | 1555 | 15 | 16 | 1511 |  |
| Future Volume (veh/h) | 40 | 16 | 18 | 1555 | 15 | 16 | 1511 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 42 | 17 |  | 1620 | 16 | 17 | 1574 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 74 | 66 |  | 2814 | 1228 | 34 | 3051 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.79 | 0.79 | 0.02 | 0.86 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 42 | 17 |  | 1620 | 16 | 17 | 1574 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 2.2 | 1.0 |  | 16.2 | 0.2 | 0.9 | 10.4 |  |
| Cycle Q Clear(g_c), s | 2.2 | 1.0 |  | 16.2 | 0.2 | 0.9 | 10.4 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 74 | 66 |  | 2814 | 1228 | 34 | 3051 |  |
| V/C Ratio(X) | 0.57 | 0.26 |  | 0.58 | 0.01 | 0.50 | 0.52 |  |
| Avail Cap(c_a), veh/h | 483 | 431 |  | 2814 | 1228 | 123 | 3051 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 44.1 | 43.5 |  | 3.6 | 2.0 | 45.5 | 1.6 |  |
| Incr Delay (d2), s/veh | 6.6 | 2.0 |  | 0.9 | 0.0 | 11.0 | 0.6 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 1.2 | 0.5 |  | 8.0 | 0.1 | 0.5 | 5.1 |  |
| LnGrp Delay(d),s/veh | 50.6 | 45.5 |  | 4.5 | 2.0 | 56.6 | 2.2 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 59 |  |  | 1636 |  |  | 1591 |  |
| Approach Delay, s/veh | 49.2 |  |  | 4.5 |  |  | 2.8 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 6.3 | 79.0 |  |  |  | 85.3 |  | 8.4 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 6.5 | 74.5 |  |  |  | 74.5 |  | 25.5 |
| Max Q Clear Time (g_c+l1), s | 2.9 | 18.2 |  |  |  | 12.4 |  | 4.2 |
| Green Ext Time (p_c), s | 0.0 | 21.6 |  |  |  | 17.7 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 4.5 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | 7 | 4 | 71 |  | 7 |  | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 7 | $\square$ | 44 | F' | ${ }^{7}$ | 中4 |  |
| Traffic Volume (veh/h) | 20 | 16 | 0 | 1473 | 30 | 20 | 1488 |  |
| Future Volume (veh/h) | 20 | 16 | 0 | 1473 | 30 | 20 | 1488 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 21 | 17 |  | 1534 | 31 | 21 | 1550 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 60 | 53 |  | 2828 | 1234 | 40 | 3079 |  |
| Arrive On Green | 0.03 | 0.03 |  | 0.80 | 0.80 | 0.02 | 0.87 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 21 | 17 |  | 1534 | 31 | 21 | 1550 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 1.1 | 1.0 |  | 14.3 | 0.4 | 1.1 | 9.5 |  |
| Cycle Q Clear(g_c), s | 1.1 | 1.0 |  | 14.3 | 0.4 | 1.1 | 9.5 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 60 | 53 |  | 2828 | 1234 | 40 | 3079 |  |
| V/C Ratio(X) | 0.35 | 0.32 |  | 0.54 | 0.03 | 0.53 | 0.50 |  |
| Avail Cap(c_a), veh/h | 485 | 433 |  | 2828 | 1234 | 124 | 3079 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 44.1 | 44.0 |  | 3.3 | 1.9 | 45.1 | 1.4 |  |
| Incr Delay (d2), s/veh | 3.5 | 3.4 |  | 0.8 | 0.0 | 10.3 | 0.6 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 0.6 | 0.5 |  | 7.1 | 0.2 | 0.7 | 4.6 |  |
| LnGrp Delay(d),s/veh | 47.6 | 47.4 |  | 4.1 | 2.0 | 55.4 | 2.0 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 38 |  |  | 1565 |  |  | 1571 |  |
| Approach Delay, s/veh | 47.5 |  |  | 4.0 |  |  | 2.7 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 6.6 | 79.0 |  |  |  | 85.6 |  | 7.6 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 6.5 | 74.5 |  |  |  | 76.0 |  | 25.5 |
| Max Q Clear Time (g_c+11), s | 3.1 | 16.3 |  |  |  | 11.5 |  | 3.1 |
| Green Ext Time (p_c), s | 0.0 | 19.9 |  |  |  | 17.3 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 3.9 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | 7 | $4$ | $\dagger 1$ |  |  |  | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 7 | $\dagger$ | 44 | 「7 | ${ }^{7}$ | 中4 |  |
| Traffic Volume (veh/h) | 40 | 16 | 18 | 1742 | 15 | 93 | 1640 |  |
| Future Volume (veh/h) | 40 | 16 | 18 | 1742 | 15 | 93 | 1640 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial Q $(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.97 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 42 | 17 |  | 1815 | 16 | 97 | 1708 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 74 | 66 |  | 2643 | 1153 | 124 | 3057 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.75 | 0.75 | 0.07 | 0.86 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 42 | 17 |  | 1815 | 16 | 97 | 1708 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 2.2 | 1.0 |  | 25.3 | 0.3 | 5.1 | 12.1 |  |
| Cycle Q Clear(g_c), s | 2.2 | 1.0 |  | 25.3 | 0.3 | 5.1 | 12.1 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 74 | 66 |  | 2643 | 1153 | 124 | 3057 |  |
| V/C Ratio(X) | 0.57 | 0.26 |  | 0.69 | 0.01 | 0.79 | 0.56 |  |
| Avail Cap(c_a), veh/h | 467 | 416 |  | 2643 | 1153 | 196 | 3057 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 44.7 | 44.1 |  | 6.3 | 3.1 | 43.5 | 1.7 |  |
| Incr Delay (d2), s/veh | 6.8 | 2.1 |  | 1.5 | 0.0 | 10.4 | 0.7 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 1.2 | 0.5 |  | 12.6 | 0.1 | 2.9 | 6.0 |  |
| LnGrp Delay(d),s/veh | 51.5 | 46.2 |  | 7.7 | 3.1 | 53.9 | 2.4 |  |
| LnGrp LOS | D | D |  | A | A | D | A |  |
| Approach Vol, veh/h | 59 |  |  | 1831 |  |  | 1805 |  |
| Approach Delay, s/veh | 50.0 |  |  | 7.7 |  |  | 5.2 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 11.1 | 75.5 |  |  |  | 86.6 |  | 8.4 |
| Change Period ( $Y+R \mathrm{c}$ ), $s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 10.5 | 71.0 |  |  |  | 76.0 |  | 25.0 |
| Max Q Clear Time (g_c+11), s | 7.1 | 27.3 |  |  |  | 14.1 |  | 4.2 |
| Green Ext Time (p_c), s | 0.1 | 23.6 |  |  |  | 24.5 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 7.2 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | $\bigcirc$ | 4 | 7 |  | $p$ | $\pm$ | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 7 | $\square$ | 44 | 7 | ${ }^{7}$ | 44 |  |
| Traffic Volume (veh/h) | 20 | 16 | 0 | 1650 | 30 | 45 | 1605 |  |
| Future Volume (veh/h) | 20 | 16 | 0 | 1650 | 30 | 45 | 1605 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 21 | 17 |  | 1719 | 31 | 47 | 1672 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 60 | 53 |  | 2772 | 1209 | 67 | 3077 |  |
| Arrive On Green | 0.03 | 0.03 |  | 0.78 | 0.78 | 0.04 | 0.87 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 21 | 17 |  | 1719 | 31 | 47 | 1672 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 1.1 | 1.0 |  | 19.0 | 0.4 | 2.4 | 10.9 |  |
| Cycle Q Clear(g_c), s | 1.1 | 1.0 |  | 19.0 | 0.4 | 2.4 | 10.9 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 60 | 53 |  | 2772 | 1209 | 67 | 3077 |  |
| V/C Ratio(X) | 0.35 | 0.32 |  | 0.62 | 0.03 | 0.70 | 0.54 |  |
| Avail Cap(c_a), veh/h | 477 | 426 |  | 2772 | 1209 | 166 | 3077 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 43.9 | 43.9 |  | 4.2 | 2.2 | 44.2 | 1.5 |  |
| Incr Delay (d2), s/veh | 3.5 | 3.4 |  | 1.1 | 0.0 | 12.4 | 0.7 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 0.6 | 0.5 |  | 9.5 | 0.2 | 1.4 | 5.4 |  |
| LnGrp Delay(d),s/veh | 47.4 | 47.3 |  | 5.3 | 2.3 | 56.6 | 2.2 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 38 |  |  | 1750 |  |  | 1719 |  |
| Approach Delay, s/veh | 47.3 |  |  | 5.2 |  |  | 3.7 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 8.0 | 77.3 |  |  |  | 85.3 |  | 7.6 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 8.7 | 72.8 |  |  |  | 76.5 |  | 25.0 |
| Max Q Clear Time (g_c+11), s | 4.4 | 21.0 |  |  |  | 12.9 |  | 3.1 |
| Green Ext Time (p_c), s | 0.0 | 23.5 |  |  |  | 23.7 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 4.9 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |

## Appendix I. Horizon Year (2050) Highway LOS Worksheets

| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Toro/Sun Valley Dr trans <br> 0 No Build/Altt-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1826 | 2511 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1826 | 2511 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 94.3 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 9.3 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.2 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.07 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 29.8 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1826.1 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.63 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB Toro/Sun Valley Dr trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width  <br>  Segment length, $\mathrm{L}_{\mathrm{t}}$  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2853 | 2511 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} h$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br> $0.5 \mathrm{mi} / \mathrm{h}$ <br> 13.4 |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2853 | 2511 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 98.4 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 7.4 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $v / c$ | 1.68 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\text {d,PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS (Equation 15-11-Class III only) | 13.4 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2853.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.85 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh $/ \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/SB Toro/Sun Valley Dr rans 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Sane width <br>    |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2511 | 1826 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{g}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{* f} \mathrm{HV}, \mathrm{PTSF}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2511 | 1826 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 97.6 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 9.3 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.48 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 29.8 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2510.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.79 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Toro/Sun Valley Dr trans <br> 50 No Build/Altt 1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2511 | 2853 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$ <br> $0.0 \mathrm{mi} / \mathrm{h}$ <br>  <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ <br>  $\mathrm{f}_{\mathrm{np}, \text { ATS }}$$\quad$$48.7 \mathrm{mi} / \mathrm{h}$ <br> $6.5 \mathrm{mi} / \mathrm{h}$ <br> 13.4 m |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}{ }^{\star} \mathrm{F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2511 | 2853 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.6 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 7.4 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{\mathrm{d}, \mathrm{PTSF}}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.48 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 13.4 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2510.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.79 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To Jurisdiction Analysis Year | 133/NB <br> oro/Sun Valley Dr rans <br> Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi <br> Peak-hour factor, PHF No-passing zone <br> \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ <br> Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1022 | 2815 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{vl} / \mathrm{fHV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f_{A}}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{mi} / \mathrm{h}$  <br> $0.0 \mathrm{mi} / \mathrm{h}$  <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $18.4 \mathrm{mi} / \mathrm{h}$ <br> 37.8 m  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1022 | 2815 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}}{ }_{\mathrm{d}}{ }^{\mathrm{b}}\right)$ | 83.2 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 13.2 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n \mathrm{f}, \mathrm{PTSF}}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 86.7 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) <br> Volume to capacity ratio, $v / c$ | $F$ |  |
|  | 0.60 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Bicycle Level of Service |  |  |
|  |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1021.7 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.33 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |





| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst BM <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Valley Dr/Stan Oaks Dr Itrans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1826 | 2625 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1826 | 2625 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 94.3 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 9.8 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+\mathrm{f}_{\mathrm{np,PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{\mathrm{d}, \mathrm{PTSF}}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 98.3 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.07 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 28.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1826.1 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.63 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel SR <br> From/To S <br> Jurisdiction C <br> Analysis Year 20 | R-133/NB <br> Sun Valley Dr/Stan Oaks Dr Caltrans <br> 050 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain $\square$ Level Grade Length 0.25 mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.998 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2973 | 2511 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 0.92 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}{ }^{\star} \mathrm{F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 3225 | 2511 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 99.0 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) <br> Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+v_{o, P T S F}\right)$ | 7.8 |  |
|  | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.90 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1697 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1564 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.5 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2967.4 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.87 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2625 | 1826 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2625 | 1826 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 9.8 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\text {np, PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.54 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { PTSF }}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 28.0 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2625.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.81 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2511 | 2967 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$ <br> $0.0 \mathrm{mi} / \mathrm{h}$ <br>  <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ <br>  $\mathrm{f}_{\mathrm{np}, \text { ATS }}$ <br> $48.7 \mathrm{mi} / \mathrm{h}$  <br> $5.7 \mathrm{mi} / \mathrm{h}$  <br> $11.6 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}{ }^{\star} \mathrm{F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2511 | 2967 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.6 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 7.8 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{\mathrm{d}, \mathrm{PTSF}}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.48 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2510.9 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.79 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> Valley Dr/Stan Oaks Dr Itrans <br> 0 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1022 | 2935 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>   <br>  $17.5 \mathrm{mi} / \mathrm{h}$ <br>  $35.9 \%$ |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1022 | 2935 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 83.2 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 12.9 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 86.5 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.60 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 35.9 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1021.7 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.33 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Valley Dr/Stan Oaks Dr Itrans <br> 0 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1408 | 3326 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1408 | 3326 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 90.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 14.4 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 94.4 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.83 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 23.5 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1407.6 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.49 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB <br> Oaks Dr/LCAD dwy trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1940 | 2625 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $12.7 \mathrm{mi} / \mathrm{h}$ <br>  $26.2 \%$ |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1940 | 2625 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 95.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 9.2 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.14 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 26.2 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1940.2 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.66 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB <br> Oaks Dr/LCAD dwy trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2853 | 2625 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$ <br> $0.0 \mathrm{mi} / \mathrm{h}$ <br>  <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ <br>  $\mathrm{f}_{\mathrm{np}, \text { ATS }}$ <br> $48.7 \mathrm{mi} / \mathrm{h}$  <br> $5.7 \mathrm{mi} / \mathrm{h}$  <br> $11.6 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2853 | 2625 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 98.4 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 7.0 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.68 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2853.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.85 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Oaks Dr/LCAD dwy trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2625 | 1940 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$  <br>  $0.0 \mathrm{mi} / \mathrm{h}$ <br>  $48.7 \mathrm{mi} / \mathrm{h}$ <br>  $12.7 \mathrm{mi} / \mathrm{h}$ <br>  $26.2 \%$ |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2625 | 1940 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 9.2 |  |
| Percent time-spent-following, PTSF ${ }_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.54 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 26.2 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2625.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.81 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> Oaks Dr/LCAD dwy trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>  Segment length, $\mathrm{L}_{\mathrm{t}}$  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2625 | 2853 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$ <br> $0.0 \mathrm{mi} / \mathrm{h}$ <br>  <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ <br>  $\mathrm{f}_{\mathrm{np}, \text { ATS }}$ <br> $48.7 \mathrm{mi} / \mathrm{h}$  <br> $5.7 \mathrm{mi} / \mathrm{h}$  <br> $11.6 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2625 | 2853 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 7.0 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.54 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2625.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.81 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB <br> dwy/Canyon Acres Dr rans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1940 | 2625 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1940 | 2625 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 95.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 9.2 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f} \mathrm{n}_{\mathrm{p}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\text {d,PTSF }} / \mathrm{v}_{\text {d,PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 99.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.14 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 26.2 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1940.2 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.66 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company HDR <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | 133/NB <br> dwy/Canyon Acres Dr trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width  <br>  Segment length, $\mathrm{L}_{\mathrm{t}}$  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (0) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2853 | 2625 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4}{ }^{4}$ Ls (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f $\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}$ ) <br> Average travel speed, ATS $=$ FFS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}+\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2853 | 2625 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{d}{ }^{\text {b }}\right)$ | 98.4 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 7.0 |  |
| Percent time-spent-following, PTSF $_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | $F$ |  |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 1.68 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2853.3 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.85 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> dwy/Canyon Acres Dr trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 | 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.1 | 1.1 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.994 | 0.994 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2641 | 1952 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2625 | 1940 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np,PTSF }}$ (Exhibit 15-21) | 9.2 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}{ }_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| 泿 ${ }^{\text {Volume to capacity ratio, } \mathrm{v} / \mathrm{c}}$ | 1.55 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1690 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 25.7 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2625.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.81 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as lever <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period PM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/SB <br> dwy/Canyon Acres Dr trans <br> 0 No Build/Alt1-Alt4 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 2625 | 2853 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  $50.0 \mathrm{mi} / \mathrm{h}$ <br> $1.3 \mathrm{~m} / \mathrm{h}$ <br> $0.0 \mathrm{mi} / \mathrm{h}$ <br>  <br> $\left.\mathrm{v}_{\mathrm{o}, \text { ATS }}\right)$ <br>  $\mathrm{f}_{\mathrm{np}, \text { ATS }}$ <br> $48.7 \mathrm{mi} / \mathrm{h}$  <br> $5.7 \mathrm{mi} / \mathrm{h}$  <br> $11.6 \%$  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) \mathrm{v}_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}{ }^{\star} \mathrm{F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 2625 | 2853 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 97.9 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 7.0 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}{ }^{*}\left(\mathrm{v}_{\mathrm{d}, \mathrm{PTSF}} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 100.0 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 1.54 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 11.6 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 2625.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.81 |  |
| Bicycle level of service (Exhibit 15-4) | D |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst KK <br> Agency or Company $H D R$ <br> Date Performed $3 / 14 / 2022$ <br> Analysis Time Period AM Peak Hour | Highway / Direction of Travel From/To <br> Jurisdiction <br> Analysis Year | -133/NB <br> dwy/Canyon Acres Dr trans <br> 0 Build/Alt5 |
| Project Description: SR-133 PSR/PDS |  |  |
| Input Data |  |  |
|  Lane width Lane width <br>    | Class I highway <br> Terrain Level Grade Length mi Peak-hour factor, PHF No-passing zone \% Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ <br> \% Recreational vehicles, $\mathrm{P}_{\mathrm{R}}$ Access points mi |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 1087 | 2935 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}$ (Exhibit 15-7) <br> Adj. for access points ${ }^{4}$, $\mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) <br> Free-flow speed, FFS (FSS=BFFS-f LS $^{-f}{ }_{A}$ ) <br> Average travel speed, ATS $=$ FFS-0.00776 $\left(v_{d, A T S}+v_{o, A T S}\right)-f_{n p, A T S}$ <br> Percent free flow speed, PFFS |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star *} \mathrm{HV}, \mathrm{PTSF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 1087 | 2935 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 84.7 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 13.4 |  |
| Percent time-spent-following, $\mathrm{PTSF}_{\mathrm{d}}(\%)=\mathrm{BPTSF}_{\mathrm{d}}+\mathrm{f}_{\text {np,PTSF }}{ }^{*}\left(\mathrm{v}_{d, \text { PTSF }} / \mathrm{v}_{d, \text { PTSF }}+\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}\right)$ | 88.3 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | F |  |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.64 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { ATS }}$ (Equation 15-12) veh/h | 1700 |  |
| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{PTSF}}$ (Equation 15-13) veh/h | 1700 |  |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 34.8 |  |
| Bicycle Level of Service |  |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 1087.0 |  |
| Effective width, Wv (Eq. 15-29) ft | 22.00 |  |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |  |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.36 |  |
| Bicycle level of service (Exhibit 15-4) | C |  |
| Notes |  |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh/h. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |  |
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## Appendix J. Horizon Year (2050) Intersection LOS Worksheets

|  | $\downarrow$ | 4 | 4 | $p$ |  | $\ddagger$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | \％ | F | 个4 | F | ${ }^{7}$ | 个个 |  |  |
| Traffic Volume（veh／h） | 1035 | 21 | 1225 | 976 | 38 | 1334 |  |  |
| Future Volume（veh／h） | 1035 | 21 | 1225 | 976 | 38 | 1334 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate，veh／h | 1089 | 22 | 1289 | 1027 | 40 | 1404 |  |  |
| Adj No．of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap，veh／h | 909 | 811 | 1219 | 1357 | 54 | 1460 |  |  |
| Arrive On Green | 0.51 | 0.51 | 0.34 | 0.34 | 0.03 | 0.41 |  |  |
| Sat Flow，veh／h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume（v），veh／h | 1089 | 22 | 1289 | 1027 | 40 | 1404 |  |  |
| Grp Sat Flow（ s ，veh／h／ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| $Q$ Serve（g＿s），s | 61.5 | 0.8 | 41.3 | 31.7 | 2.7 | 46.4 |  |  |
| Cycle Q Clear（g＿c），s | 61.5 | 0.8 | 41.3 | 31.7 | 2.7 | 46.4 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 909 | 811 | 1219 | 1357 | 54 | 1460 |  |  |
| V／C Ratio（ X ） | 1.20 | 0.03 | 1.06 | 0.76 | 0.73 | 0.96 |  |  |
| Avail Cap（c＿a），veh／h | 909 | 811 | 1219 | 1357 | 74 | 1460 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay（d），s／veh | 29.3 | 14.5 | 39.3 | 3.5 | 57.7 | 34.3 |  |  |
| Incr Delay（d2），s／veh | 99.7 | 0.0 | 42.5 | 4.0 | 21.7 | 16.0 |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \％ile BackOfQ（50\％），veh／ln | 55.0 | 0.4 | 27.3 | 35.5 | 1.7 | 25.9 |  |  |
| LnGrp Delay（d），s／veh | 128.9 | 14.5 | 81.9 | 7.5 | 79.4 | 50.4 |  |  |
| LnGrp LOS | F | B | F | A | E | D |  |  |
| Approach Vol，veh／h | 1111 |  | 2316 |  |  | 1444 |  |  |
| Approach Delay，s／veh | 126.7 |  | 48.9 |  |  | 51.2 |  |  |
| Approach LOS | F |  | D |  |  | D |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 8.2 | 45.8 |  |  |  | 54.0 |  | 66.0 |
| Change Period（ $Y+R \mathrm{Rc}$ ），$s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.0 | 40.0 |  |  |  | 49.5 |  | 61.5 |
| Max Q Clear Time（g＿ct11），s | 4.7 | 43.3 |  |  |  | 48.4 |  | 63.5 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 |  |  |  | 0.9 |  | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 67.3 |  |  |  |  |  |
| HCM 2010 CtrI Delay |  |  | E |  |  |  |  |  |


|  |  | $4$ |  |  | $\pm$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | ${ }^{7}$ | F゙ | 44 | F゙ | ${ }^{1}$ | 4柬 |  |  |
| Traffic Volume（veh／h） | 900 | 53 | 1095 | 999 | 46 | 1223 |  |  |
| Future Volume（veh／h） | 900 | 53 | 1095 | 999 | 46 | 1223 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial Q $(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate，veh／h | 947 | 56 | 1153 | 1052 | 48 | 1287 |  |  |
| Adj No．of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap，veh／h | 909 | 811 | 1204 | 1350 | 62 | 1460 |  |  |
| Arrive On Green | 0.51 | 0.51 | 0.34 | 0.34 | 0.03 | 0.41 |  |  |
| Sat Flow，veh／h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume（v），veh／h | 947 | 56 | 1153 | 1052 | 48 | 1287 |  |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| Q Serve（g＿s），$s$ | 61.5 | 2.1 | 38.3 | 35.0 | 3.2 | 40.3 |  |  |
| Cycle Q Clear（g＿c），s | 61.5 | 2.1 | 38.3 | 35.0 | 3.2 | 40.3 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 909 | 811 | 1204 | 1350 | 62 | 1460 |  |  |
| V／C Ratio（X） | 1.04 | 0.07 | 0.96 | 0.78 | 0.78 | 0.88 |  |  |
| Avail Cap（c＿a），veh／h | 909 | 811 | 1204 | 1350 | 74 | 1460 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay（d），s／veh | 29.3 | 14.8 | 38.7 | 3.9 | 57.5 | 32.5 |  |  |
| Incr Delay（d2），s／veh | 41.2 | 0.0 | 17.5 | 4.5 | 34.5 | 8.0 |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \％ile BackOfQ（50\％），veh／In | 40.2 | 0.9 | 21.5 | 36.5 | 2.2 | 21.3 |  |  |
| LnGrp Delay（d），s／veh | 70.5 | 14.8 | 56.3 | 8.4 | 91.9 | 40.5 |  |  |
| LnGrp LOS | F | B | E | A | F | D |  |  |
| Approach Vol，veh／h | 1003 |  | 2205 |  |  | 1335 |  |  |
| Approach Delay，s／veh | 67.4 |  | 33.4 |  |  | 42.4 |  |  |
| Approach LOS | E |  | C |  |  | D |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 8.7 | 45.3 |  |  |  | 54.0 |  | 66.0 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.0 | 40.0 |  |  |  | 49.5 |  | 61.5 |
| Max Q Clear Time（g＿c＋l1），s | 5.2 | 40.3 |  |  |  | 42.3 |  | 63.5 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 |  |  |  | 4.5 |  | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 43.5 |  |  |  |  |  |
| $\text { HCM } 2010 \text { LOS }$ |  |  | D |  |  |  |  |  |


|  |  | $4$ |  |  | $t$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | ${ }^{7}$ | F゙ | 44 | F゙ | ${ }^{1 /}$ | 4柬 |  |  |
| Traffic Volume（veh／h） | 1035 | 21 | 1452 | 976 | 38 | 1494 |  |  |
| Future Volume（veh／h） | 1035 | 21 | 1452 | 976 | 38 | 1494 |  |  |
| Number | 3 | 18 | 2 | 12 | 1 | 6 |  |  |
| Initial Q $(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |  |  |
| Adj Flow Rate，veh／h | 1089 | 22 | 1528 | 1027 | 40 | 1573 |  |  |
| Adj No．of Lanes | 1 | 1 | 2 | 1 | 1 | 2 |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 |  |  |
| Cap，veh／h | 850 | 759 | 1337 | 1357 | 54 | 1578 |  |  |
| Arrive On Green | 0.48 | 0.48 | 0.38 | 0.38 | 0.03 | 0.45 |  |  |
| Sat Flow，veh／h | 1774 | 1583 | 3632 | 1583 | 1774 | 3632 |  |  |
| Grp Volume（v），veh／h | 1089 | 22 | 1528 | 1027 | 40 | 1573 |  |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 | 1770 | 1583 | 1774 | 1770 |  |  |
| Q Serve（g＿s），$s$ | 57.5 | 0.9 | 45.3 | 31.7 | 2.7 | 53.2 |  |  |
| Cycle Q Clear（g＿c），s | 57.5 | 0.9 | 45.3 | 31.7 | 2.7 | 53.2 |  |  |
| Prop In Lane | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 850 | 759 | 1337 | 1357 | 54 | 1578 |  |  |
| V／C Ratio（X） | 1.28 | 0.03 | 1.14 | 0.76 | 0.73 | 1.00 |  |  |
| Avail Cap（c＿a），veh／h | 850 | 759 | 1337 | 1357 | 74 | 1578 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay（d），s／veh | 31.3 | 16.5 | 37.3 | 3.5 | 57.7 | 33.2 |  |  |
| Incr Delay（d2），s／veh | 135.5 | 0.0 | 73.8 | 2.5 | 21.7 | 21.9 |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \％ile BackOfQ（50\％），veh／In | 60.1 | 0.4 | 35.8 | 34.9 | 1.7 | 30.6 |  |  |
| LnGrp Delay（d），s／veh | 166.7 | 16.5 | 111.2 | 6.0 | 79.4 | 55.1 |  |  |
| LnGrp LOS | F | B | F | A | E | E |  |  |
| Approach Vol，veh／h | 1111 |  | 2555 |  |  | 1613 |  |  |
| Approach Delay，s／veh | 163.8 |  | 68.9 |  |  | 55.7 |  |  |
| Approach LOS | F |  | E |  |  | E |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 8.2 | 49.8 |  |  |  | 58.0 |  | 62.0 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.0 | 44.0 |  |  |  | 53.5 |  | 57.5 |
| Max Q Clear Time（g＿c＋11），s | 4.7 | 47.3 |  |  |  | 55.2 |  | 59.5 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 |  |  |  | 0.0 |  | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |  |
|  |  |  | 84.8 |  |  |  |  |  |
| $\text { HCM } 2010 \text { LOS }$ |  |  | F |  |  |  |  |  |



HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 62.4 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\mathbf{T}$ |  | l | 个 |
| Traffic Vol, veh/h | 20 | 151 | 2050 | 30 | 178 | 2191 |
| Future Vol, veh/h | 20 | 151 | 2050 | 30 | 178 | 2191 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 156 | 2113 | 31 | 184 | 2259 |



HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy



HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 168.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\mathbf{F}$ |  | a | 个4 |
| Traffic Vol, veh/h | 20 | 151 | 2353 | 30 | 178 | 2427 |
| Future Vol, veh/h | 20 | 151 | 2353 | 30 | 178 | 2427 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 156 | 2426 | 31 | 184 | 2502 |


| Major/Minor | Minor1 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 4061 | 2442 | 0 | 0 | 2457 | 0 |
| $\quad$ Stage 1 | 2442 | - | - | - | - | - |
| $\quad$ Stage 2 | 1619 | - | - | - | - | - |
| Critical Hdwy | 6.63 | 6.23 | - | -4.13 | - |  |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.83 | - | - | - | - | - |
| Follow-up Hdwy | 3.519 | 3.319 | - | -2.219 | - |  |
| Pot Cap-1 Maneuver | $\sim 2$ | $\sim 40$ | - | - | 188 | - |
| $\quad$ Stage 1 | 68 | - | - | - | - | - |
| $\quad$ Stage 2 | 148 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 0 | $\sim 40$ | - | - | 188 | - |
| Mov Cap-2 Maneuver | $\sim 3$ | - | - | - | - | - |
| Stage 1 | 68 | - | - | - | - | - |
| Stage 2 | $\sim 3$ | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | WB | NB |
| :--- | :---: | :---: |
| HCM Control Delay, $\$ 4973.3$ | 0 | 7.6 |

HCMLOS F

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | - | - | 16 | 188 |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+:$ Computation Not Defined $\quad *:$ All major volume in platoon

HCM 2010 TWSC
2: Laguna Cyn Rd \& Anneliese Dwy

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2 |  |  |  |  |  |  |
| Movement W | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * ${ }^{\prime}$ |  | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 中4 |
| Traffic Vol, veh/h | 16 | 60 | 2273 | 10 | 56 | 2232 |
| Future Vol, veh/h | 16 | 60 | 2273 | 10 | 56 | 2232 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 62 | 2343 | 10 | 58 | 2301 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | F |  | F |  | a | 4 |
| Traffic Vol, veh/h | 2 | 2 | 2084 | 6 | 2 | 1959 |
| Future Vol, veh/h | 2 | 2 | 2084 | 6 | 2 | 1959 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 2 | 2265 | 7 | 2 | 2129 |


| Major/Minor | Minor1 | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 4402 | 2269 | 0 | 0 | 2272 | 0 |  |
| Stage 1 | 2269 | - | - | - | - | - |  |
| Stage 2 | 2133 | - | - | - |  | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | ~2 | 51 | - | - | 224 | - |  |
| Stage 1 | 84 | - | - | - | - | - |  |
| Stage 2 | 98 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | ~ 2 | 51 | - | - | 224 | - |  |
| Mov Cap-2 Maneuver | 42 | - | - | - | - | - |  |
| Stage 1 | 84 | - | - | - | - | - |  |
| Stage 2 | 97 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 91.3 |  | 0 |  | 0 |  |  |
| HCM LOS | F |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBR | BLn1 | SBL | SBT |  |
| Capacity (veh/h) |  | - | - | 46 | 224 | - |  |
| HCM Lane V/C Ratio |  | - | - | 0.095 | 0.01 | - |  |
| HCM Control Delay (s) |  | - | - | 91.3 | 21.2 | - |  |
| HCM Lane LOS |  | - | - | F | C | - |  |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0 | - |  |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s +: Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\mathbf{r}$ | $\mathbf{T}$ |  |  | 个4 |
| Traffic Vol, veh/h | 0 | 10 | 2083 | 3 | 0 | 2402 |
| Future Vol, veh/h | 0 | 10 | 2083 | 3 | 0 | 2402 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 11 | 2264 | 3 | 0 | 2611 |



|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection |  |  |  |  |  |  |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement V | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | */ |  | 4 | F | * | 4 |
| Traffic Vol, veh/h | 5 | 5 | 2085 | 11 | 5 | 1956 |
| Future Vol, veh/h | 5 | 5 | 2085 | 11 | 5 | 1956 |
| Conflicting Peds, \#/hr | 0 | 5 | 0 | 5 | 5 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 165 | 205 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 5 | 2149 | 11 | 5 | 2016 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



HCM 2010 TWSC
5: Laguna Cyn Rd \& Stan Oaks Dr

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | r |  | $\mathbf{T}$ |  | l | 个 |
| Traffic Vol, veh/h | 4 | 6 | 1779 | 1 | 2 | 2161 |
| Future Vol, veh/h | 4 | 6 | 1779 | 1 | 2 | 2161 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 7 | 1934 | 1 | 2 | 2349 |



HCM 2010 TWSC
5: Laguna Cyn Rd \& Stan Oaks Dr

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | F |  | F |  | a | 4 |
| Traffic Vol, veh/h | 3 | 2 | 2094 | 6 | 2 | 1959 |
| Future Vol, veh/h | 3 | 2 | 2094 | 6 | 2 | 1959 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 2 | 2276 | 7 | 2 | 2129 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



HCM 2010 TWSC
6: Laguna Cyn Rd \& Castle Rock Rd

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | $\mathbf{T}$ |  | l | 个 |
| Traffic Vol, veh/h | 6 | 8 | 1772 | 2 | 3 | 2162 |
| Future Vol, veh/h | 6 | 8 | 1772 | 2 | 3 | 2162 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 100 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 7 | 9 | 1926 | 2 | 3 | 2350 |



HCM 2010 TWSC
6: Laguna Cyn Rd \& Castle Rock Rd



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |







| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



|  | 4 |  | 4 |  |  | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | * |  | ${ }^{7}$ | 4 | $\uparrow$ |  |  |  |
| Traffic Volume (veh/h) | 55 | 45 | 52 | 1719 | 2126 | 42 |  |  |
| Future Volume (veh/h) | 55 | 45 | 52 | 1719 | 2126 | 42 |  |  |
| Number | 7 | 14 | 5 | 2 | 6 | 16 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |  |  | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1900 | 1863 | 1863 | 1863 | 1900 |  |  |
| Adj Flow Rate, veh/h | 60 | 49 | 57 | 1868 | 2311 | 46 |  |  |
| Adj No. of Lanes | 0 | 0 | 1 | 1 | 1 | 0 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Percent Heavy Veh, \% | 0 | 0 | 2 | 2 | 2 | 2 |  |  |
| Cap, veh/h | 74 | 61 | 73 | 1561 | 1377 | 27 |  |  |
| Arrive On Green | 0.08 | 0.08 | 0.04 | 0.84 | 0.76 | 0.76 |  |  |
| Sat Flow, veh/h | 919 | 750 | 1774 | 1863 | 1820 | 36 |  |  |
| Grp Volume(v), veh/h | 110 | 0 | 57 | 1868 | 0 | 2357 |  |  |
| Grp Sat Flow(s),veh/h/ln | 1684 | 0 | 1774 | 1863 | 0 | 1856 |  |  |
| Q Serve(g_s), s | 7.1 | 0.0 | 3.5 | 93.0 | 0.0 | 83.9 |  |  |
| Cycle Q Clear(g_c), s | 7.1 | 0.0 | 3.5 | 93.0 | 0.0 | 83.9 |  |  |
| Prop In Lane | 0.55 | 0.45 | 1.00 |  |  | 0.02 |  |  |
| Lane Grp Cap(c), veh/h | 136 | 0 | 73 | 1561 | 0 | 1404 |  |  |
| V/C Ratio(X) | 0.81 | 0.00 | 0.78 | 1.20 | 0.00 | 1.68 |  |  |
| Avail Cap(c_a), veh/h | 273 | 0 | 80 | 1561 | 0 | 1404 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 50.2 | 0.0 | 52.7 | 9.0 | 0.0 | 13.5 |  |  |
| Incr Delay (d2), s/veh | 10.7 | 0.0 | 35.2 | 95.0 | 0.0 | 308.6 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 3.7 | 0.0 | 2.4 | 87.2 | 0.0 | 162.5 |  |  |
| LnGrp Delay(d),s/veh | 60.9 | 0.0 | 87.9 | 104.0 | 0.0 | 322.1 |  |  |
| LnGrp LOS | E |  | F | F |  | F |  |  |
| Approach Vol, veh/h | 110 |  |  | 1925 | 2357 |  |  |  |
| Approach Delay, s/veh | 60.9 |  |  | 103.5 | 322.1 |  |  |  |
| Approach LOS | E |  |  | F | F |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 97.5 |  | 13.5 | 9.1 | 88.4 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ |  | 4.5 |  | 4.5 | 4.5 | 4.5 |  |  |
| Max Green Setting (Gmax), s |  | 93.0 |  | 18.0 | 5.0 | 83.5 |  |  |
| Max Q Clear Time (g_c+11), s |  | 95.0 |  | 9.1 | 5.5 | 85.9 |  |  |
| Green Ext Time (p_c), s |  | 0.0 |  | 0.2 | 0.0 | 0.0 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 219.8 |  |  |  |  |  |
| HCM 2010 LOS |  |  | F |  |  |  |  |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 1306 | - | 0 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.93 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.319 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 151 | 0 | - | - | - |
| $\quad$ Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | - | 151 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 27.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 「 | ${ }^{7}$ | 4 | 4 | 「 |
| Traffic Vol, veh/h | 80 | 66 | 76 | 1691 | 2109 | 62 |
| Future Vol, veh/h | 80 | 66 | 76 | 1691 | 2109 | 62 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None |  | None |
| Storage Length | 0 | 0 | 100 | - | - | 300 |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 87 | 72 | 83 | 1838 | 2292 | 67 |



HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot


| Major/Minor | Minor2 | Major1 | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 4884 | 1275 | 2617 | 0 | - |

HCM LOS F

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 162 | -16 | 158 | - | - |
| HCM Lane V/C Ratio | 0.51 | -5.435 | 0.454 | - | - |
| HCM Control Delay (s) | 48.3 | $\$ 2471.2$ | 45.5 | - | - |
| HCM Lane LOS | E | - | F | E | - |
| HCM 95th \%tile Q(veh) | 2.5 | -11.7 | 2.1 | - | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+:$ Computation Not Defined $\quad *:$ All major volume in platoon

HCM 2010 TWSC
8: Laguna Cyn Rd \& Act V Parking Lot

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



|  |  | $4$ | $\dagger 1$ |  | $p$ | $\pm$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 「' | $\dagger$ | 44 | F゙ | ${ }^{1}$ | 44 |  |
| Traffic Volume (veh/h) | 40 | 21 | 0 | 1895 | 15 | 21 | 1836 |  |
| Future Volume (veh/h) | 40 | 21 | 0 | 1895 | 15 | 21 | 1836 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 42 | 22 |  | 1974 | 16 | 22 | 1912 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 75 | 67 |  | 2811 | 1226 | 41 | 3058 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.79 | 0.79 | 0.02 | 0.86 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 42 | 22 |  | 1974 | 16 | 22 | 1912 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 2.2 | 1.3 |  | 25.0 | 0.2 | 1.2 | 15.4 |  |
| Cycle Q Clear(g_c), s | 2.2 | 1.3 |  | 25.0 | 0.2 | 1.2 | 15.4 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 75 | 67 |  | 2811 | 1226 | 41 | 3058 |  |
| V/C Ratio(X) | 0.56 | 0.33 |  | 0.70 | 0.01 | 0.54 | 0.63 |  |
| Avail Cap(c_a), veh/h | 460 | 411 |  | 2811 | 1226 | 92 | 3058 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 45.2 | 44.8 |  | 4.6 | 2.1 | 46.5 | 1.9 |  |
| Incr Delay (d2), s/veh | 6.3 | 2.8 |  | 1.5 | 0.0 | 10.5 | 1.0 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 1.2 | 0.6 |  | 12.4 | 0.1 | 0.7 | 7.6 |  |
| LnGrp Delay (d), s/veh | 51.5 | 47.5 |  | 6.1 | 2.1 | 57.0 | 2.9 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 64 |  |  | 1990 |  |  | 1934 |  |
| Approach Delay, s/veh | 50.1 |  |  | 6.1 |  |  | 3.5 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 6.7 | 81.0 |  |  |  | 87.7 |  | 8.6 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 5.0 | 76.5 |  |  |  | 76.5 |  | 25.0 |
| Max Q Clear Time (g_c+11), s | 3.2 | 27.0 |  |  |  | 17.4 |  | 4.2 |
| Green Ext Time (p_c), s | 0.0 | 28.9 |  |  |  | 25.8 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 5.5 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | 7 | 4 | 71 |  | 7 |  | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 7 | $\square$ | 44 | F' | ${ }^{7}$ | 中4 |  |
| Traffic Volume (veh/h) | 20 | 21 | 0 | 1843 | 30 | 20 | 1898 |  |
| Future Volume (veh/h) | 20 | 21 | 0 | 1843 | 30 | 20 | 1898 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$, veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate, veh/h | 21 | 22 |  | 1920 | 31 | 21 | 1977 |  |
| Adj No. of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap, veh/h | 63 | 56 |  | 2834 | 1236 | 40 | 3080 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.80 | 0.80 | 0.02 | 0.87 |  |
| Sat Flow, veh/h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume(v), veh/h | 21 | 22 |  | 1920 | 31 | 21 | 1977 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve(g_s), s | 1.1 | 1.3 |  | 22.6 | 0.4 | 1.1 | 15.7 |  |
| Cycle Q Clear(g_c), s | 1.1 | 1.3 |  | 22.6 | 0.4 | 1.1 | 15.7 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 63 | 56 |  | 2834 | 1236 | 40 | 3080 |  |
| V/C Ratio(X) | 0.33 | 0.39 |  | 0.68 | 0.03 | 0.53 | 0.64 |  |
| Avail Cap(c_a), veh/h | 464 | 414 |  | 2834 | 1236 | 93 | 3080 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 45.0 | 45.1 |  | 4.1 | 1.9 | 46.2 | 1.8 |  |
| Incr Delay (d2), s/veh | 3.0 | 4.3 |  | 1.3 | 0.0 | 10.5 | 1.0 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 0.6 | 0.6 |  | 11.2 | 0.2 | 0.7 | 7.9 |  |
| LnGrp Delay(d),s/veh | 48.0 | 49.4 |  | 5.5 | 2.0 | 56.7 | 2.9 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol, veh/h | 43 |  |  | 1951 |  |  | 1998 |  |
| Approach Delay, s/veh | 48.7 |  |  | 5.4 |  |  | 3.4 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 6.6 | 81.0 |  |  |  | 87.6 |  | 7.9 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting (Gmax), s | 5.0 | 76.5 |  |  |  | 76.5 |  | 25.0 |
| Max Q Clear Time (g_c+11), s | 3.1 | 24.6 |  |  |  | 17.7 |  | 3.3 |
| Green Ext Time (p_c), s | 0.0 | 28.4 |  |  |  | 27.5 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 4.9 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  |  |  | $\dagger$ |  |  |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 「 | $\square$ | 44 | 「7 | ${ }^{1 /}$ | 中4 |  |
| Traffic Volume（veh／h） | 40 | 21 | 0 | 2122 | 15 | 98 | 1996 |  |
| Future Volume（veh／h） | 40 | 21 | 0 | 2122 | 15 | 98 | 1996 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$ ，veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  |  | 0.97 | 1.00 |  |  |
| Parking Bus，Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate，veh／h | 42 | 22 |  | 2210 | 16 | 102 | 2079 |  |
| Adj No．of Lanes | 1 | 1 |  | 2 | 1 | ， | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh，\％ | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap，veh／h | 74 | 66 |  | 2651 | 1156 | 128 | 3068 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.75 | 0.75 | 0.07 | 0.87 |  |
| Sat Flow，veh／h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume（v），veh／h | 42 | 22 |  | 2210 | 16 | 102 | 2079 |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve（g＿s），s | 2.3 | 1.3 |  | 41.2 | 0.3 | 5.6 | 18.7 |  |
| Cycle Q Clear（g＿c），s | 2.3 | 1.3 |  | 41.2 | 0.3 | 5.6 | 18.7 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap（c），veh／h | 74 | 66 |  | 2651 | 1156 | 128 | 3068 |  |
| V／C Ratio（X） | 0.56 | 0.33 |  | 0.83 | 0.01 | 0.80 | 0.68 |  |
| Avail Cap（c＿a），veh／h | 450 | 401 |  | 2651 | 1156 | 137 | 3068 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter（l） | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay（d），s／veh | 46.4 | 45.9 |  | 8.3 | 3.1 | 45.1 | 2.1 |  |
| Incr Delay（d2），s／veh | 6.6 | 2.9 |  | 3.3 | 0.0 | 25.9 | 1.2 |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \％ile BackOfQ（50\％），veh／ln | 1.3 | 0.6 |  | 20.8 | 0.1 | 3.7 | 9.2 |  |
| LnGrp Delay（d），s／veh | 52.9 | 48.8 |  | 11.5 | 3.2 | 70.9 | 3.3 |  |
| LnGrp LOS | D | D |  | B | A | E | A |  |
| Approach Vol，veh／h | 64 |  |  | 2226 |  |  | 2181 |  |
| Approach Delay，s／veh | 51.5 |  |  | 11.5 |  |  | 6.5 |  |
| Approach LOS | D |  |  | B |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 11.6 | 78.4 |  |  |  | 90.0 |  | 8.6 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 7.6 | 73.9 |  |  |  | 76.5 |  | 25.0 |
| Max Q Clear Time（g＿c＋11），s | 7.6 | 43.2 |  |  |  | 20.7 |  | 4.3 |
| Green Ext Time（p＿c），s | 0.0 | 24.0 |  |  |  | 33.5 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.6 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | 7 | $4$ | 71 |  | $p$ | $\pm$ | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7}$ | 「 | － | 44 | 「＇ | ${ }^{7}$ | 中4 |  |
| Traffic Volume（veh／h） | 20 | 21 | 0 | 2064 | 30 | 45 | 2045 |  |
| Future Volume（veh／h） | 20 | 21 | 0 | 2064 | 30 | 45 | 2045 |  |
| Number | 3 | 18 |  | 2 | 12 | 1 | 6 |  |
| Initial $Q(Q b)$ ，veh | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Ped－Bike Adj（A＿pbT） | 1.00 | 1.00 |  |  | 0.98 | 1.00 |  |  |
| Parking Bus，Adj | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj Sat Flow，veh／h／ln | 1863 | 1863 |  | 1863 | 1863 | 1863 | 1863 |  |
| Adj Flow Rate，veh／h | 21 | 22 |  | 2150 | 31 | 47 | 2130 |  |
| Adj No．of Lanes | 1 | 1 |  | 2 | 1 | 1 | 2 |  |
| Peak Hour Factor | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Percent Heavy Veh，\％ | 2 | 2 |  | 2 | 2 | 2 | 2 |  |
| Cap，veh／h | 63 | 56 |  | 2791 | 1217 | 66 | 3086 |  |
| Arrive On Green | 0.04 | 0.04 |  | 0.79 | 0.79 | 0.04 | 0.87 |  |
| Sat Flow，veh／h | 1774 | 1583 |  | 3632 | 1544 | 1774 | 3632 |  |
| Grp Volume（v），veh／h | 21 | 22 |  | 2150 | 31 | 47 | 2130 |  |
| Grp Sat Flow（s），veh／h／ln | 1774 | 1583 |  | 1770 | 1544 | 1774 | 1770 |  |
| Q Serve（g＿s），s | 1.1 | 1.3 |  | 31.8 | 0.4 | 2.5 | 18.8 |  |
| Cycle Q Clear（g＿c），s | 1.1 | 1.3 |  | 31.8 | 0.4 | 2.5 | 18.8 |  |
| Prop In Lane | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap（c），veh／h | 63 | 56 |  | 2791 | 1217 | 66 | 3086 |  |
| V／C Ratio（X） | 0.33 | 0.39 |  | 0.77 | 0.03 | 0.72 | 0.69 |  |
| Avail Cap（c＿a），veh／h | 457 | 408 |  | 2791 | 1217 | 91 | 3086 |  |
| HCM Platoon Ratio | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter（I） | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay（d），s／veh | 45.7 | 45.8 |  | 5.5 | 2.2 | 46.2 | 2.0 |  |
| Incr Delay（d2），s／veh | 3.1 | 4.4 |  | 2.1 | 0.0 | 14.7 | 1.3 |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \％ile BackOfQ（50\％），veh／ln | 0.6 | 0.6 |  | 15.8 | 0.2 | 1.5 | 9.1 |  |
| LnGrp Delay（d），s／veh | 48.8 | 50.2 |  | 7.7 | 2.3 | 61.0 | 3.3 |  |
| LnGrp LOS | D | D |  | A | A | E | A |  |
| Approach Vol，veh／h | 43 |  |  | 2181 |  |  | 2177 |  |
| Approach Delay，s／veh | 49.5 |  |  | 7.6 |  |  | 4.5 |  |
| Approach LOS | D |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 8.1 | 81.0 |  |  |  | 89.1 |  | 7.9 |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 4.5 | 4.5 |  |  |  | 4.5 |  | 4.5 |
| Max Green Setting（Gmax），s | 5.0 | 76.5 |  |  |  | 76.5 |  | 25.0 |
| Max Q Clear Time（g＿c＋l1），s | 4.5 | 33.8 |  |  |  | 20.8 |  | 3.3 |
| Green Ext Time（p＿c），s | 0.0 | 29.8 |  |  |  | 34.8 |  | 0.1 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 6.5 |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |

## ATTACHMENT E

## TRANSPORTATION MANAGEMENT PLAN (TMP) DATA SHEETS

# TRANSPORTATION MANAGEMENT PLAN DATA SHEET （Preliminary TMP Elements and Costs） 

$\mathrm{Co} / \mathrm{Rte} / \mathrm{PM} \quad$ 12－ORA－133（PM 0．9－3．4）

Project ID No．$\underline{1217000086 \quad \text { EA＿12－0Q670K Alternatives No．} 2,3,4, \& 5}$

Project Limit $\quad \underline{\text { SR－1 }} 133$ from Canyon Acres Drive（PM 0．9）to El Toro Road（PM 3．4）
Project Description Laguna Canyon Road（SR－133）PSR－PDS

1）Public Information
$\boxtimes_{\text {a．Brochures and Mailers }}$
$\boxtimes_{b}$ ．Press Release
$\$ \quad 30,000$
$\boxtimes_{\text {c．Paid Advertising }}$
$\$ \quad 0$
$\square$ d．Public Information Center／Kiosk
】e．Public Meeting／Speakers Bureau
$\$ \quad 40,000$
$\square$ f．Telephone Hotline
$\$ \quad 0$
$\$ \quad 0$
$\boxtimes_{g}$ ．Internet
$\$ \quad 30,000$
$\square_{\mathrm{h}}$ ．Others $\qquad$
$\qquad$
$\$$
$\$ \quad 20,000$
\＄
0

0

2）Motorists Information Strategies
$\square$ a．Changeable Message Signs（Fixed）
$\$$
0
区b．Changeable Message Signs（Portable）
$\$ \quad 100,000$
】c．Ground Mounted Signs
$\$ \quad 48,000$
$\square$ d．Highway Advisory Radio
$\$ \quad 0$
$\square$ e．Caltrans Highway Information Network（CHIN）
$\$ \quad 0$
$\square$ f．Others
$\$ \quad 0$
3) Incident Management
】a. Construction Zone Enhanced Enforcement Program(COZEEP)
$\boxtimes_{\mathrm{b}}$. Freeway Service Patrol
$\$ \quad 200,000$
$\$ \quad 250,000$
$\square$ c. Traffic Management Team
$\$ \quad 0$
$\square$ d. Helicopter Surveillance
$\square$ e. Traffic Surveillance Stations (Loop Detector and CCTV)
$\square$ f. Others $\qquad$
4) Construction Strategies

区a. Lane Closure Chart
$\$ \quad 0$
$\boxtimes_{b}$. Reversible Lanes
$\$$
0
$\square$ c. Total Facility Closure
$\square$ d. Contra Flow
$\square$ e. Truck Traffic Restrictions
\$
$\$ \quad 0$
$\square$ f. Reduced Speed Zone
$\square$ g. Connector and Ramp Closures
$\square_{\text {h. Incentive and Disincentive }}$
$\square$ i. Movable Barrier
$\square$ j. Others $\qquad$
$\$$
$\$ \quad 0$
$\$$
$\$ \quad 0$
5) Demand Management
$\square$ a. HOV Lanes/Ramps (New or Convert)
$\$$ 0
$\square$ b. Park and Ride Lots
$\square$ c. Rideshare Incentives
\$0
$\square$ d. Variable Work Hours
$\$$0
$\square$ e. Telecommute $\square$
$\square$ f. Ramp Metering (Temporary Installation)
$\$ \quad 0$
$\square$ g. Ramp Metering (Modify Existing)
$\$ \quad 0$
$\square_{\text {h. Others }}$
$\$ \quad 0$
6) Alternative Route Strategies
$\square$ a. Add Capacity to Freeway Connector
\$

Х $_{\text {b. Street Improvement (widening, traffic }}$ signal... etc.)
$\$ \quad 300,000$
$\square$ c. Traffic Control Officers
$\$$0
$\square$ d. Parking Restrictions
$\$$

## 0

$\square$ e. Others $\qquad$
$\$$
7) Other Strategies
$\square$ a. Application of New Technology
$\square$ b. Others $\qquad$
$\$$0
$\$$ ..... 0

## TMP Notes:

## PUBLIC INFORMATION

## BROCHURES AND MAILERS:

Send courtesy notices by direct mail to the project neighborhood to inform them of construction and work zone information. The information provided will include the project's start date, schedules and alternative routes. It is anticipated that 10,000 brochures and mailers will be needed at $\$ 3$ each $=\$ 30,000$.

## PRESS RELEASE:

Provide press release whenever any facilities are closed for construction. During any closures necessitated for construction, Caltrans will implement the press release upon receiving closure information from the Project Resident Engineer. No costs are associated with press releases.

## PAID ADVERTISING:

Paid advertising includes additional advertising through other media means and may include local television advertising, social media advertising, newspaper advertising, cost for these types of advertisements are expected to be approximately $\$ 20,000$.

## PUBLIC MEETING:

It is anticipated that public meetings will be held at the project start and at the beginning of each stage to present the project information to the community. It is anticipated that the meetings will be held in one location. This yields a total of 4 meetings at $\$ 10,000=\$ 40,000$.

## INTERNET:

A project website will be designed to provide real-time interactive information on project plans and progress. The cost to develop and maintain the website for two years is expected to be $\$ 30,000$.

## MOTORISTS INFORMATION STRATEGIES

## PORTABLE CHANGEABLE MESSAGE SIGNS:

PCMS will be placed at key locations to notify motorists of construction activities, road closures and detours. It is assumed that a total of 10 PCMS at a cost of $\$ 10,000$ each $=\$ 100,000$ would be used as a TMP measure to be used for all stages of construction. The PCMS will be moved for each stage as needed. Additional PCMSs may be specified as part of the project signing.

## GROUND MOUNTED SIGNS:

Temporary ground mounted signs will provide traveler information to guide motorists through the work zone.

Each stage will require up to 40 signs at $\$ 400$ per sign $=\$ 16,000$ per stage $X 3$ Stages $=\$ 48,000$

## INCIDENT MANAGEMENT

## COZEEP:

It is assumed that CHP or similar agency enforcement will be used during setting of K-rail and general construction for a total of 100 working days at 10 hours per shift including travel time to and from the project site.
$\$ 100 /$ Officer/Hour (2 officers): $\$ 100 \times 2 \times 1,000$ hours $=\$ 200,000$

## FREEWAY SERVICE PATROL:

It is assumed that Freeway Service Patrol (FSP) will be required. FSP will include tow truck service that will be needed during construction when the shoulders are reduced in width or temporarily eliminated. Currently OCTA manages the Orange County FSP program. Laguna Canyon Road is not one of the highways that is serviced by FSP. It is assumed that the FSP would be used for peak hours (6-10 AM and 3-7 PM) during the week for two years.
$\$ 80 /$ Truck/Hour (1 truck): $\$ 80 \times 1$ trucks x 4,160 hours $=\$ 332,800$ use $\$ 335,000$

## CONSTRUCTION STRATEGIES

## STAGE CONSTRUCTION:

Construction is to be completed in multiple stages with multiple phases within each major stage of the Project. Detailed staging for this alternative will be considered in the next project phase.

## STAGE CONSTRUCTION AND TRAFFIC HANDLING PLANS:

As part of the PS\&E package, Construction Staging Plans shall be prepared that shows the sequence of construction activities. The construction staging approach for this Project is to be completed in a specific sequence to minimize impacts to the traveling public.

In addition to the construction staging plans, traffic handling plans shall be included. The traffic handling plans shall contain sufficient alignment detail, profiles and typical cross-sections to guide traffic through the work zone in the sequence shown in the stage construction plans.

## ALTERNATE ROUTE STRATEGIES

## STREET IMPROVEMENTS

Temporary traffic signals may be needed to provide access to properties within the project area. It is anticipated that a total of three temporary signals for three stages of construction may be needed at a cost of approximately $\$ 100,000$ for each temporary signal. This would total up to be $\$ 300,000$.

## DATE

Steve Crouch, P.E.

## ATTACHMENT F

## STORM WATER DATA REPORT (SWDR)

Dist-County-Route: 12-ORA-133
Post Mile Limits: $0.96 / 3.41$
Type of Work: Bike and Pedestrian Path Addition and Utility Undergounding
Project ID (EA): 12-00670K
Program Identification: 20.10.800.100
Phase: $\boxtimes$ RID (FIR) PSR/PDS

Regional Water Quality Control Board(s):San Diego, Region 9
Total Disturbed Soil Area: 6.81 acres
PCTA: 6.81 acres

Estimated Const. Start Date:07-01-28
Estimated Cont. Completion Date: 2-28-30

Is the Project within a TMDL watershed?
Yes $\boxtimes \quad$ No

This Report has been prepared under the direction of the following Licensed Person. The Licensed Person attests to the technical information contained herein and the date upon which recommendations, conclusions, and decisions are based. Professional Engineer or Landscape Architect stamp required at PS\&E only.


7-22-2022
Stephen P.A. Crouch, Registered Project Engineer
Date

I have reviewed the stormwater quality design issues and find this report to be complete, current and accurate:


## STORMWATER DATA INFORMATION

## 1. Project Description

- The City of Laguna Beach (City), in cooperation with the California Department of Transportation (Caltrans) District 12, is proposing to construct improvements along the State Route (SR) 133 corridor extending approximately 2.5 miles from Canyon Acres Drive (PM 0.96) to El Toro Road (PM 3.41) in Orange County (the Project).This segment of SR-133 consists of a two-lane highway with a center turn lane, limited shoulders, and sporadic off-street angled and parallel parking located along the north bound side of the roadway. The 34 -foot roadway section is comprised of two 12 -foot travel lanes and a 10 -foot center turn lane. Two signalized intersections at Canyon Acres Drive and El Toro Road are located within this segment of Laguna Canyon Road (LCR). In addition, an existing midblock pedestrian crossing of SR-133 is located at the Laguna College of Art and Design. The right-of-way is constrained by residential and light commercial developments as well as various environmental constraints and open space preserve along the route. The route is further constrained by Southern California Edison's (SCE) overhead transmission and distribution line poles in close proximity to the travel way.The proposed improvements to LCR within this segment generally consist of a Class II and Class IV bicycle lane(s), pedestrian pathways/sidewalks, improving access to transit facilities, improved shoulders, undergrounding of the SCE transmission and distribution lines outside the travel way, and the introduction of additional signalized intersections at select locations and cross streets. Four alternatives are being analyzed for the Project: a no build alternative and three build alternatives, which include a combination of the above elements. No additional travel lanes are proposed for the Project.
At the PID and PA/ED phases, the DSA should consider all areas where ground disturbance is anticipated. Alternative 5 with the largest impact/footprint was evaluated for the purpose of this study (Figure 1-1). The total disturbed soil area (DSA) for the project is estimated to be 6.81 acres. The area was estimated using limited data and includes areas for construction, access, and staging. DSA will be recalculated when the project survey is complete.
- The post construction treatment area (PCTA) for the project is estimated to be 6.81 acres. The areas in Table 1-1 were calculated in Microstation based on Alternative 5 in Figure 1-1 and according to the typical section in Figure 1-2 below. A similar exercised was completed for Alternative 3. Alternative 3's areas are included in Table 1-1 for comparison.
- Since there are no existing BMPs within the project footprint are impacted (removed or modified), by the proposed project, Additional Treated Area (ATA\#1) condition is zero. Also, since Net New Impervious area (NNI) is less than $50 \%$ of the total post project impervious area, thus ATA\#2 is zero.
- The project site is very constrained with no space to be able to locate BMPs for post construction treatment. As a result, it was decided early in the development of this project to propose a porous pavement material type call Open Graded Friction Course (OGFC) for the bike lanes.


Figure 1-1. Alternative 5 with the largest impact/footprint


Figure 2-2. Alternative 5 Typical Section

Table 1-1 Project Area Calculations for Alternatives 3 and 5

| Variable | Areas | Alt 3 Acres | Alt 5 Acres |
| :---: | :--- | :---: | :---: |
| A | Existing Impervious Area | 17.92 | 17.92 |
| B | New Impervious AC over Pervious Area | 0.97 | 1.14 |
| C | New Impervious Concrete Sidewalk over Pervious Area | 0.78 | 2.56 |
| D | New Pervious Class 1 Ped/ Bikeway (eg. Open Grade Friction Course (OGFC)) over <br> Pervious Area** | 1.50 | 0.00 |
| E | Replace Impervious AC w/ Impervious Concrete for New Sidewalk (AB remains in <br> place*)** | 0.63 | 0.76 |
| F | Replace Impervious AC w/ Pervious Class 4 Ped/ Bikeway (eg. OGFC) | 3.86 | 0.00 |
| G | Replace Impervious AC w/ Impervious AC (shoulder to full-depth) | 2.52 | 5.67 |
| DSA | Disturbed Soil Area | 7.23 | 6.81 |

*Remove existing AC up to AB layer * *For Information Only (Not used in the calculations in table below)

Table 1-2
PCTA Calculations for Alternatives 3 and 5

| Variable | Impervious Areas | Arithmetic | Alt 3 Acres | Alt 5 Acres |
| :---: | :--- | :---: | :---: | :---: |
| M | Pre-project Impervious Area | A | 17.92 | 17.92 |
| EIA | Excluded Impervious Areas | C | 0.78 | 2.56 |
| N | Post-project Impervious Area | M+B+C-F | 15.03 | 21.62 |
| NNI | Net New Impervious area | N-M-EIA | -2.89 | 1.14 |
| RIS | Replaced Impervious Surface | G | 2.52 | 5.67 |
| NIS | New Impervious Surface | NNI+RIS | 0 | 6.81 |
| ATA\#1 | Additional Treated Area (condition 1) | - | 0 | 0.00 |
| ATA\#2 | Additional Treated Area (condition 2) | - | 0 | 0.00 |
| PCTA | Post Construction Treatment Area | NIS+ ATA\#1+ ATA\#2 | 0 | 6.81 |

## 2. Site Data and Stormwater Quality Design Issues

- A 401 Water Quality Certification is anticipated.
- According to the Caltrans Water Quality Planning Tool (WQPT), the project is located within an unincorporated portion of the Orange County and within San Diego Municipal Separate Storm Sewer System (MS4) area. Directly south of State Route 133 (SR-133) is the City of Laguna Beach; however, there are no major incorporated cities or towns within the project area.
- The project is located within the San Juan Hydrologic Unit (HU) [901.00], the Laguna Hydrologic Area (HA) [901.10], and the Laguna Beach Hydrologic Sub-Area (HSA) [901.12],
which is under the jurisdiction of the San Diego Regional Water Quality Control Board (RWQCB).
- The recieving water body within the project limit is Laguna Canyon Channel which is not listed as an impaired water body in the RWQCB 2020/2022 303(d) list. Laguna Canyon Channel ultimately drains to Pacific Ocean which is approximately 1 mile south of Canyon Acres Drive. The outlet of Laguna Canyon Channel to the Pacific Ocean is within the TMDL "Project I Revised Twenty Beaches and Creeks in the San Diego Region (including Tecolote Creek) (Indicator Bacteria)", per the Caltrans Stormwater Portal and TMDL Reach Proritaztion Ranking \& PM D12 (Table 2-1).

| Table 2-1. TMDLs within the project limits |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Regional <br> Board | District | County | TMDL | Reach | Route | BPM | EPM | Final Ranking |
| 8 | 12 | ORA | Project I- Twenty Beaches and Creeks in the San <br> Diego Region including Tecolote Creek (indicator <br> bacteria) | 1 | 133 | 0.00 | 6.469 | 200 |

Source: Caltrans, Oct.28, 2015. "TMDL Reach Proritaztion Ranking \& PM D12"

- Figures 2-1, and 2-2 represent snapshots of the TMDL analysis of the receiving water bodies per Caltrans Stormwater Portal and SWRCB 2014/2016 California Integrated Report (Clean Water Act Section 303(d) List / 305(b) Report).

Figure 2-1A, Snapshot of the TMDL analysis of the receiving water bodies (Caltrans Stormwater Portal).


Figure 2-2B, Snapshot of the TMDL analysis of the receiving water bodies (Caltrans Stormwater Portal).


Source: Caltrans Stormwater Portal, < https://caltransesp.com/tmdlsearch/index.html >

Figure 2-3, Snapshot of the TMDL analysis of the receiving water bodies (SWRCB: 2014/2016 California Integrated Report (Clean Water Act Section 303(d) List/ 305(b) Report))

| Final 2014/2016 California Integrated Report (Clean Water Act Section 303(d) List / 305(b) Report) |
| :--- |
| 2014 and 2016 Integrated Report Map 303(d) List References Data Download Contact Us |

2014 AND 2016 INTEGRATED REPORT - 303(D) LISTED WATERS



#### Abstract

Show water bodies by pollutant:


Pollutant category:
All


Pollutant:
All



Source: SWRCB, Final 2014/2016 California Integrated Report (Clean Water Act Section 303(d) List / 305(b) Report) <https://www.waterboards.ca.gov/water issues/programs/tmdl/integrated2014 2016.shtml >

## Geotechnical Data

- The predominant soil type in the project area is Capistrano Sandy Loam (2 to 9 percent slopes) and identified as Hydraologic Soil Group (HSG) B. A short segment of the project area is in Chino Silty Clay Loam and identified as HSG C. More geotechnical information will be available in the next project phase. The soil erodibility of the site (erosion factor K ) within the project area is 0.32 .


## Topographic Data

- The United States Geological Survey (USGS) topography map of the area shows the elevation of the project area ranging from 80 ft to 240 ft .


## Hydraulic Data

- According to the NRCS Web Soil Survey, the groundwater is about 7 feet below ground. The Log of Test Borings will be performed in later phases of the project.


## Climate

- The historic climate data is based on information obtained from Laguna Beach Station (ID 044647), which is located approximately 1 miles south of the project site. The average temperature ranges from $55.1^{\circ} \mathrm{F}$ to $70.2^{\circ} \mathrm{F}$ at the Laguna Beach Station. The average annual rainfall depth is 13.81 inches. The $85^{\text {th }}$ percentile 24 -hour storm (daily rainfall total) is 0.85 inches per Basin Sizer (Ver 1.47).


## 3. Construction Site BMPs to be used on Project

- Project BMP measures will be specified and quantified during later phases of the project.


## Risk Assessment

- This project was determined to be Risk Level 2 based on Method 1, GIS Map Method, Appendix 1, 2009 CGP. The Risk Level documentation is attached to this report.


## Construction Site BMP Strategy

- The construction work for this project is scheduled to cover approximately 3 years. This project will disturb more than one acre of soil, so a Storm Water Pollution Prevention Plan (SWPPP) is required. DSA will be protected in accordance with the project's approved SWPPP. The BMP categories suitable for controlling potential pollutants to be considered for this project will be detailed during the design phase and include: Soil Stabilization, Sediment Control, Tracking Control, Wind Erosion Control, Non-storm Water Management, Waste

Management and Materials Pollution Control. Project specific BMP measures will be specified and quantified during the design phase.

## 4. Maintenance BMPs

- Drain inlet stenciling is required to be installed on inlets and catch basins since pedestrian traffic is expected along the highway.

5. Other Water Quality Requirements and Agreements

- Not applicable

6. Permanent BMPs

- Permanent BMPs are strategies and measures to minimize and avoid water quality impacts in the post construction condition. Permanent BMPs include Design Pollution Prevention and Treatment BMP strategies. Based upon Alternative 5, which is the largest footprint for the project, permanent BMPs may be required for the project depending on which Alternative is selected during the PA/ED phase of the project.


## Rapid Stability Assessment

- This project potentially requires an RSA based on the algorithm (items listed below) provided in Section 2 of Caltrans Hydromodification Guidance dated February 2015. An RSA is potentially required based on all 4 bullets.
- This project includes stream crossings.
- This project does include 1 acre or more of net new impervious (NNI) surface.
- The NNI is within the stream threshold drainage areas.
- Stream crossings are "Water of the US" as defined by Army Corps of Engineers latest guidance on determination of jurisdiction for CWA section 404.


## Design Pollution Prevention (DPP) BMP Strategy

Design Pollution Prevention BMPs will be incorporated into the project where appropriate to minimize impacts to water quality by preventing downstream erosion and stabilizing disturbed soil areas. These BMPs can provide water quality benefits including settling of solids and other pollutants and increasing detention time by incorporating and preserving vegetated surfaces. Further investigation will be provided during the PA/ED and PS\&E phases of the project to determine which treatment

## Treatment BMP Strategy

Depending upon the Alternative selected Treatment BMPs may be required. For example, Alternative 2 and 3 provide bikepath facilities that are proposed to be constructed with Open Grade Friction Course (OGFC) pavement thus increasing pervious area. If either of these alternatives are chosen, the New Net Impervious may be less than zero thus preventing any additional Treatment BMPs. The applicability of this Treatment BMP will be reviewed and studied along with others during the PA/ED and PS\&E phases of the project.

## Required Attachments

- Vicinity Map
- Evaluation Documentation Form
- Risk Level Determination Documentation
- SWDR Summary Spreadsheets

Vicinity Map


## Evaluation Documentation Form

DATE: 05-26-22
Project ID (EA): $\quad 00670$

\begin{tabular}{|c|c|c|c|c|}
\hline No. \& Criteria \& \begin{tabular}{l}
Yes \\
\(\checkmark\)
\end{tabular} \& \begin{tabular}{l}
No \\
\(\checkmark\)
\end{tabular} \& Supplemental Information for Evaluation \\
\hline 1. \& Begin Project evaluation regarding requirement for implementation of Treatment BMPs \& \(\checkmark\) \& \& See Figure 4-1, Project Evaluation Process for Consideration of Treatment BMPs. Continue to 2. \\
\hline 2. \& Is the scope of the Project to install Treatment BMPs (e.g., Alternative Compliance or TMDL Compliance Units)? \& \& \(\checkmark\) \& \begin{tabular}{l}
If Yes, go to 8. \\
If No, continue to 3.
\end{tabular} \\
\hline 3. \& Is there a direct or indirect discharge to surface waters? \& \(\checkmark\) \& \& If Yes, continue to 4. If No , go to 9 . \\
\hline 4. \& \begin{tabular}{l}
As defined in the WQAR or ED, does the project: \\
a. discharge to areas of Special Biological Significance (ASBS), or \\
b. discharge to a TMDL watershed where Caltrans is named stakeholder, or \\
c. have other pollution control requirements for surface waters within the project limits?
\end{tabular} \& \(\checkmark\) \& \(\checkmark\)

$\checkmark$ \& | If Yes to any, contact the District/Regional Design Stormwater Coordinator or District/Regional NPDES Coordinator to discuss the Department's obligations, go to 8 or 5 . $\qquad$ (Dist./Reg. Coordinator initials) |
| :--- |
| If No to all, continue to 5 . | <br>


\hline 5. \& | Are any existing Treatment BMPs partially or completely removed? |
| :--- |
| (ATA condition \#1, Section 4.4.1) | \& \& $\checkmark$ \& | If Yes, go to 8 AND continue to 6 . |
| :--- |
| If No , continue to 6. | <br>


\hline 6. \& Is this a Routine Maintenance Project? \& \& $\checkmark$ \& | If Yes, go to 9 . |
| :--- |
| If No , continue to 7 . | <br>


\hline 7. \& Does the project result in an increase of one acre or more of new impervious surface (NIS)? \& $\checkmark$ \& \& | If Yes, go to 8 . |
| :--- |
| If No , go to 9 . | <br>

\hline 8. \& Project is required to implement Treatment BMPs. \& \multicolumn{3}{|l|}{Complete Checklist T-1, Part 1. (To be completed in PA/ED Phase)} <br>
\hline 9. \& Project is not required to implement Treatment BMPs.
$\qquad$ (Dist./Reg. Design SW Coord. Initials)
$\qquad$ (Project Engineer Initials) (Date) \& \multicolumn{3}{|l|}{Document for Project Files by completing this form and attaching it to the SWDR.} <br>
\hline
\end{tabular}

## Risk Level Determination Documentation

Figure 1. $R$ factor $($ Value $=43.91)$

## Facility Information

Start Date: 07/01/2028

End Date: 02/28/2030

## Calculation Results

Rainfall erosivity factor (R Factor) $=43.91$
A rainfall erosivity factor of 5.0 or greater has been calculated for your site's period of construction.
You do NOT qualify for a waiver from NPDES permitting requirements and must seek Construction General Permit (CGP)
coverage. If you are located in an area where EPA is the permitting authority, you must submit a Notice of Intent (NOI) through the NPDES eReporting Tool (NeT).Otherwise, you must seek coverage under your state's CGP.

Source: https://www.epa.gov/npdes/rainfall-erosivity-factor-calculator-small-construction-sites


Source: : $\underline{\text { http://caltransesp.com/stormdrainsysteminventory-q10348-TMDL Map Tool.aspx }}$

Figure 2. K factor from GIS Map (Value $=0.32$ )


Source: http://svctenvims.dot.ca.gov/wqpt/wqpt.aspx

Figure 3. LS factor from GIS Map (Value $=7.89$ )


Source: http://svctenvims.dot.ca.gov/wqpt/wqpt.aspx

Figure 4. Receiving Water Risk GIS Map


Source: http://svctenvims.dot.ca.gov/wqpt/wapt.aspx

Figure 5. Sediment Risk factor Worksheet

| Sediment Risk Factor Worksheet |  | Entry |
| :---: | :---: | :---: |
| A) R Factor |  |  |
| Analyses of data indicated that when factors other than rainfall are held constant, soil loss is directly proportional to a rainfall factor composed of total storm kinetic energy ( E ) times the maximum $30-\mathrm{min}$ intensity ( 130 ) (Wischmeier and Smith, 1958). The numerical value of $R$ is the average annual sum of EI 30 for storm events during a rainfall record of at least 22 years. "Isoerodent" maps were developed based on R values calculated for more than 1000 locations in the Western U.S. Refer to the link below to determine the R factor for the project site. |  |  |
| hitto://cfoub.epa,gov/nodes/stormwater/LEW/lewCalculator.cfm |  |  |
|  | R Factor Value | 43.91 |
| B) K Factor (weighted average, by area, for all site soils) |  |  |
| The soil-erodibility factor K represents: (1) susceptibility of soil or surface material to erosion, (2) transportability of the sediment, and (3) the amount and rate of runoff given a particular rainfall input, as measured under a standard condition. Fine-textured soils that are high in clay have low K values (about 0.05 to 0.15 ) because the particles are resistant to detachment. Coarse-textured soils, such as sandy soils, also have low K values (about 0.05 to 0.2 ) because of high infiltration resulting in low runoff even though these particles are easily detached. Medium-textured soils, such as a silt loam, have moderate K values (about 0.25 to 0.45 ) because they are moderately susceptible to particle detachment and they produce runoff at moderate rates. Soils having a high silt content are especially susceptible to erosion and have high K values, which can exceed 0.45 and can be as large as 0.65 . Silt-size particles are easily detached and tend to crust, producing high rates and large volumes of runoff. Use Site-specific data must be submitted. |  |  |
| Site-specific K factor quidance |  |  |
|  | K Factor Value | 0.32 |
| C) LS Factor (weighted average, by area, for all slopes) |  |  |
| The effect of topography on erosion is accounted for by the LS factor, which combines the effects of a hillslope-length factor, L, and a hillslope-gradient factor, S. Generally speaking, as hillslope length and/or hillslope gradient increase, soil loss increases. As hillslope length increases, total soil loss and soil loss per unit area increase due to the progressive accumulation of runoff in the downslope direction. As the hillslope gradient increases, the velocity and erosivity of runoff increases. Use the LS table located in separate tab of this spreadsheet to determine LS factors. Estimate the weighted LS for the site prior to construction. |  |  |
| LS Table |  |  |
|  | LS Factor Value | 7.89 |
| Watershed Erosion Estimate (=RxKxLS) in tons/acre | tons/acre 110 | 863968 |
| Site Sediment Risk Factor | sk Factor | High |
| Low Sediment Risk: < 15 tons/acre | tons/acre |  |
| Medium Sediment Risk: $>=15$ and $<75$ tons/acre High Sediment Risk: $>=75$ tons/acre | tons/acre |  |

Figure 6. Risk Level Determination (Value = Risk Level 2)


## SWDR Summary Spreadsheets

| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWDR <br> Signed Date | District | EA/Project ID | County | Route | Beg_PM | End_PM | Project Description | Project Phase | Long SWDR | Risk Level | $\begin{aligned} & \text { DSA } \\ & \text { (ac) } \end{aligned}$ | TMDL Waterbody |
| 6/17/2022 | 12 | 12-00670K | ORA | 133 | 0.96 | 3.41 | Improvement of SR-133 corridor extending 2.5 miles from Canyon Acres Drive to El Toro Road in the City of Laguna Beach, Orange County. | PID | Yes | RL2 | 6.81 | Yes |


| 15 | 16 | 17 | 18 | 19 | CNo 20 | 21 | 22 | 23 | 24 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detention | Infiltration <br> Devices | GSRD | TST | MedFiter | DPPIA | SA | Other BMP | Est. <br> Const_Start | Est. Const <br> _Comp |
| 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |


| 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Net New Impervious area ( NNI ) | Replaced Impervious Surface (RIS) | Additional Treatment Area (ATA) | Post <br> Const <br> Treatment <br> Area (ac) | Treated Impervious Area (ac) | Treated Impervious Area Balance (ac) | Treated Pervious Area (ac) | Stabilized <br> Area (ac) | MWELO | RSA | SW <br> Comment |
| 1.14 | 5.67 | 0.00 | 6.81 | 0.00 | -6.81 | 0.00 | 0.00 |  | No |  |

## ATTACHMENT G

## ALTERNATIVES SCREENING PROCESS AND EVALUATION MATRIX

Southbound


Northbound

(1) Grey icons indicate the alterative does not meet criteria

## Evaluation Criteria

|  | High | Medium | Low |
| :--- | :---: | :---: | :---: |
| Undergrounding Outside <br> Travel Lanes/Safety | Greater than 19' | Between 12' and 19' | Less than 12' |
| Off-Street Bicycle <br> Facilities | Bicycle Only | Greater than 12' <br> shared-use path | 12' shared-use path |
| Pedestrian Sidewalk <br> or Path | Dedicated, separate <br> pedestrian path | Bike facility-adjacent <br> pedestrian path | Shared-use path |
| Bus Stop Compatability | Dedicated bus stop | Remove parking <br> to accommodate <br> bus stop | Shared bus stop with <br> bike lane |
| Emergency Access | Greater than 3 <br> evacuation lanes, <br> 1 emergency lane | 3 evacuation lanes, <br> 1 emergency lane | Less than 3 <br> evacuation lanes, <br> 1 emergency lane |
| Breakdown Shoulder | Dedicated Shoulder | Bike lane | Parking lane <br> On-Street Bicycle <br> Facilities <br> On-Street Parking$\quad$ Painted Buffer |
| Greater than 5' | 5' |  |  |

LAGUNA CANYON ROAD COMPLETE STREETS (EI Toro Road to Canyon Acres Drive)
No Build

| Alternative | Undergrounding <br> Outside Travel <br> Lanes/Safety | Off-Street <br> Bicycle Facilities | Pedestrian <br> Sidewalk or Path | Bus Stop <br> Compatibility | Emergency <br> Access | Breakdown <br> Shoulder |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No-Build |  |  |  |  | On-Street <br> Bicycle Facilities | On-Street <br> Parking |



## Description:

The existing condition on Laguna Canyon Road between El Toro Road and Canyon Acres Drive is a $34^{\prime}$ roadway comprised of two $12^{\prime}$ travel lanes and a $10^{\prime}$ center turn lane. Some segments have a paved shoulder which varies throughout. The right-of-way (ROW) varies from a minimum of 53', in the vicinity of the "Big Bend" area, to a maximum of 218', but the median ROW is 73'. Currently the roadway is bordered on both the northbound and southbound sides of the road by utility poles.

The following alternative alignments for Laguna Canyon Rd - SR 133 assume that the utility poles on both the northbound and southbound sides of the road would be undergrounded to allow full use of the ROW.

LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)
Alternative 1
Alternative 1.1
(TYPICAL)


Alternative 1.2 (CONSTRAINED)


## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative includes narrowed 11 'travel lanes, for traffic calming, and a $10^{\prime}$ center turn lane, a pedestrian path on the northbound side of the road, and a Class I shared-use path on the southbound side. The option also includes on-street Class II bike lanes on both the northbound and southbound side, and during emergencies there is space for 3 outbound evacuation travel lanes and 1 inbound emergency vehicle lane.

## Constrained Features:

The constrained $58^{\prime}$ condition reduces the width of the buffer on the southbound side, requiring the addition of a k -rail or other vertical barrier. The northbound Class II bike lane will receive a 2' buffer, while the southbound Class II bike lane will end during the constrained condition, requiring cyclists to enter the shared-use path or take the travel lane. At the pinch point of $53.1^{\prime}$ the northbound pedestrian path and buffer could be removed, and replaced by a small 2 ' shoulder outside the bike lane.

## LAGUNA CANYON ROAD COMPLETE STREETS (EI Toro Road to Canyon Acres Drive)

Alternative 2

Evaluation Summary:

| Alternative | Undergrounding <br> Outside Travel <br> Lanes/Safety | Off-Street <br> Bicycle Facilities | Pedestrian <br> Sidewalk or Path | Bus Stop <br> Compatibility | Emergency <br> Access | Breakdown <br> Shoulder |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt.2 |  |  |  |  |  | On-Street <br> Bicycle Facilities |

Alternative 2.1 (TYPICAL)


Alternative 2.2 (CONSTRAINED)


## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative includes narrowed 11'travel lanes, for traffic calming, and a 10' center turn lane, a pedestrian path on the northbound side of the road, and a Class I shared-use path on the southbound side. The option provides a parking lane/shoulder on the northbound side of the road, and during emergencies there is space for 3 outbound evacuation travel lanes and 1 inbound emergency vehicle lane.

## Constrained Features:

The constrained condition reduces widths of the pedestrian path, the parking lane, and the shared-use path. The buffer on the southbound side is narrowed and includes a K-Rail or other vertical barrier. At the pinch point of 53.1 ' the pedestrian path on the northbound side could be removed.
alta

LAGUNA CANYON ROAD COMPLETE STREETS (EI Toro Road to Canyon Acres Drive) Alternative 3

## Evaluation

 Summary:| Alternative | Undergrounding <br> Outside Travel <br> Lanes/Safety | Off-Street <br> Bicycle Facilities | Pedestrian <br> Sidewalk or Path | Bus Stop <br> Compatibility | Emergency <br> Access | Breakdown <br> Shoulder | On-Street <br> Bicycle Facilities | On-Street <br> Parking |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt.3 |  |  |  |  |  |  |  |  |



Alternative 3.2 (CONSTRAINED)

## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative has 12 ' travel lanes, and a $10^{\prime}$ center turn lane, a pedestrian path on the northbound side of the road, and a Class I shared-use path on the southbound side. This option includes a parking lane/shoulder and during emergencies there is space for 3 outbound evacuation lanes and 1 inbound emergency vehicle lane, additionally the shared-use path on the southbound side has a mountable curb and could be used in emergencies as an emergency vehicle lane.

## Constrained Features:

The constrained condition removes the parking lane and widens the northbound pedestrian path and widens the buffer along the southbound shared-use path. At the pinch point of 53.1 'the width of the shared-use path and the pedestrian path on the northbound side could be reduced.

## LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)

Alternative 4


Alternative 4.1
(TYPICAL)


Alternative 4.2 (CONSTRAINED)

## Typical Features

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative includes $12^{\prime}$ 'travel lanes, and a $10^{\prime}$ center turn lane, a pedestrian path on the northbound side of the road, and one-directional Class IV separated bikeways with buffers with flexible posts on both sides. The option provides a parking lane/shoulder on the north bound side of the road, and during emergencies there is space for 3 outbound evacuation lanes and 1 inbound emergency vehicle lane.

## Constrained Features:

The constrained condition removes the southbound bike lane buffer, leaving a Class II bike lane, and narrows the travel lanes to 11'. At the pinch point of 53.1 'the parking could be removed, or alternatively the northbound bike lane buffer could be removed, and the pedestrian path could transition to a more narrow paved shoulder outside the bike lane.

LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)
Alternative 5



## Typical Features:

This alternative proposes a typical width of 64 ' including the vehicle, pedestrian and bicycle facilities. The alternative includes $12^{\prime}$ travel lanes, and a 10 ' center turn lane, and a pedestrian path on the northbound side of the road. The option includes one-directional Class IV separated bikeways on both sides of the road, and provides a parking lane on the north bound side of the road. During emergencies there is space for 3 outbound evacuation travel lanes and 1 inbound emergency vehicle lane.

Alternative 5.2 (CONSTRAINED)



## Constrained Features:

The constrained condition narrows the travel lanes to 11 'and narrows the Class IV bikeways as well as the buffer on the northbound side. At the pinch point of 53.1 ' the parking lane on the northbound side would be removed.

## LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)

Alternative 6

| Evaluation | Alternative | Undergrounding Outside Travel Lanes/Safety | Off-Street Bicycle Facilities | Pedestrian Sidewalk or Path | Bus Stop Compatibility | Emergency Access | Breakdown Shoulder | On-Street Bicycle Facilities | On-Street Parking |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Summary: | Alt. 6 |  |  |  |  |  |  |  | $\uparrow$ |



Alternative 6.2 (CONSTRAINED)

Typical Features:
This alternative proposes a typical width of 64 ' including the vehicle, pedestrian and bicycle facilities. The alternative includes narrowed 11'travel lanes for traffic calming, and a 10' center turn lane. The option includes a Class IV separated bikeway on the southbound side of the roadway, buffered with a flexible post or other vertical barrier. Adjacent to the separated bikeway is a bus stop/shoulder lane. During emergencies there is space for 4 outbound evacuation travel lanes on the roadway and 1 inbound emergency vehicle lane

## Constrained Features:

The constrained condition removes the southbound bus stop/shoulder and the adjacent bikeway becomes Class I shared-use path with a more narrow buffer with a flexible post or other vertical barrier. At the pinch point of 53.1' the northbound parking lane would end.

LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)
Alternative 7 (Former Alt. F.1)
Evaluation
Summary:

| Alternative | Undergrounding <br> Outside Travel <br> Lanes/Safety | Off-Street <br> Bicycle Facilities | Pedestrian <br> Sidewalk or Path | Bus Stop <br> Compatibility | Emergency <br> Access | Breakdown <br> Shoulder | On-Street <br> Bicycle Facilities |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt. 7 <br> (former Alt. F.1) |  |  |  |  | On-Street <br> Parking |  |  |

Alternative 7.1
(TYPICAL)


## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative has $12^{\prime}$ travel lanes, and provides a $12^{\prime}$ center turn lane. On the southbound side is a Class IV separated bikeway with an adjacent pedestrian path. The option provides a Class II bike lane/shoulder on the northound side. During emergencies there is space for 3 outbound evacuation travel lanes and 1 inbound emergency vehicle lane. Additionally the bikeway and pedestrian path on the southbound side have a mountable curb and could be used in emergencies as an emergency vehicle lane.

## Constrained Features:

The constrained condition reduces widths of the pedestrian path, the travel lanes and the center turn lane. At the pinch point of 53.1' the center turn lane could be removed, or alternatively the northbound bike lane could be narrowed and the southbound pedestrian path could be removed, making the Class IV bikeway a shared-use path, requiring the addition of a K-Rail or vertical barrier in the buffer area.


LAGUNA CANYON ROAD COMPLETE STREETS (EI Toro Road to Canyon Acres Drive)
Alternative 8 (Former Alt. F.2)

| Evaluation Summary: | Alternative | Undergrounding Outside Travel Lanes/Safety | Off-Street Bicycle Facilities | Pedestrian Sidewalk or Path | Bus Stop Compatibility | Emergency Access | Breakdown Shoulder | On-Street Bicycle Facilities | On-Street Parking |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Alt. 8 (former Alt. F.2) |  |  |  |  |  |  |  |  |

Alternative 8.1 (TYPICAL)

## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative includes narrowed 11'travel lanes for traffic calming, and a $10^{\prime}$ center turn lane, as well there is a pedestrian path on the northbound side of the road. The option includes a Class IV separated bikeway with adjacent pedestrian path on the southbound side. The option also provides a Class II bike lane on the northbound side of the road. During emergencies there is space for 3 outbound evacuation travel lanes and 1 inbound emergency vehicle lane, additionally the bikeway and pedestrian path on the southbound side have a mountable curb and could be used in emergencies as an emergency vehicle lane.

## Constrained Features:

The constrained condition removes the pedestrian path on the southbound side. At the pinch point of 53.1 ' the pedestrian path on the northbound side could be removed.

LAGUNA CANYON ROAD COMPLETE STREETS (EI Toro Road to Canyon Acres Drive)
Alternative 9 (Former Alt. G)
Evaluation Summary:

| Alternative | Undergrounding <br> Outside Travel <br> Lanes/Safety | Off-Street <br> Bicycle Facilities | Pedestrian <br> Sidewalk or Path | Bus Stop <br> Compatibility | Emergency <br> Access | Breakdown <br> Shoulder | On-Street <br> Bicycle Facilities | On-Street <br> Parking |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt. 9 <br> (former Alt. G) |  |  |  |  |  |  |  |  |

Alternative 9.1
(TYPICAL)


## Typical Features:

This alternative proposes a typical width of $64^{\prime}$ including the vehicle, pedestrian and bicycle facilities. The alternative includes 12 ' travel lanes, and a $10^{\prime}$ center turn lane, a pedestrian path on both sides of the road, and a Class II buffered bike lane on both sides. During emergencies there is space for 4 outbound evacuation travel lanes and 1 inbound emergency vehicle lane.

## Constrained Features:

The constrained condition reduces widths bike lanes as well as the travel lanes. At the pinch point of 53.1'a pedestrian path on the either side could be removed, or alternatively the bike lane buffers could be removed.


## LAGUNA CANYON ROAD COMPLETE STREETS (El Toro Road to Canyon Acres Drive)

## CLASS I

## Shared-Use Path

Provides a completely separated right of way for the exclusive use of bicycles and pedestrians with crossflow minimized.


14'min. total width recommended/preferred ( $10^{\prime}$ paved width, $2^{\prime}$ clear shoulders) $8^{\prime} \mathrm{min}$. paved width required $2^{\prime}$ gravel shoulders required $12^{\prime} \mathrm{min}$. total width required


## CLASS II

## Bike Lane

Provides a striped lane for one-way bike travel on a street or highway.



## CLASS III

## Bike Route

Provides for shared use with pedestrian or motor vehicle traffic, typically on lower volume roadways.


## CLASS IV

## Separated Bikeway

Provides a separated path for one-way bicycle travel adjacent to a street or highway. Bicycles are separated from motor vehicle traffic by a raised curb, bollards, parking with a painted buffer, or other vertical physical barrier.


## ATTACHMENT H

## RIGHT-OF-WAY DATA SHEETS

To: Jennifer Pham
Office Chief Date: $\quad$ 6-17-22

Office of Right of Way and Right of Way Engineering

$$
\text { Co. ORA Rte. } 133
$$

$\qquad$

Expense Authorization 0Q670K Project ID \#1217000086

## Subject: RIGHT OF WAY DATA SHEET - LOCAL PUBLIC AGENCIES

Project Description: Improve SR-133 (Laguna Canyon Road) between Canyon Acres Drive \& El Toro Road Alternative 1 - No Build

Right of way necessary for the subject project will be the responsibility of $\qquad$ City of Laguna Beach

The information in this data sheet was developed by $\qquad$
$\qquad$

## I. Right of Way Engineering

Will Right of Way Engineering be required for this project alternative?

- No X
- Yes $\qquad$


## II. Engineering Surveys

1. Is any surveying or photogrammetric mapping required?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Complete the following.) }
$$

2. Datum Requirements

Yes $\qquad$ Project will adhere to the following criteria:

No $\qquad$ Provide an explanation on additional page.

No Build alternative. No R/W work.
3. Will land survey monument perpetuation be scoped into the project, if required?

Yes $\qquad$
No X Provide explanation on additional page.
No Build alternative. No R/W work.

## III. Parcel Information (Land and Improvements)

Are there any property rights required within the proposed project limits?
No $\quad \mathrm{X}$ Yes ___ (Complete the following.)
A. Number of Vacant Land Parcels
B. Number of Single Family Residential Units
C. Number of Multifamily Residential Units
D. Number of Commercial/Industrial Parcels
E. Number of Farm/Agricultural Parcels
F. Permanent and/or Temporary Easements
G. Other Parcels (define in "Remarks" section)

Totals
$\qquad$ \$ $\qquad$
\$ $\qquad$
\$ $\qquad$
$\qquad$
$\qquad$ \$ $\qquad$
$\qquad$
$\qquad$ \$ $\qquad$
$\qquad$
$\qquad$ \$ $\qquad$
$\qquad$ \$ $\qquad$


Provide a general description of the right of way and excess lands required (zoning, use, improvements, critical, or sensitive parcels, etc.).

No Build alternative. No right of way required.

## IV. Dedications

Are there any property rights which have been acquired, or anticipate will be acquired, through the "dedication" process for the Project?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Complete the following.) }
$$

Number of dedicated parcels
Have the dedication parcel(s) been accepted by the municipality involved? No dedications.

## V. Excess Lands / Relinquishments

Are there Caltrans property rights which may become excess lands or potential relinquishment areas?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Provide an explanation on additional page.) }
$$

## VI. Relocation Information

Are relocation displacements anticipated?
No $\underline{X} \quad$ Yes ___ (Complete the following.)
A. Number of Single Family Residential Units

Estimated RAP Payments $\qquad$
B. Number of Multifamily Residential Units

Estimated RAP Payments $\qquad$
C. Number of Business/Nonprofit

Estimated RAP Payments
$\qquad$
\$ $\qquad$
D. Number of Farms

Estimated RAP Payments
$\qquad$
\$ $\qquad$
E. Other (define in the "Remarks" section)

Estimated RAP Payments
$\qquad$
\$ $\qquad$

Totals $\qquad$ \$ $\qquad$

## VII. Utility Relocation Information

Do you anticipate any utility facilities or utility rights of way to be affected?

$$
\text { No } \underline{X} \quad \text { Yes } \xrightarrow{\mathrm{X}} \text { (Complete the following.) }
$$

| Facility | Owner | Estimated Relocation Expense (Thousands)* |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | State <br> Obligation | Local Obligation* | Utility Owner Obligation |
| A. Electrical (Transmission) |  | \$0 | \$0 | \$0 |
| B. Electrical (Distribution) |  | \$0 | \$0 | \$0 |
| C. Gas |  | \$0 | \$0 | \$0 |
| D. Sewer |  | \$0 | \$0 | \$0 |
| E. Water |  | \$0 | \$0 | \$0 |
| F. Fiber Optics / <br> Telephone / <br> Wireless (combined) |  | \$0 | \$0 | \$0 |
| G. Streetlight conduits |  | \$0 | \$0 | \$0 |
| Totals |  | \$0 | \$0 | \$0 |

Alternative 1

Number of facilities

| 0 | 0 | 0 |
| :--- | :--- | :--- |

Any additional information concerning utility involvement on this project?
No Build alternative. No right of way required

## VIII. Rail Information

Are railroad facilities or railroad rights of way affected?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Describe railroad facilities or railroad rights of way affected.

| Owner's Name | Transverse Crossing | Longitudinal Encroachment |
| :--- | :--- | :--- |
| A. |  |  |
| B. |  |  |

Discuss types of agreements and rights required from the railroads. Are grade crossings that require services contracts, or grade separations that require construction and maintenance agreements involved?

## IX. Clearance Information

Are there improvements that require clearance?

$$
\text { No } X \quad \text { Yes ___ (Complete the following.) }
$$

A. Number of Structures to be Demolished Estimated Cost of Demolition
$\qquad$
\$ $\qquad$
X. Hazardous Materials/Waste

Are there any site(s) and/or improvements(s) in the Project Limits that are known to contain
hazardous materials? None X_Y_ (Explain in the "Remarks" section.)
Are there any site(s) and/or improvement(s) in the Project Limits that are suspected to contain
hazardous waste? None X Y___ (Explain in the "Remarks" section.)

## XI. Project Scheduling

|  | Proposed lead time |  |
| :--- | :--- | :---: |$\quad$| Completion date |
| :---: |
| * Preliminary Engineering, Surveys |
| * R/W Engineering Submittals |
| * R/W Appraisals/Acquisition |
| Proposed Environmental Clearance |

Alternative 1

## XII. Proposed Funding

NOTE: Potential funding sources to be determined.


## XIII. Remarks <br> None

Project Sponsor Consultant
HDR Engineering, Inc.
Prepared by:
Staple Wa. Coned
Stephen P.A. Crouch, PE; Project Engineer, HDR Engineering, Inc.


Jill Craig, ROW Agent, HDR Engineering, Inc.


Project Sponsor
City of Laguna Beach
Reviewed and Approved by:


Thomas Perez; Capital Progran Manager;
City of Lagena Beach Public Works

06/17/2022
Date

Caltrans
Reviewed and approved based on information provided to date:


Linda Lundblad, Branch Chief Right of Way - Appraisals, Condemnation \& Local Programs

08/09/2022
Date

To: Jennifer Pham
Office Chief Date: $\quad 6$-17-22

Office of Right of Way and Right of Way Engineering

Attention: Linda Lundblad
District Branch Chief
R/W Local Programs

Co. ORA Rte. 133

Expense Authorization 0Q670K Project ID \#1217000086

## Subject: RIGHT OF WAY DATA SHEET - LOCAL PUBLIC AGENCIES

Project Description: Improve SR-133 (Laguna Canyon Road) between Canyon Acres Drive \& El Toro Road - Alternative 2

Right of way necessary for the subject project will be the responsibility of $\qquad$ City of Laguna Beach

The information in this data sheet was developed by $\qquad$ HDR Engineering, Inc. $\qquad$

## I. Right of Way Engineering

Will Right of Way Engineering be required for this project?

- No $\qquad$
- Yes X
- Hard copy (base map)
- Appraisal map
- Acquisition Documents
- Property Transfer Documents
- R/W Record Map
- Record of Survey

| $\frac{X}{X}$ |
| :--- |
| $X$ |
| $X$ |
| $X$ |

## II. Engineering Surveys

1. Is any surveying or photogrammetric mapping required?

$$
\text { No ___ Yes } \xlongequal{\mathrm{X}} \text { (Complete the following.) }
$$

2. Datum Requirements

Yes X Project will adhere to the following criteria:

- Horizontal - datum policy is NAD 83, CA-HPGN, EPOCH 1991.35 and English system of units and measures.
- Vertical - datum policy is NAVD 88.
- Units - metric is not required.

No $\qquad$ Provide an explanation on additional page.
3. Will land survey monument perpetuation be scoped into the project, if required?

Yes $\qquad$

No $\qquad$ Provide explanation on additional page.

## III. Parcel Information (Land and Improvements)

Are there any property rights required within the proposed project limits?

$$
\text { No ___ Yes } \quad \text { X__ (Complete the following.) }
$$

A. Number of Vacant Land Parcels
B. Number of Single Family Residential Units
C. Number of Multifamily Residential Units
D. Number of Commercial/Industrial Parcels
E. Number of Farm/Agricultural Parcels
F. Permanent Easements
G. Other Parcels/Temporary Easements

Totals
$\qquad$
$\qquad$
2

83

85
\$
\$ $\qquad$
\$ $\qquad$
\$ $\qquad$
\$ $\qquad$
\$ 560,956
\$ 1,970,384
\$ 2,531,340

Provide a general description of the right of way and excess lands required (zoning, use, improvements, critical, or sensitive parcels, etc.).

In Alternative 2 there are a total of two permanent easements and 83 temporary easements needed for the project. The two permanent easements consist of approximately 5,100 sf. of highway easement from the County of Orange and Laguna College of Art \& Design. The temporary easements consist of approximately 188,898 sf. needed from commercial, industrial, single family and multiple residential, and government owned properties. Parcels own by the City of Laguna Beach are not included in this measurement. These temporary easements are expected to be needed for construction purposes. For estimating purposes, it is assumed that the temporary easement will need a width of 10 ' of each parcel's frontage adjacent to proposed sidewalk. It is also assumed that the easements will be needed for a three-year period. The government owned properties needed for construction purposes (excluding the City of Laguna Beach) are proposed to be procured through each government entities' permitting process and not by fee. Costs for these properties include only the services needed to obtain the permits.
RIGHT OF WAY DATA SHEET FOR LOCAL PUBLIC AGENCIES (Cont.)

| EXHIBIT |
| :--- |
| (Form \#) | | 17-EX-21 (NEW 12/2007) |
| :--- |
| Page 3 of 7 |

IV. Dedications

Are there any property rights which have been acquired, or anticipate will be acquired, through the "dedication" process for the Project?

No $\xlongequal{\mathrm{X}} \quad$ Yes ___ (Complete the following.)
Number of dedicated parcels $\qquad$ 0

Have the dedication parcel(s) been accepted by the municipality involved? N/A

## V. Excess Lands/Relinquishments

Are there Caltrans property rights which may become excess lands or potential relinquishment areas?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes } \quad \text { (Provide an explanation on additional page.) }
$$

VI. Relocation Information

Are relocation displacements anticipated?
No $\underline{\mathrm{X}} \quad \mathrm{Yes} \quad$ (Complete the following.)
A. Number of Single Family Residential Units

Estimated RAP Payments
B. Number of Multifamily Residential Units

Estimated RAP Payments
C. Number of Business/Nonprofit

Estimated RAP Payments
D. Number of Farms

Estimated RAP Payments
E. Other (define in the "Remarks" section)

Estimated RAP Payments

Totals
$\qquad$
\$
$\qquad$
\$ $\qquad$
$\qquad$
\$ $\qquad$
$\qquad$
\$ $\qquad$
$\qquad$
\$ $\qquad$
\$ $\qquad$

## VII. Utility Relocation Information

Do you anticipate any utility facilities or utility rights of way to be affected?

$$
\text { No } \quad \text { Yes } \quad \mathrm{X} \quad \text { (Complete the following.) }
$$

|  |  | Estim | ocation Expe | ousands)* |
| :---: | :---: | :---: | :---: | :---: |
| Facility | Owner | State <br> Obligation | Local Obligation* | Utility Owner Obligation |
| A. Electrical (Transmission) | SOUTHERN CALIFORNIA EDISON | \$0 | \$22,600 | \$ |
| B. Electrical (Distribution) | SOUTHERN <br> CALIFONIA EDISON | \$0 | \$23,700 | \$ |
| C. Gas | SOUTHERN <br> CALIFORNIA GAS | \$0 | \$2,500 | \$ |
| D. Sewer | CITY OF LAGUNA BEACH | \$0 | \$1,750 | \$ |
| E. Water | LaGUNA BEACH COUNTY WATER DIST | \$0 | \$1,750 | \$ |
| F. Fiber Optics / <br> Telephone / Wireless (combined) | CROWN CASTLE- LA <br> \& VEN <br> SPRINT <br> T-MOBILE USA <br> FRONTIER <br> COX <br> COMMUNICATIONS <br> extenet systems, INC | \$0 | \$3,000 | \$ |
| G. Streetlight conduits | SOUTHERN <br> CALIFONIA EDISON | \$0 | \$750 | \$ |
| Totals |  | \$0 | \$56,050 | \$ |
| Number of facilities |  | TBD | 7 | TBD |

## *NOTE: Share of obligation is unknown at this time. Estimate totals placed in Local Obligation until further investigation.

Any additional information concerning utility involvement on this project?
This project undergrounds overhead utilities within the right-of-way to outside of the travel lanes where feasible.

## SCE Transmission

SCE has approximately 2.5 pole-miles of $66-\mathrm{kV}$ single circuit and double circuit transmission lines. The transmission lines are on wood poles and for the most part located on the southbound side of Laguna Canyon Road with sections also located on the northbound side of the roadway.

SCE Distribution
SCE also has 2.5 pole-miles of overhead distribution lines placed as underbuild on the same poles as the $66-\mathrm{kV}$ transmission lines although at some locations the distribution lines are on separate poles.

## Telecommunications

It is proposed that all overhead telecommunication lines be undergrounded in conjunction with the electrical lines as part of the project so that all overhead poles can be removed to improve safety. It is likely that the various owners' lines could be located within a joint trench within the new roadway section. Other potential conflicts such as with wireless communication towers will have to be investigated.

## Streetlights

The City will take ownership of the streetlights within the project limits and will install them under a separate project concurrent with the proposed undergrounding.

## SCG Gas

SCG has a gas line that exists along northbound side of the roadway for the length of the project. It is assumed that the existing gas lines will have to be relocated outside of the proposed roadway for the length of the project.

## City of Laguna Beach Sewer

The City of Laguna Beach has a sewer line along northbound side of the roadway for the length of the project. For this stage of the project it is unknown if the sewer line can remain in place. As such it is assumed that the sewer line will be relocated.

## Laguna Beach County Water District

The Laguna Beach County Water District has water lines on both sides of the project. It is assumed that the waterline located on the southbound side of the roadway will not require relocation because there are no apparent conflicts; however, further investigation will be required. For the northbound side of the roadway it uncertain if the water lines can remain in place. As such, it is assumed that the waterline on the northbound side of the roadway will be relocated.

## VIII. Rail Information

Are railroad facilities or railroad rights of way affected?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Describe railroad facilities or railroad rights of way affected.

| Owner's Name | Transverse Crossing | Longitudinal Encroachment |
| :--- | :--- | :--- |
| A. |  |  |
| B. |  |  |

Discuss types of agreements and rights required from the railroads. Are grade crossings that require services contracts, or grade separations that require construction and maintenance agreements involved?

## IX. Clearance Information

Are there improvements that require clearance?
No $\begin{aligned} & \mathrm{X} \\ & \text { Yes ___ (Complete the following.) }\end{aligned}$
A. Number of Structures to be Demolished Estimated Cost of Demolition
$\qquad$
$\qquad$

## X. Hazardous Materials/Waste

Are there any site(s) and/or improvements(s) in the Project Limits that are known to contain hazardous materials? None $\quad \mathrm{X} \quad$ Yes ___ (Explain in the "Remarks" section.)

Are there any site(s) and/or improvement(s) in the Project Limits that are suspected to contain
hazardous waste? None $\qquad$ Yes X (Explain in the "Remarks" section.)

## XI. Project Scheduling

|  | Proposed lead time | Completion date |
| :---: | :---: | :---: |
| * Preliminary Engineering, Surveys | 24 (months) | July 2023 |
| * R/W Engineering Submittals | 16 (months) | January 2024 |
| * R/W Appraisals/Acquisition | 16 (months) | January 2024 |
| Proposed Environmental Clearance |  | January 2025 |
| Proposed R/W Certification |  | April 2027 |

## XII. Proposed Funding

NOTE: Potential funding sources to be determined.

|  | Local | State | Federal | Other* |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Acquisition |  |  |  |  | 531,340 |
| Utilities |  |  |  |  | 50,000 |
| Relocation Assistance Program |  |  |  | \$ | 0 |
| R/W Support** |  |  |  |  | 77,500 |
| Other Costs (Env. Review, Demo, etc.) |  |  |  | \$ | 60,000 |

[^12]
## XIII. Remarks

The ISA Checklist for hazardous waste was completed in June 2018 and is included as Attachment J in the PSR/PDS. Potential hazardous waste/materials issues associated with the proposed Project include aeriallydeposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and pad mounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles. A full ISA for all right-of-way acquisition properties and Preliminary Site Investigations (PSI) will be conducted during PA/ED phase.

Project Sponsor Consultant
Prepared by:


Jill Craig, ROW Agent, HDR Engineering, Inc.

## 6/17/2022

Date

Project Sponsor
City of Laguna Beach Reviewed and Approved by:

Stephen P.A. Crouch, PE; Project Engineer, HDR Engineering, Inc.



Thomas Perez; Capital Progran Manager; City of Laguna Beach Public Works

6/17/2022
Date

Caltrans
Reviewed and accent based on information provided to date:


$$
08 / 09 / 2022
$$

Date

To: Jennifer Pham
Office Chief Date: $\underline{6-17-22}$

Office of Right of Way and Right of Way Engineering
Attention: Linda Lundblad
District Branch Chief
R/W Local Programs

Co. ORA Rte. 133

Expense Authorization 0Q670K
Project ID \#1217000086

## Subject: RIGHT OF WAY DATA SHEET - LOCAL PUBLIC AGENCIES

Project Description: Improve SR-133 (Laguna Canyon Road) between Canyon Acres Drive \& El Toro Road - Alternative 3

Right of way necessary for the subject project will be the responsibility of $\qquad$ City of Laguna Beach

The information in this data sheet was developed by $\qquad$ HDR Engineering, Inc. $\qquad$
I. Right of Way Engineering

Will Right of Way Engineering be required for this project?

- No
- Yes X
- Hard copy (base map)
- Appraisal map
- Acquisition Documents
- Property Transfer Documents
- R/W Record Map
- Record of Survey

| X |
| :--- |
| X |
| X |
| X |
| X |

## II. Engineering Surveys

1. Is any surveying or photogrammetric mapping required?

No __ Yes $\xrightarrow{\mathrm{X}}$ (Complete the following.)
2. Datum Requirements

Yes X Project will adhere to the following criteria:

- Horizontal - datum policy is NAD 83, CA-HPGN, EPOCH 1991.35 and English system of units and measures.
- Vertical - datum policy is NAVD 88.
- Units - metric is not required.

No $\qquad$ Provide an explanation on additional page.
3. Will land survey monument perpetuation be scoped into the project, if required?

Yes X
$\qquad$
No $\qquad$ Provide explanation on additional page.

## III. Parcel Information (Land and Improvements)

Are there any property rights required within the proposed project limits?

$$
\text { No } \quad \text { Yes } \quad \mathrm{X} \quad \text { (Complete the following.) }
$$

Part Take Full Take Estimate \$

| A. Number of Vacant Land Parcels |  | \$ |  |
| :---: | :---: | :---: | :---: |
| B. Number of Single Family Residential Units |  | \$ |  |
| C. Number of Multifamily Residential Units |  | \$ |  |
| D. Number of Commercial/Industrial Parcels |  | \$ |  |
| E. Number of Farm/Agricultural Parcels |  | \$ |  |
| F. Temporary Easements | 2 | \$ | 2,170,491 |
| G. Other Parcels / Temporary Easements | 85 | \$ | 743,578 |
| Totals | 87 | \$ | 2,914,089 |

Provide a general description of the right of way and excess lands required (zoning, use, improvements, critical, or sensitive parcels, etc.).

In Alternative 3 there are a total of two permanent easements and 85 temporary easements needed for the project. The two permanent easements consist of approximately 6,760 sf. of highway easement from the County of Orange and Laguna College of Art \& Design. The temporary easements consist of approximately 195,708 sf. needed from commercial, industrial, single family and multiple residential, and government owned properties Parcels own by the City of Laguna Beach are not included in this measurement. These temporary easements are expected to be needed for construction purposes. For estimating purposes, it is assumed that the temporary easement will need a width of $10^{\prime}$ of each parcel's frontage adjacent to proposed sidewalk. It is also assumed that the easements will be needed for a three-year period. The government owned properties needed for construction purposes (excluding the City of Laguna Beach) are proposed to be procured through each government entities' permitting process and not by fee. Costs for these properties include only the services needed to obtain the permits.

## IV. Dedications

Are there any property rights which have been acquired, or anticipate will be acquired, through the "dedication" process for the Project?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Complete the following.) }
$$

Number of dedicated parcels $\qquad$
Have the dedication parcel(s) been accepted by the municipality involved? No dedications expected.

|  |  |
| :--- | :--- |
| RIGHT OF WAY DATA SHEET FOR LOCAL PUBLIC AGENCIES (Cont.) <br> (Form \#) | EXHIBIT <br> 17-EX-21 (NEW 12/2007) <br> Page 3 of 7 |

## V. Excess Lands/Relinquishments

Are there Caltrans property rights which may become excess lands or potential relinquishment areas?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Provide an explanation on additional page.) }
$$

## VI. Relocation Information

Are relocation displacements anticipated?
No $\underline{X} \quad$ Yes ___ (Complete the following.)
A. Number of Single Family Residential Units

Estimated RAP Payments
B. Number of Multifamily Residential Units

Estimated RAP Payments
C. Number of Business/Nonprofit

Estimated RAP Payments
D. Number of Farms

Estimated RAP Payments
E. Other (define in the "Remarks" section)

Estimated RAP Payments

Totals $\qquad$ \$ $\qquad$

## VII. Utility Relocation Information

Do you anticipate any utility facilities or utility rights of way to be affected?

$$
\text { No } \quad \text { Yes } \quad \mathrm{X} \quad \text { (Complete the following.) }
$$

|  |  | Estim | ocation Expe | ousands)* |
| :---: | :---: | :---: | :---: | :---: |
| Facility | Owner | State <br> Obligation | Local Obligation* | Utility Owner Obligation |
| A. Electrical (Transmission) | SOUTHERN CALIFORNIA EDISON | \$0 | \$22,600 | \$ |
| B. Electrical (Distribution) | SOUTHERN <br> CALIFONIA EDISON | \$0 | \$23,700 | \$ |
| C. Gas | SOUTHERN <br> CALIFORNIA GAS | \$0 | \$2,500 | \$ |
| D. Sewer | CITY OF LAGUNA BEACH | \$0 | \$1,750 | \$ |
| E. Water | LaGUNA BEACH COUNTY WATER DIST | \$0 | \$1,750 | \$ |
| F. Fiber Optics / <br> Telephone / Wireless (combined) | CROWN CASTLE- LA <br> \& VEN <br> SPRINT <br> T-MOBILE USA <br> FRONTIER <br> COX <br> COMMUNICATIONS <br> extenet systems, INC | \$0 | \$3,000 | \$ |
| G. Streetlight conduits | SOUTHERN <br> CALIFONIA EDISON | \$0 | \$750 | \$ |
| Totals |  | \$0 | \$56,050 | \$ |
| Number of facilities |  | TBD | 7 | TBD |

## *NOTE: Share of obligation is unknown at this time. Estimate totals placed in Local Obligation until further investigation.

Any additional information concerning utility involvement on this project?
This project undergrounds overhead utilities within the right-of-way to outside of the travel lanes where feasible.

## SCE Transmission

SCE has approximately 2.5 pole-miles of $66-\mathrm{kV}$ single circuit and double circuit transmission lines. The transmission lines are on wood poles and for the most part located on the southbound side of Laguna Canyon Road with sections also located on the northbound side of the roadway.

## SCE Distribution

Alternative 3

SCE also has 2.5 pole-miles of overhead distribution lines placed as underbuild on the same poles as the $66-\mathrm{kV}$ transmission lines although at some locations the distribution lines are on separate poles.

## Telecommunications

It is proposed that all overhead telecommunication lines be undergrounded in conjunction with the electrical lines as part of the project so that all overhead poles can be removed to improve safety. It is likely that the various owners' lines could be located within a joint trench within the new roadway section. Other potential conflicts such as with wireless communication towers will have to be investigated.

## Streetlights

The City will take ownership of the streetlights within the project limits and will install them under a separate project concurrent with the proposed undergrounding.

## SCG Gas

SCG has a gas line that exists along northbound side of the roadway for the length of the project. It is assumed that the existing gas lines will have to be relocated outside of the proposed roadway for the length of the project.

## City of Laguna Beach Sewer

The City of Laguna Beach has a sewer line along northbound side of the roadway for the length of the project. For this stage of the project it is unknown if the sewer line can remain in place. As such it is assumed that the sewer line will be relocated.

## Laguna Beach County Water District

The Laguna Beach County Water District has water lines on both sides of the project. It is assumed that the waterline located on the southbound side of the roadway will not require relocation because there are no apparent conflicts; however, further investigation will be required. For the northbound side of the roadway it uncertain if the water lines can remain in place. As such, it is assumed that the waterline on the northbound side of the roadway will be relocated.

## VIII. Rail Information

Are railroad facilities or railroad rights of way affected?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Describe railroad facilities or railroad rights of way affected.

| Owner's Name | Transverse Crossing | Longitudinal Encroachment |
| :--- | :--- | :--- |
| A. |  |  |
| B. |  |  |

Discuss types of agreements and rights required from the railroads. Are grade crossings that require services contracts, or grade separations that require construction and maintenance agreements involved?

## IX. Clearance Information

Are there improvements that require clearance?

$$
\text { No } \mathrm{X} \quad \text { Yes } \quad \text { (Complete the following.) }
$$

A. Number of Structures to be Demolished
$\qquad$
\$ $\qquad$

## X. Hazardous Materials/Waste

Are there any site(s) and/or improvements(s) in the Project Limits that are known to contain hazardous materials? None X_Yes__ (Explain in the "Remarks" section.)

Are there any site(s) and/or improvement(s) in the Project Limits that are suspected to contain
hazardous waste? None $\qquad$ Yes X (Explain in the "Remarks" section.)

## XI. Project Scheduling

|  | Proposed lead time | Completion date |
| :---: | :---: | :---: |
| * Preliminary Engineering, Surveys | 24 (months) | July 2023 |
| * R/W Engineering Submittals | 16 (months) | January 2024 |
| * R/W Appraisals/Acquisition | 16 (months) | January 2024 |
| Proposed Environmental Clearance |  | January 2025 |
| Proposed R/W Certification |  | April 2027 |

## XII. Proposed Funding

NOTE: Potential funding sources to be determined.

|  | Local | State | Federal | Other* |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Acquisition |  |  |  |  | 14,089 |
| Utilities |  |  |  |  | 60,000 |
| Relocation Assistance Program |  |  |  | \$ | 0 |
| R/W Support** |  |  |  |  | 28,500 |
| Other Costs (Env. Review, Demo, etc.) |  |  |  |  | 60,000 |

> *Proposed funding to be determined. Purpose of PSR is to obtain funding and potential funding sources.
> $* * R / W$ Support costs include costs for engineering, appraisals, etc. ROW cost estimate is assumed to be probable to optimistic.

## XIII. Remarks

The ISA Checklist for hazardous waste was completed in June 2018 and is included as Attachment J in the PSR/PDS. Potential hazardous waste/materials issues associated with the proposed Project include aeriallydeposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and padmounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles. A full ISA for all right-of-way acquisition properties and Preliminary Site Investigations (PSI) will be conducted during PA/ED phase.

Alternative 3

Project Sponsor Consultant
HDR Engineering, Inc.
Prepared by:


Stephen P.A. Crouch, PE; Project Engineer, HDR Engineering, Inc.


Jill Craig, ROW Agent, HDR Engineering, Inc.

06/17/2022
Date

Project Sponsor
City of Laguna Beach
Reviewed and Approved by:


Thomas Perez; Capital Pr gram Manager;
City of Laguna Beach Public Works

6/17/2022
Date

Caltrans
Reviewed and accent based on information provided to date:


Linda Lundblad, Branch Chief
Right of Way - Appraisals,
Condemnation \& Local Programs

08/09/2022
Date

To: Jennifer Pham
Office Chief Date: $\quad$ 6-17-22

Office of Right of Way and Right of Way Engineering
Attention: Linda Lundblad
District Branch Chief
R/W Local Programs

Co. ORA Rte. $\qquad$

Expense Authorization 0Q670K Project ID \#1217000086

## Subject: RIGHT OF WAY DATA SHEET - LOCAL PUBLIC AGENCIES

Project Description: Improve SR-133 (Laguna Canyon Road) between Canyon Acres Drive \& El Toro Road - Alternative 4

Right of way necessary for the subject project will be the responsibility of $\qquad$
City of Laguna Beach
The information in this data sheet was developed by $\qquad$ HDR Engineering, Inc. $\qquad$
I. Right of Way Engineering

Will Right of Way Engineering be required for this project?

- No
- Yes X
- Hard copy (base map)
- Appraisal map
- Acquisition Documents
- Property Transfer Documents
- R/W Record Map
- Record of Survey

| $\frac{X}{X}$ |
| :--- |
| $X$ |
| $X$ |
| $X$ |

## II. Engineering Surveys

1. Is any surveying or photogrammetric mapping required?

No __ Yes $\xrightarrow{\mathrm{X}}$ (Complete the following.)
2. Datum Requirements

Yes X Project will adhere to the following criteria:

- Horizontal - datum policy is NAD 83, CA-HPGN, EPOCH 1991.35 and English system of units and measures.
- Vertical - datum policy is NAVD 88.
- Units - metric is not required.

No $\qquad$ Provide an explanation on additional page.
3. Will land survey monument perpetuation be scoped into the project, if required?

Yes X
$\qquad$
No $\qquad$ Provide explanation on additional page.

## III. Parcel Information (Land and Improvements)

Are there any property rights required within the proposed project limits?

$$
\text { No ___ Yes } \quad \text { X__ (Complete the following.) }
$$

Part Take Full Take Estimate \$

| A. Number of Vacant Land Parcels |  | \$ |  |
| :---: | :---: | :---: | :---: |
| B. Number of Single Family Residential Units |  | \$ |  |
| C. Number of Multifamily Residential Units |  | \$ |  |
| D. Number of Commercial/Industrial Parcels |  | \$ |  |
| E. Number of Farm/Agricultural Parcels |  | \$ |  |
| F. Permanent Easements | 18 | \$ | 793,300 |
| G. Temporary Easements | 78 | \$ | 1,932,491 |
| Totals | 96 | \$ | 2,725,791 |

Provide a general description of the right of way and excess lands required (zoning, use, improvements, critical, or sensitive parcels, etc.).

In Alternative 4 there are a total of 18 permanent easements and 78 temporary easements needed for the project. The 18 permanent easements consist of approximately 6,760 sf. of highway easement. The temporary easements consist of approximately 186,954 sf. needed from commercial, industrial, single family and multiple residential, and government owned properties. Parcels own by the City of Laguna Beach are not included in this measurement. These temporary easements are expected to be needed for construction purposes. For estimating purposes, it is assumed that the temporary easement will need a width of 10 ' of each parcel's frontage adjacent to proposed sidewalk. It is also assumed that the easements will be needed for a three-year period. The government owned properties needed for construction purposes (excluding the City of Laguna Beach) are proposed to be procured through each government entities' permitting process and not by fee. Costs for these properties include only the services needed to obtain the permits.

## IV. Dedications

Are there any property rights which have been acquired, or anticipate will be acquired, through the "dedication" process for the Project?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Number of dedicated parcels $\quad 0$
Have the dedication parcel(s) been accepted by the municipality involved? N/A

## V. Excess Lands/Relinquishments

Alternative 4

No $\quad \mathrm{X}$ Yes ___ (Provide an explanation on additional page.)

## VI. Relocation Information

Are relocation displacements anticipated?
No $\underline{\mathrm{X}} \quad$ Yes ___ (Complete the following.)
A. Number of Single Family Residential Units

Estimated RAP Payments
$\qquad$
\$ $\qquad$
B. Number of Multifamily Residential Units

Estimated RAP Payments
$\qquad$
\$ $\qquad$
C. Number of Business/Nonprofit

Estimated RAP Payments
$\qquad$
\$ $\qquad$
D. Number of Farms

Estimated RAP Payments
$\qquad$
\$ $\qquad$
E. Other (define in the "Remarks" section)

Estimated RAP Payments
$\qquad$
\$ $\qquad$

Totals $\qquad$ \$ $\qquad$
VII. Utility Relocation Information

Do you anticipate any utility facilities or utility rights of way to be affected?
No $\qquad$ Yes X
$\qquad$ (Complete the following.)

| Facility | Owner | Estimated Relocation Expense (Thousands)* |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | State Obligation | Local Obligation* | Utility Owner Obligation |
| A. Electrical (Transmission) | SOUTHERN CALIFORNIA EDISON | \$0 | \$22,600 | \$ |
| B. Electrical (Distribution) | SOUTHERN <br> CALIFONIA EDISON | \$0 | \$23,700 | \$ |
| C. Gas | SOUTHERN <br> CALIFORNIA GAS | \$0 | \$2,500 | \$ |
| D. Sewer | CITY OF LAGUNA BEACH | \$0 | \$1,750 | \$ |
| E. Water | LaGUNA BEACH COUNTY WATER DIST | \$0 | \$1,750 | \$ |
| F. Fiber Optics / <br> Telephone / Wireless(combined) | CROWN CASTLE- LA <br> \& VEN <br> SPRINT | \$0 | \$3,000 | \$ |

Alternative 4

RIGHT OF WAY DATA SHEET FOR LOCAL PUBLIC AGENCIES (Cont.)
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|  | T-MOBILE USA <br> FRONTIER <br> COX <br> COMMUNICATIONS <br> EXTENET SYSTEMS, <br> INC |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| G. Streetlight <br> conduits | SOUTHERN <br> CALIFONIA EDISON | $\$ 0$ | $\$ 750$ | $\$$ |
| Totals <br> Number of facilities |  | $\$ 0$ | $\$ 56,050$ | $\$$ |
|  | TBD | 7 | TBD |  |
|  |  |  |  |  |

## *NOTE: Share of obligation is unknown at this time. Estimate totals placed in Local Obligation until further investigation.

Any additional information concerning utility involvement on this project?
This project undergrounds overhead utilities within the right-of-way to outside of the travel lanes where feasible.

## SCE Transmission

SCE has approximately 2.5 pole-miles of $66-\mathrm{kV}$ single circuit and double circuit transmission lines. The transmission lines are on wood poles and for the most part located on the southbound side of Laguna Canyon Road with sections also located on the northbound side of the roadway.

## SCE Distribution

SCE also has 2.5 pole-miles of overhead distribution lines placed as underbuild on the same poles as the $66-\mathrm{kV}$ transmission lines although at some locations the distribution lines are on separate poles.

## Telecommunications

It is proposed that all overhead telecommunication lines be undergrounded in conjunction with the electrical lines as part of the project so that all overhead poles can be removed to improve safety. It is likely that the various owners' lines could be located within a joint trench within the new roadway section. Other potential conflicts such as with wireless communication towers will have to be investigated.

## Streetlights

The City will take ownership of the streetlights within the project limits and will install them under a separate project concurrent with the proposed undergrounding.

## SCG Gas

SCG has a gas line that exists along northbound side of the roadway for the length of the project. It is assumed that the existing gas lines will have to be relocated outside of the proposed roadway for the length of the project.

## City of Laguna Beach Sewer

The City of Laguna Beach has a sewer line along northbound side of the roadway for the length of the project. For this stage of the project it is unknown if the sewer line can remain in place. As such it is assumed that the sewer line will be relocated.

## Laguna Beach County Water District

The Laguna Beach County Water District has water lines on both sides of the project. It is assumed that the waterline located on the southbound side of the roadway will not require relocation because there are no apparent conflicts; however, further investigation will be required. For the northbound side of the roadway it uncertain if the water lines can remain in place. As such, it is assumed that the waterline on the northbound side of the roadway will be relocated.
VIII. Rail Information

Are railroad facilities or railroad rights of way affected?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Describe railroad facilities or railroad rights of way affected.

| Owner's Name | Transverse Crossing | Longitudinal Encroachment |
| :--- | :--- | :--- |
| A. |  |  |
| B. |  |  |

Discuss types of agreements and rights required from the railroads. Are grade crossings that require services contracts, or grade separations that require construction and maintenance agreements involved?

## IX. Clearance Information

Are there improvements that require clearance?

$$
\text { No } \underline{X} \quad \text { Yes } \quad \text { (Complete the following.) }
$$

A. Number of Structures to be Demolished Estimated Cost of Demolition $\qquad$

## X. Hazardous Materials/Waste

Are there any site(s) and/or improvements(s) in the Project Limits that are known to contain
hazardous materials? None $\quad \mathrm{X} \quad Y e s \quad$ (Explain in the "Remarks" section.)
Are there any site(s) and/or improvement(s) in the Project Limits that are suspected to contain
hazardous waste? None $\qquad$ Yes $\quad \mathrm{X}$ (Explain in the "Remarks" section.)
XI. Project Scheduling

|  | Proposed lead time | Completion date |
| :---: | :---: | :---: |
| * Preliminary Engineering, Surveys | 24 (months) | July 2023 |
| * R/W Engineering Submittals | 16 (months) | January 2024 |
| * R/W Appraisals/Acquisition | 16 (months) | January 2024 |
| Proposed Environmental Clearance |  | January 2025 |
| Proposed R/W Certification |  | April 2027 |

## XII. Proposed Funding

NOTE: Potential funding sources to be determined.

|  | Local | State |  | Federal |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Other* |  |  |  |  |  |  |
| Acquisition |  |  |  |  |  |  |
| Utilities |  |  |  |  |  |  |
| Relocation Assistance Program |  |  |  |  |  |  |
| R/W Support |  |  |  |  |  |  |
| Other Costs (Envir. Review, |  |  |  |  |  |  |
| Demo, etc.) |  |  |  |  |  |  |

*Proposed funding to be determined. Purpose of PSR is to obtain funding and potential funding sources.
**R/W Support costs include costs for engineering, appraisals, etc. ROW cost estimate is assumed to be probable to optimistic.

## XIII. Remarks

The ISA Checklist for hazardous waste was completed in June 2018 and is included as Attachment J in the PSR/PDS. Potential hazardous waste/materials issues associated with the proposed Project include aeriallydeposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and pad mounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles. A full ISA for all right-of-way acquisition properties and Preliminary Site Investigations (PSI) will be conducted during PA/ED phase.

Project Sponsor Consultant HDR Engineering, Inc.
Prepared by:


Stephen P.A. Crouch, PE; Project Engineer, HDR Engineering, Inc.


Jill Craig, ROW Agent, HDR Engineering, Inc.
Date 6/17/2022

Project Sponsor
City of Laguna Beach
Reviewed and Approved by:


Thomas Perez; Capital Program Manager;
City of Lagena Beach Pubic Works

6/17/2022
Date

Caltrans
Reviewed and accent based on information provided to date:


Linda Lundblad, Branch Chief
08/09/2022
Right of Way - Appraisals, Condemnation \& Local Programs

To: Jennifer Pham
Office Chief
Office of Right of Way and Right of Way Engineering

Attention: Linda Lundblad
District Branch Chief
R/W Local Programs

Date: 6-17-2022

Co. ORA Rte. 133

Expense Authorization 0Q670K
Project ID \#1217000086

## Subject: RIGHT OF WAY DATA SHEET - LOCAL PUBLIC AGENCIES

Project Description: Improve SR-133 (Laguna Canyon Road) between Canyon Acres Drive \& El Toro Road - Alternative 5

Right of way necessary for the subject project will be the responsibility of $\qquad$ City of Laguna Beach .

The information in this data sheet was developed by $\qquad$ HDR Engineering, Inc. $\qquad$ .

## I. Right of Way Engineering

Will Right of Way Engineering be required for this project?

- No
- Yes X
- Hard copy (base map)
- Appraisal map
- Acquisition Documents
- Property Transfer Documents
- R/W Record Map
- Record of Survey

| X |
| :--- |
| X |
| X |
| X |
| X |
| X |

## II. Engineering Surveys

1. Is any surveying or photogrammetric mapping required?

No _ Yes $\xrightarrow{\mathrm{X}}$ (Complete the following.)
2. Datum Requirements

Yes X Project will adhere to the following criteria:

- Horizontal - datum policy is NAD 83, CA-HPGN, EPOCH 1991.35 and English system of units and measures.
- Vertical - datum policy is NAVD 88.
- Units - metric is not required.

No $\qquad$ Provide an explanation on additional page.
3. Will land survey monument perpetuation be scoped into the project, if required?

Yes X
No $\qquad$ Provide explanation on additional page.

## III. Parcel Information (Land and Improvements)

Are there any property rights required within the proposed project limits?

$$
\text { No ___ Yes } \quad \text { X__ (Complete the following.) }
$$

Part Take Full Take Estimate \$

| A. Number of Vacant Land Parcels |  | N/A | \$ |  |
| :---: | :---: | :---: | :---: | :---: |
| B. Number of Single Family Residential Units |  | N/A | \$ |  |
| C. Number of Multifamily Residential Units |  | N/A | \$ |  |
| D. Number of Commercial/Industrial Parcels |  | N/A | \$ |  |
| E. Number of Farm/Agricultural Parcels |  | N/A | \$ |  |
| F. Permanent Easements | 29 | N/A | \$ | 2,488,019 |
| G. Temporary Easements/ Other Parcels | 86 | N/A | \$ | 2,013,158 |
| Totals | 115 | N/A | \$ | 4,501,177 |

Provide a general description of the right of way and excess lands required (zoning, use, improvements, critical, or sensitive parcels, etc.).

In Alternative 5 there are a total of 29 permanent easements and 86 temporary easements needed for the project. The 29 permanent easements consist of approximately $19,672 \mathrm{sf}$. of highway easement. The temporary easements consist of approximately 192,688 sf. needed from commercial, industrial, single family and multiple residential, and government owned properties. Parcels own by the City of Laguna Beach are not included in this measurement. These temporary easements are expected to be needed for construction purposes. For estimating purposes, it is assumed that the temporary easement will need a width of 10 ' of each parcel's frontage adjacent to proposed sidewalk. It is also assumed that the easements will be needed for a three-year period. The government owned properties needed for construction purposes (excluding the City of Laguna Beach) are proposed to be procured through each government entities' permitting process and not by fee. Costs for these properties include only the services needed to obtain the permits.

## IV. Dedications

Are there any property rights which have been acquired, or anticipate will be acquired, through the "dedication" process for the Project?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Complete the following.) }
$$

Number of dedicated parcels $\underline{0}$
Have the dedication parcel(s) been accepted by the municipality involved? N/A

## V. Excess Lands/Relinquishments

Are there Caltrans property rights which may become excess lands or potential relinquishment areas?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes } \quad \text { (Provide an explanation on additional page.) }
$$

VI. Relocation Information

Are relocation displacements anticipated?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

A. Number of Single Family Residential Units $\qquad$ \$ $\qquad$
Estimated RAP Payments
B. Number of Multifamily Residential Units $\qquad$ \$ $\qquad$
Estimated RAP Payments
C. Number of Business/Nonprofit $\qquad$ \$ $\qquad$
Estimated RAP Payments
D. Number of Farms $\qquad$ \$ $\qquad$
Estimated RAP Payments
E. Other (define in the "Remarks" section) $\qquad$ \$ $\qquad$ Estimated RAP Payments

Totals $\qquad$
$\qquad$

## VII. Utility Relocation Information

Do you anticipate any utility facilities or utility rights of way to be affected?
No $\qquad$ Yes $\qquad$ (Complete the following.)

|  |  |  | Estimated Relocation Expense (Thousands)* |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: |
| Facility | State <br> Obligation | Local <br> Obligation* | Utility Owner <br> Obligation |  |  |
| A. Electrical <br> (Transmission) | SOUTHERN <br> CALIFORNIA <br> EDISON | $\$ 0$ | $\$ 22,600$ | $\$$ |  |
| B. Electrical <br> (Distribution) | SOUTHERN <br> CALIFONIA EDISON | $\$ 0$ | $\$ 23,700$ | $\$$ |  |
| C. Gas | SOUTHERN <br> CALIFORNIA GAS | $\$ 0$ | $\$ 2,500$ | $\$$ |  |
| D. Sewer | CITY OF LAGUNA <br> BEACH | $\$ 0$ | $\$ 1,750$ | $\$$ |  |
| E. Water | LAGUNA BEACH <br> COUNTY WATER <br> DIST | $\$ 0$ | $\$ 1,750$ | $\$$ |  |

RIGHT OF WAY DATA SHEET FOR LOCAL PUBLIC AGENCIES (Cont.)
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| F. Fiber Optics / <br> Telephone / <br> Wireless (combined) | CROWN CASTLE- LA <br> \& VEN <br> SPRINT <br> T-MOBILE USA <br> FRONTIER <br> cox <br> COMMUNICATIONS <br> EXTENET SYSTEMS, <br> INC | \$0 | \$3,000 | \$ |
| :---: | :---: | :---: | :---: | :---: |
| G. Streetlight conduits | SOUTHERN CALIFONIA EDISON | \$0 | \$750 | \$ |
| Totals |  | \$0 | \$56,050 | \$ |
| Number of facilities |  | TBD | 7 | TBD |

## *NOTE: Share of obligation is unknown at this time. Estimate totals placed in Local Obligation until further investigation.

Any additional information concerning utility involvement on this project?
This project undergrounds overhead utilities within the right-of-way to outside of the travel lanes where feasible.

## SCE Transmission

SCE has approximately 2.5 pole-miles of $66-\mathrm{kV}$ single circuit and double circuit transmission lines. The transmission lines are on wood poles and for the most part located on the southbound side of Laguna Canyon Road with sections also located on the northbound side of the roadway.

## SCE Distribution

SCE also has 2.5 pole-miles of overhead distribution lines placed as underbuild on the same poles as the $66-\mathrm{kV}$ transmission lines although at some locations the distribution lines are on separate poles.

## Telecommunications

It is proposed that all overhead telecommunication lines be undergrounded in conjunction with the electrical lines as part of the project so that all overhead poles can be removed to improve safety. It is likely that the various owners' lines could be located within a joint trench within the new roadway section. Other potential conflicts such as with wireless communication towers will have to be investigated.

## Streetlights

The City will take ownership of the streetlights within the project limits and will install them under a separate project concurrent with the proposed undergrounding.

## SCG Gas

SCG has a gas line that exists along northbound side of the roadway for the length of the project. It is assumed that the existing gas lines will have to be relocated outside of the proposed roadway for the length of the project.

## City of Laguna Beach Sewer

The City of Laguna Beach has a sewer line along northbound side of the roadway for the length of the project. For this stage of the project it is unknown if the sewer line can remain in place. As such it is assumed that the sewer line will be relocated.

## Laguna Beach County Water District

The Laguna Beach County Water District has water lines on both sides of the project. It is assumed that the waterline located on the southbound side of the roadway will not require relocation because there are no apparent conflicts; however, further investigation will be required. For the northbound side of the roadway it uncertain if
the water lines can remain in place. As such, it is assumed that the waterline on the northbound side of the roadway will be relocated.

## VIII. Rail Information

Are railroad facilities or railroad rights of way affected?

$$
\text { No } \underline{X} \quad \text { Yes ___ (Complete the following.) }
$$

Describe railroad facilities or railroad rights of way affected.

| Owner's Name | Transverse Crossing | Longitudinal Encroachment |
| :--- | :--- | :--- |
| A. |  |  |
| B. |  |  |

Discuss types of agreements and rights required from the railroads. Are grade crossings that require services contracts, or grade separations that require construction and maintenance agreements involved?

## IX. Clearance Information

Are there improvements that require clearance?

$$
\text { No } \quad \mathrm{X} \quad \text { Yes ___ (Complete the following.) }
$$

A. Number of Structures to be Demolished Estimated Cost of Demolition \$ $\qquad$

## X. Hazardous Materials/Waste

Are there any site(s) and/or improvements(s) in the Project Limits that are known to contain


Are there any site(s) and/or improvement(s) in the Project Limits that are suspected to contain
hazardous waste? None $\qquad$ Yes_X (Explain in the "Remarks" section.)

## XI. Project Scheduling

|  | Proposed lead time | Completion date |
| :---: | :---: | :---: |
| * Preliminary Engineering, Surveys | 24 (months) | July 2023 |
| * R/W Engineering Submittals | 16 (months) | January 2024 |
| * R/W Appraisals/Acquisition | 16 (months) | January 2024 |
| Proposed Environmental Clearance |  | January 2025 |
| Proposed R/W Certification |  | April 2027 |

## XII. Proposed Funding

NOTE: Potential funding sources to be determined.

RIGHT OF WAY DATA SHEET FOR LOCAL PUBLIC AGENCIES (Cont.)
(Form \#)

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Local State Federal Other*

*Proposed funding to be determined. Purpose of PSR is to obtain funding and potential funding sources.
**R/W Support costs include costs for engineering, appraisals, etc. ROW cost estimate is assumed to be probable to optimistic.

## XIII. Remarks

The ISA Checklist for hazardous waste was completed in June 2018 and is included as Attachment J in the PSR/PDS. Potential hazardous waste/materials issues associated with the proposed Project include aeriallydeposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and padmounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles. A full ISA for all right-of-way acquisition properties and Preliminary Site Investigations (PSI) will be conducted during PA/ED phase.

Project Sponsor Consultant HDR Engineering, Inc. Prepared by:

Project Sponsor
City of Laguna Beach
Reviewed and Approved by:


Stephen P.A. Crouch, PE; Project Engineer, HDR Engineering, Inc.


Jill Craig, ROW Agent, HDR Engineering, Inc.


Thomas Perez; Capital Program Manager; City of Laguna Beach Public Works

6/17/2022
Date

Caltrans
Reviewed and accept based on information provided to date:


Linda Lundblad, Branch Chief
Right of Way - Appraisals, Condemnation \& Local Programs

08/09/2022
Date

## ATTACHMENT I

## PRELIMINARY ENVIRONMENTAL ANALYSIS REPORT (PEAR)

(With Attachments)

## PRELIMINARY ENVIRONMENTAL ANALYSIS REPORT

## 1. Project Information

| DIST-CO-RTE: 12-OR-133 | PM/PM: 0.96/3.41 |
| :--- | :--- |
| EA: 0Q670K | EFIS Project ID: |
| Project Title: State Route 133 (SR-133) <br> Project | Laguna Canyon Road (LCR) Improvement |
| Project Manager: Lorica Subida | Phone: |
| Project Engineer: Raouf Fam | Phone: (657) 328-6269 |
| Environmental Office Chief/Manager: Smita Deshpande | Phone: (657) 328-6151 |
| PEAR Preparer: Angie Kung, HDR | Phone: (949) 241-6192 |

## 2. Project Description

## Purpose and Need

## Project Purpose

The purpose of the Project is to:

- Improve vehicular safety along the existing corridor;
- Improve pedestrian and bicycle mobility and safety; and
- Encourage the use of active transportation along the corridor.


## Project Need

- Overhead Southern California Edison (SCE) transmission and distribution lines currently exist along both sides of the State Route 133 (SR-133) corridor within the Clear Recovery Zone (CRZ) and in close proximity to the edge of travel way. Coupled with high traffic demand, vehicle queuing during both peak and non-peak periods, the lack of traffic breaks or protected left-turn movements, and inadequate shoulders, there is a high concentration of accidents that occur at various locations within the Project limits.
- The corridor currently lacks adequate shoulders and pedestrian and bicycle facilities within the Project limits. Dedicated pedestrian and bicycle paths, sidewalks with Americans with Disabilities Act (ADA) access, and improved shoulders along the corridor would improve access, connectivity, and safety for pedestrians and bicyclists.
- Due to special events and the proximity to the Pacific Ocean as well as multiple adjacent recreational facilities and trails within the Project limits, traffic demand within this corridor already exceeds capacity during weekday AM and PM peak hours and during most summer weekends and holidays. Without the provision for alternative transportation modes such as public transit, walking, and biking to improve connectivity and access to adjacent residential and commercial land uses,
recreational trails, and parks within the City of Laguna Beach (City) this multimodal corridor will continue to degrade.


## Description of work

The City, in cooperation with the California Department of Transportation (Caltrans), is proposing to improve a 2.5 -mile corridor of the SR-133 in the City of Laguna Beach, California. The regional location of the proposed Project (Figure 1. Regional Location) is provided in Attachment A of this Preliminary Environmental Analysis Report (PEAR). The Project limits on SR-133, also known as Laguna Canyon Road (LCR), extend from Canyon Acres Drive (PM 0.96) to El Toro Road (PM 3.41) in Orange County (Project).

LCR is one of three gateways to Laguna Beach and provides critical access to adjacent recreational spaces as well as activities in the City. As such, ensuring that LCR provides efficient, safe access to the area is vital both to the region and to the City itself. LCR within the Project limits consists of a two-lane conventional highway with a center turn lane, limited shoulders, and sporadic off-street angled and parallel parking located along the northbound (NB) side of the roadway. The right-of-way (ROW) is constrained by residential and light commercial land uses, as well as various trails, park uses, institutional uses, and open space preservation areas. This portion of LCR is further constrained by Southern California Edison's (SCE) overhead transmission and distribution line poles in close proximity to the travel way within the CRZ that pose potential safety concerns.

The proposed improvements to LCR within the Project limits generally consist of a Class I and Class II bicycle lane(s), pedestrian pathways/sidewalks, improved access to transit facilities, improved shoulders and undergrounding of the SCE transmission and distribution lines outside the travel way.

## Alternatives

## Alternative 1 - No-Build Alternative

The No-Build Alternative would maintain LCR in its current condition. No improvements would be implemented at this time; therefore, no capital costs are associated with this alternative. Utility poles on both the northbound and southbound sides of the road would not be undergrounded to allow full use of the State ROW for complete street elements to be incorporated into the corridor that encourage increased use of active modes of transportation. As the traffic demand increases, traffic operational characteristics will further deteriorate which may result in an increase in congestion, vehicle queuing, vehicle delay, and safety issues. This alternative would not satisfy the purpose and need of the Project.


#### Abstract

Alternative 2 Alternative 2 generally consists of a typical width of 64 feet ( ft ) including the vehicle, pedestrian and bicycle facilities. This alternative includes narrowed 11-ft. travel lanes for majority of the Project limits that would be widened to $12-\mathrm{ft}$. from approximately Phillips Street to El Toro Road, a 10-ft. center dual turn lane, 7 - ft . shoulders, and a pedestrian path on the NB side. Alternative 2 also includes a Class I separated bikeway on the southbound side of the roadway. During emergencies there is space for four outbound evacuation travel lanes on the roadway and one inbound emergency vehicle lane.


## Alternative 3

Alternative 3 generally consists of a typical width of 64 ft . including the vehicle, pedestrian and bicycle facilities. This alternative includes narrowed 11-ft. travel lanes for majority of the Project limits that would be widened to 12-ft. from approximately Phillips Street to El Toro Road, a 10-ft. center turn lane, and 7 -ft. shoulders and a pedestrian path on the NB side of the roadway. Alternative 3 also includes a Class I separated bikeway with adjacent pedestrian path on the southbound (SB) side and a Class II bike lane on the NB side of the roadway. During emergencies there is space for three outbound evacuation travel lanes and one inbound emergency vehicle lane. Additionally, the bikeway and pedestrian path on the SB side of the roadway will have a mountable curb, which could be used as an emergency vehicle lane.

## Alternative 4

Alternative 4 generally consists of a typical width of 64-ft. including the vehicle, pedestrian and bicycle facilities. This alternative includes 12-foot travel lanes, and a 10-foot center dual left-turn lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 7 -foot Class II buffered bike lane on both sides of the roadway. During emergencies, there is space for four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes.

## Alternative 5

Alternative 5 introduces a reversible lane that would provide a peak-direction capacity to a two-way road and decrease congestion by borrowing available lane capacity from the other (off-peak) direction. This alternative generally consists of a typical width of 64 - ft. including the vehicle, pedestrian, and bicycle facilities. It would include 12 -foot travel lanes and a 12- to 14- foot center reversible lane, pedestrian paths/sidewalks on both the NB and SB sides of the roadway, and a 5 -foot Class II buffered bike lane on both sides of the roadway. During emergencies, there is space for four outbound evacuation travel lanes and one inbound emergency vehicle lane by utilizing the bike lanes.

## Summary of Alternatives

The primary difference between the Build Alternatives (Alternatives 2 through 5) consist of the width of the travel lanes and the type of proposed bicycle and pedestrian facilities. Alternatives 2 and 3 would propose primarily $11-\mathrm{ft}$. travel lanes, while Alternative 4 would propose a mix of $11-\mathrm{ft}$. and $12-\mathrm{ft}$. travel lanes. Alternative 5 , with its reversible lane, would also propose a mix of 11-ft. and 12-ft. travel lanes.

All of the Build Alternatives would include a pedestrian path along the NB side of LCR. However, Alternatives 2 and 3 would propose a Class I separated bikeway on the SB of LCR and Alternative 3 would also include a Class II bike lane on the NB side of LCR. Alternatives 4 and 5 would construct an additional pedestrian path on the SB side of LCR and a Class II bicycle lane on both sides of LCR. These differences would result in the same impacts to adjacent parcels for Alternatives 2 to 4 but would vary in the amount of acreage needed for each partial acquisition or temporary construction easement (TCE). Alternative 5 would result in additional impacts to adjacent parcels because slither partial acquisitions would be required.

## 3. Anticipated Environmental Approval

## CEQA (choose one):

$\square$ Exemption
$\square$ Statutory $\quad \square$ Categorical $\square$ Common Sense
$\boxtimes$ Initial Study or Focused Initial Study with proposed Negative Declaration (ND) or Mitigated ND
$\square$ Environmental Impact Report

## NEPA (choose one):

Categorical Exclusion
$\boxtimes$ Environmental Assessment with Finding of No Significant Impact
$\boxtimes$ Routine $\quad \square$ Complex
$\square$ Environmental Impact Statement
CEQA Lead Agency (if determined): Caltrans District 12
Estimated length of time (months) to obtain environmental approval: 18 to 24
Estimated person hours to complete identified tasks: TBD

## 4. Special Environmental Considerations

Based on the preliminary assessment of the four Build Alternatives (Alternatives 2 through 5) proposed, a number of environmental impacts have been identified which require special considerations. These following issues are discussed below.

## Community Impacts

Build Alternatives 2 through 5 would require two permanent partial acquisitions from City and privately-owned parcels for turn pocket, a local roadway intersection and private driveway reconstruction. In addition, Alternative 5 would also require 27 additional permanent partial acquisitions. These ROW requirements are not anticipated to affect access to the property. Highway Easements and TCEs would also be required during construction throughout the proposed Project limits. It is not anticipated that the highway easements or TCEs will result in impacts to access during construction. Permanent and temporary impacts to City-permitted on-street parking may occur along LCR within the Project limits. A Traffic Study will identify parking and driveway impacts under each Build Alternative (Alternatives 2 through 5).

The undergrounding of existing overhead SCE utilities and various traffic and safety improvements proposed under the Build Alternatives (Alternatives 2 through 5) would result in an overall permanent net benefit to the communities adjacent to the Project limits. Impacts to the community during construction of the proposed Project would occur, however, a transportation management plan (TMP) would be implemented to avoid and minimize temporary impacts related to access and circulation. Early and ongoing public outreach efforts will be undertaken to educate and inform the public and stakeholders.

Under the Build Alternatives (Alternatives 2 through 5), the proposed Project would require a TCE and work within the Laguna Coast Wilderness Park, Laguna Beach Dog Park, and Laguna Beach Batting Cages. In addition, Alternative 5 would also require partial acquisition of the Laguna Beach Batting Cages. Orange County Parks is the owner with jurisdiction (OWJ) of the Laguna Coast Wilderness Park, and the City is the OWJ of the Laguna Beach Dog Park and the Laguna Beach Batting Cages. Any impacts to these properties would need to be evaluated under Section 4(f) and would require compliance with Section 4(f) of the Department of Transportation Act.

## Biological Resources

The biological study area (BSA) for the proposed Project includes the Project limits plus a 50-ft. buffer for assessing direct impacts.

Available literature resources, including the California Department of Fish and Wildlife's California Natural Diversity Database RareFind 5 program (Online CDFW 2018), California Native Plant Society's (CNPS) Inventory of Rare and Endangered Plants of California (Online Edition, v. 8.2; CNPS 2018), Consortium of California Herbaria (Jepson Flora Project 2018), and USFWS online Information for Planning and Consultation Environmental Conservation Online System were reviewed to identify special-status plant and wildlife species and designated Critical Habitat with the potential to occur in the vicinity of the Project limits. Searches of the California Natural Diversity Database and

CNPS databases were conducted for the six U.S. Geological Survey 7.5' quadrangles surrounding the Project, which include Newport Beach, Tustin, El Toro, Laguna Beach, San Juan Capistrano, and Dana Point, California.

Additional resources used to characterize existing site conditions included: U.S. Geologic Survey topographic maps at a minimum 1:24,000 scale, USFWS National Wetland Inventory dataset, Natural Resource Conservation Service Soil Mapping, aerial imagery available on Google Earth, and a field visit to conduct vegetation mapping and a habitat assessment for special-status species with potential to occur in the vicinity of the proposed Project. The consultant biologist also identified all aquatic features with the potential to be regulated by the US Army Corps of Engineers and RWQCB pursuant to Sections 401 and 404 of the Clean Water Act, respectively, and by CDFW pursuant to Section 1600 of California Fish and Game Code. This assessment did not include a delineation of jurisdictional boundaries or wetland determination. Vegetation units were defined based on methodology defined in the online Manual of California Vegetation (CNPS 2018).

The proposed Project activities are covered by the County of Orange Central/Coastal Natural Communities Conservation Plan/Habitat Conservation Plan (NCCP/HCP) that was adopted on July 17, 1996, and for which an Implementing Agreement was executed between the federal and state wildlife agencies (US Fish and Wildlife Service [USFWS] and California Department of Fish and Wildlife [CDFW]) and participating entities, including the City. The measures incorporated in the NCCP/HCP satisfy the federal, state, and local project-specific mitigation requirements for the species and habitats addressed in the NCCP/HCP under the Federal Endangered Species Act, California Endangered Species Act, CEQA, NEPA, and the Migratory Bird Treaty Act. Impacts to coastal California gnatcatcher (Polioptila californica californica, CAGN) are covered by the NCCP/HCP and impacts to Least Bell's Vireo (Vireo bellii pusillus, LBVI) and Southwestern Willow Flycatcher (Empidonax traillii extimus, SWFL) are conditionally covered by the NCCP/HCP. Therefore, Section 7 Consultation with USFWS is not required as long as the project complies with the NCCP/HCP.

Pursuant to the Implementing Agreement, the following protocol presence/absence surveys may be required:

- Least Bell's Vireo
- Southwestern Willow Flycatcher

If these species are found within the BSA during presence/absence surveys, a biological monitor would be required during Project construction. Other special-status species, including burrowing owl (Athene cunicularia), American badger (Taxidea taxus), and
nesting migratory birds, are expected to require avoidance, minimization or compensatory mitigation due to the potential for direct impacts. Therefore, the following focused species habitat assessments or surveys may be required:

- Burrowing Owl breeding season surveys and pre-construction surveys
- American badger pre-construction surveys
- Avoiding impacts to migratory bird breeding habitat during the breeding season, typically defined as February 15 through August 31.
- If removal of nesting habitat is necessary during the breeding season, preconstruction nesting bird surveys would be required. If nesting birds are detected, appropriate no-construction buffers would be required to prevent take of the nest.

A jurisdictional delineation (JD) is required and will be conducted to support regulatory permitting, if needed. Build Alternatives (Alternatives 2 through 5) may directly impact aquatic features that would require coordination and permits from other agencies, which would result in an extended environmental process. The expected review/permits associated with improvements to aquatic features are as follows:

- California Department of Fish and Wildlife 1602 Streambed Alternation Agreement
- Regional Water Quality Control Board (RWQCB) Section 401 Water Quality Certification
- US Army Corps of Engineers Section 404 Nationwide Permit (unless more than 300 linear ft . of streambed is impacted)


## Coastal Zone

The proposed Project is located within the Coastal Zone. A Coastal Development Permit (CDP) issued by the City will be required prior to the start of construction.

## Cultural Resources

The proposed Project under the Build Alternatives (Alternatives 2 through 5) has the potential to impact significant cultural and historic resources. The Native American Heritage Commission (NAHC) indicated that the area is sensitive for cultural resources as did several Native American groups. 12 prehistoric and six historic cultural resources are recorded within 0.25 miles of the proposed Project limits. A cultural monitor will be required during construction.

## Paleontological Resources

The proposed Project area is underlain by multiple geologic units and contain areas of high potential/sensitivity for paleontological resources throughout the Project limits. Build Alternatives (Alternatives 2 through 5) have the potential to impact the young axialchannel deposits, Topanga Group, and Vaqueros Formation all of which have high
potential of containing paleontological resources. A paleontological monitor will be required during construction.

## Section 4(f) Resources

Laguna Coast Wilderness Park, Laguna Beach Dog Park, and Laguna Beach Batting Cages are identified as eligible Section 4(f) resources within the Project limits. Temporary occupancy of all three Section 4 (f) facilities would occur during construction under all Build Alternatives (Alternatives 2 through 5) as a result of TCEs. In addition, Alternative 5 would also require partial acquisition of the Laguna Beach Batting Cages. Coordination with OWJs over Section 4(f) resources will be conducted, and any findings and recommendations will be included in the Section 4(f) Evaluation.

## 5. Anticipated Environmental Commitments

Project specific avoidance, mitigation, and/or minimization measures as well as the associated costs were not determined at this time because technical studies recommended in this Preliminary Environmental Analysis Report (PEAR) for the proposed Project have not been initiated. Anticipated environmental commitments for the proposed Project have been identified below. Additional environmental concerns and required environmental commitments may be identified during the Project Approval/Environmental Document (PA/ED) phase.

### 5.1 Community Impacts

### 5.1.1 Community Impacts

The proposed Project under the Build Alternatives (Alternatives 2 through 5) would result in impacts to the surrounding community as discussed below. Therefore, a Community Impact Assessment (CIA) is recommended during the PA/ED phase to identify additional impacts related to land use and community resources as a result of the proposed Project.

During and throughout construction, the TMP will address short-term impacts related to traffic and circulation during construction, including access to existing ADA-compliant cross walks, sidewalks, bus stops as well as existing handicapped/ADA parking spaces and parking spaces on public and private (including commercial) property within the Project limits.

### 5.1.2 Traffic and Transportation

The undergrounding of existing overhead utilities and various traffic and safety improvements proposed under the Build Alternatives (Alternatives 2 through 5) would result in an overall permanent net benefit to the communities adjacent to the Project limits. However, impacts to the community during construction of the proposed Project would occur. During the PA/ED phase, a Traffic Operations Analysis Report (TOAR) would be prepared to identify temporary impacts and construction staging requirements.

### 5.1.3 Utilities

Any disruptions to utility service under the Build Alternatives (Alternatives 2 through 5) would be scheduled and coordinated to ensure they would not adversely affect the surrounding community during construction of the proposed Project. As a result of the proposed Project, overhead transmission and distribution line poles on both the NB and SB directions of the LCR will be removed as the utility power lines will be underground as a result of the Project. Some of these distribution line poles include pole-mounted transformers. A utility substation is located on the southwest end of the Project, approximately 0.2 miles north of Laguna Bowl Road. Water and telecommunication (Verizon) lines are located to the east of the Project and would not be affected. These new underground utilities will connect to the SCE Morro Substation and require new tieins and minor work at the SCE Morro Substation.

### 5.1.4 Emergency Services and Transportation Management Plan

Coordination with emergency service providers and communication with the surrounding community, as part of the TMP, would minimize any adverse impacts to the adjacent community under the Build Alternatives (Alternatives 2 through 5). A TMP would be developed for implementation during construction activities to avoid and minimize temporary impacts related to access and circulation. The TMP would include, but not be limited to, information regarding any temporary lane closures, detours, signage, and a coordination plan with the local community and emergency service providers during construction activities.

### 5.1.5 Real Property Acquisitions

### 5.1.5.1 Partial Acquisitions

Partial acquisitions would be required of two parcels under all Build Alternatives (Alternatives 2 through 5). These parcels requiring partial acquisitions are identified as APNs 495-021-30 (City Corporation Yard) and 495-021-09 (Laguna College of Art and Design). Alternatives 2, 3, and 5 would also require a partial acquisition of these two parcels; whereas, Alternative 4 would only require a permanent easement. Alternative 4 would require 16 additional permanent partial acquisitions and Alternative 5 would require 27 additional permanent partial acquisitions, as identified in Table 1. Right-of-Way Impacts -Partial Acquisitions.

The proposed Project, under the Build Alternatives (Alternatives 2 through 5), is not anticipated to require full parcel acquisitions or relocation of properties. Full functional use of the property would remain and its structures would remain intact. Compensation to property owners due to property acquisition would be required in accordance with Caltrans and Federal Highway Administration (FHWA) policies and the Uniform Relocation Assistance and Real Property Acquisition Policies Act of 1970.

### 5.1.5.2 Temporary Construction Easements

The proposed Project under the Build Alternatives (Alternatives 2 through 5) is anticipated to require TCEs. The TCEs are comprised of private residential and business parcels,

County parcels, and City parcels necessary to accommodate driveway relocations, construction of a new intersection, turn pockets, and other proposed Project improvements. Full functional use of the properties would remain and all associated structures would remain intact.

### 5.1.5.3 Staging Areas

Two potential staging areas have been identified within the Project limits (see Figure 2. Project Limits in Attachment A of this document), Staging Area 1 located at the City of Laguna Beach Maintenance Facility Parking Lot 16 and Staging Area 2 located on a City lot, adjacent to Friendship Shelter.

Table 1. Right-of-Way Impacts - Partial Acquisitions

| Location | APN | Owner | Right-of-Way Requirements (Sq. Ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Alternative $2$ | $\begin{gathered} \text { Alternative } \\ 3 \end{gathered}$ | $\begin{gathered} \text { Alternative } \\ 4 \\ \hline \end{gathered}$ | Alternative 5 |
| City Maintenance Yard | 495-021-30 | City of Laguna Beach | 4,246 | 6,361 | 4,520* | 10,119 |
| Laguna College of Art \& Design | 495-021-09 | Laguna College of Art \& Design | 854 | 399 | 1,438* | 1,455 |
|  | 496-061-20 | City Of Laguna Beach | - | - | - | 62 |
|  | 496-061-38 | County of Orange | - | - | - | 3,721 |
| 21080 Laguna Canyon Rd | 632-071-16 | Oeath Gavin | - | - | 80 | 406 |
| 21094 Laguna Canyon Rd | 632-071-19 | 3501 W Segerstrom | - | - | 76 | 388 |
| 3015 Laguna Canyon Rd | 632-071-20 | 3501 W Segerstrom LLC | - | - | 74 | 377 |
| 2999 Laguna Canyon Rd | 632-071-21 | Patrick \& Glenda Curran | - | - | 54 | 275 |
| 2955 Laguna Canyon Rd | 632-071-23 | Sagebrush Properties LLC | - | - | 116 | 596 |
|  | 632-071-25 | City of Laguna Beach | - | - | 85 | 437 |
|  | 632-081-10 | City of Laguna Beach | - | - | 309 | 1,554 |
| 2515 Laguna Canyon Rd | 632-091-09 | Dennis Upchurch \& Rc Upchurch Investment Trust | - | - | - | 94 |
| 2515 Laguna Canyon Rd | 632-091-10 | Dennis Upchurch \& Rc Upchurch Investment Trust | - | - | - | 61 |
| 2621 Laguna Canyon Rd | 632-091-18 | Dirk \& Katherin Maes | - | - | - | 148 |
| 21000 Laguna Canyon Rd | 632-091-19 | Laguna College of Art \& Design | - | - | - | 261 |
| 2655 Laguna Canyon Rd | 632-091-20 | Ronald Ellis | - | - | 82 | 608 |
| 2675 Laguna Canyon Rd | 632-091-21 | Kids Love LLC | - | - | 198 | 710 |
| 2715 Laguna Canyon Rd | 632-091-24 | Gordy \& Nelly Buslach | - | - | 40 | 340 |

Table 1. Right-of-Way Impacts - Partial Acquisitions

| Location | APN | Owner | Right-of-Way Requirements (Sq. Ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Alternative 2 | Alternative 3 | Alternative $4$ | Alternative 5 |
| 2735 Laguna Canyon Rd | 632-091-25 | Caroline Brooks \& The Caroline Maxine Separate | - | - | 52 | 352 |
| 2795 Laguna Canyon Rd | 632-091-29 | Arden Smith Jr \& Antonio Oliveira | - | - | - | 212 |
| 2711 Laguna Canyon Rd | 632-091-31 | Starts LLC | - | - | 116 | 54,418 |
| 2695 Laguna Canyon Rd | 632-091-32 | Andrew \& Stephanie Chapel | - | - | 177 | 612 |
| 2605 Laguna Canyon Rd | 632-091-34 | Funke-Kaiser Kurt <br> Trust \& Funke-Kaiser Family Trust | - | - | - | 30 |
| 2761 Laguna Canyon Rd | 632-091-35 | Valbeach Garfield LLC | - | - | 84 | 390 |
| 2775 Laguna Canyon Rd | 632-091-36 | Ajmer \& Sunita Singh | - | - | 37 | 333 |
| 2745 Laguna Canyon Rd | 632-091-38 | Mark \& Susan Bolick |  |  | 68 |  |
| 2075 Laguna Canyon Rd | 632-111-05 | Dolores Warner \& The Emanuel Weiner Election Trust | - | - | - | 12.95 |
| 2055 Broadway | 632-111-06 | Laguna Canyon Road Commercial LLC | - | - | - | 68 |
| 2003 Laguna Canyon Rd | 632-111-07 | School Laguna <br> Beach Unified District | - | - | - | 423 |
| 1975 Laguna Canyon Rd | 632-111-10 | Anthony \& Irma Shaffer | - | - | - | 83 |
| Total |  |  | 5,100 | 6,760 | 1,648 | 78,546 |

*Permanent easement only.
APN=Assessor's Parcel Number

### 5.1.6 Visual Resources

Visual impacts are discussed in Section 8.5. A Visual Impact Assessment (VIA) Technical Memorandum will be prepared during the PA/ED phase.

### 5.1.7 Coastal Zone

The proposed Project is located within the Coastal Zone and would need to comply and address The Coastal Act goals and policies as they relate to aesthetics, safety, water quality, landscape plans and preservation, endangered species, cultural resources, Environmentally Sensitive Habitat Areas (ESHA), and public access. The proposed Project will also require a coastal development permit (CDP) issued by the City prior to the start of construction.

### 5.1.8 Section 4(f) Resources

Laguna Coast Wilderness Park is identified as an eligible Section 4(f) resource within the Project limits. No permanent acquisition of the park would occur; however, the proposed Project under all Build Alternatives (Alternatives 2 through 5) would require a TCE along the park property directly adjacent to LCR. The existing driveways of the Big Bend Staging Area and Willow Canyon Staging Area will remain open throughout construction to allow for full use of the parking lot and continued access to the park. No parking spaces are anticipated to be impacted as a result of construction activities.

Laguna Beach Dog Park and Laguna Beach Batting Cages are also identified as eligible Section 4(f) resources within the Project limits. TCEs would be required of these two properties under all Build Alternatives (Alternatives 2 through 5). In addition, Alternative 5 would also require a partial acquisition of the Laguna Beach Batting Cages. Access to the park and batting cages will remain open during construction. No parking spaces are anticipated to be impacted as a result of construction activities.

The Project's temporary impacts under the Build Alternatives (Alternatives 2 through 5) to both parks and the batting cages, and the permanent impacts to the batting cages under Alternative 5 only, would not affect the activities, features, or attributes of the Section 4(f) resource. Therefore, the temporary occupancy and/or partial acquisition of these properties (depending on the Build Alternative) are anticipated to result in a de minimis finding.

A Section 4(f) Evaluation will be necessary to document findings and recommendations of the Section $4(f)$ properties during the PA/ED phase. The anticipated finding of the Section 4(f) Evaluation is De Minimis for all three properties due to the limited nature of impacts to Laguna Coast Wilderness Park, Laguna Beach Dog Park, and Laguna Beach Batting Cages.

### 5.2 Noise

Although the Project under Build Alternatives 2 through 4, would not construct a highway on a new location, physically alter an existing highway either horizontally or vertically,
propose the addition of a through-traffic lane, auxiliary lane, or restriping existing pavement for the purpose of adding a through traffic lane or auxiliary lane, Build Alternative 5 would propose the additional traffic lane (although only at peak hour conditions along LCR). As a result of Alternative 5, the proposed Project would be classified as a Type I project under Title 23, Part 772, Code of Federal Regulations and thus, be subject to long-term operational noise analysis.

Additionally, the proposed Project under the Build Alternatives (Alternatives 2 through 5) would experience construction related noise impacts. These impacts are considered temporary. Therefore, A Noise Study Report (NSR) is recommended to address shortterm construction impacts, and long-term operation impacts related to noise with the proposed Project.

### 5.3 Biological Resources

The Biological Study Area (BSA) supports Habitats of High Concern as determined by the Open Space - Conservation Element of the City's General Plan and five habitats the California Department of Fish and Game (CDFW) considers special-status. Project approval could be affected by the cost of compensatory mitigation for direct impacts to non-covered habitats.

Available literature resources, including the California Department of Fish and Wildlife's California Natural Diversity Database RareFind 5 program (Online CDFW 2018), California Native Plant Society's (CNPS) Inventory of Rare and Endangered Plants of California (Online Edition, v. 8.2; CNPS 2018), Consortium of California Herbaria (Jepson Flora Project 2018), and the United States Fish and Wildlife Service (USFWS) online Information for Planning and Consultation Environmental Conservation Online System were reviewed to identify special-status plant and wildlife species and designated Critical Habitat with the potential to occur in the vicinity of the Project limits. Searches of the California Natural Diversity Database and CNPS databases were conducted for the six U.S. Geological Survey 7.5' quadrangles surrounding the Project, which include Newport Beach, Tustin, El Toro, Laguna Beach, San Juan Capistrano, and Dana Point, California.

Additional resources used to characterize existing site conditions included: U.S. Geologic Survey topographic maps at a minimum 1:24,000 scale, USFWS National Wetland Inventory dataset, Natural Resource Conservation Service Soil Mapping, aerial imagery available on Google Earth, and a field visit to conduct vegetation mapping and a habitat assessment for special-status species with potential to occur in the vicinity of the proposed Project. The consultant biologist also identified all aquatic features with the potential to be regulated by the US Army Corps of Engineers and RWQCB pursuant to Sections 401 and 404 of the Clean Water Act, respectively, and by CDFW pursuant to Section 1600 of California Fish and Game Code. This assessment did not include a delineation of jurisdictional boundaries or wetland determination. Vegetation units were defined based on methodology defined in the online Manual of California Vegetation (CNPS 2018).

Species listed under the federal and/or California Endangered Species Acts with potential to occur in and/or adjacent to the BSA include the federally threatened CAGN, federally and state-endangered least bells vireo (LBVI), and federally and state-endangered southwestern willow fly catcher (SWFL). No other federally or state-listed species are expected to occur within or adjacent to the BSA. No critical habitat occurs within the BSA.

Build Alternatives (Alternatives 2 through 5) may directly impact all three listed species through habitat removal and may indirectly impact these species through temporary disturbance from construction noise, dust, or lighting during the breeding season. No direct impacts to these species are anticipated after implementation of avoidance and minimization measures. The proposed Project activities are covered by the NCCP/HCP. Impacts to CAGN are covered the Natural Community Conservation Plan/Habitat Conservation Plan (NCCP/HCP) and impacts to LBVI and SWFL are conditionally covered by the NCCP/HCP. Compliance with the NCCP/HCP may require protocol presence/absence surveys for LVBI and SWFL. Should either species be present, a Species-Specific Mitigation and Monitoring Plan (Plan) would be required. The Plan would include avoidance and minimization measures such as 1) prohibiting the removal of suitable habitat during the breeding season, 2) conducting pre-construction surveys, and 3) establishing no-construction buffers. After implementation of these measures, direct impacts to LBVI or SWFL are not anticipated. However, compensatory mitigation may be required for indirect impacts to these species, should they be present, as a result of the loss or modification of suitable habitat.

The BSA may support 10 special-status plant species, none of which are federally or state-listed. However, only a small amount of potentially suitable habitat for these species (generally less than 0.25 acre of any single native vegetation community) would be directly impacted by the Project and these areas occur in narrow disturbed strips (generally less than 0.1 acre in size) and no more than $30-\mathrm{ft}$. of the edge of LCR pavement. As a result, it is unlikely, even if one of these species was present, that the number of plants in the impact area would constitute a significant local population. Therefore, no compensatory mitigation would be anticipated for potential impacts to special-status plant species. General avoidance and minimization measures such as 1) installing high-visibility fencing at authorized work limits in the vicinity of suitable habitat, 2) implementing water quality Best Management Practices (BMPs) and 3) implementing dust control BMPs would limit potential indirect impacts to these special-status plant species.

The Project has the potential to directly and indirectly impact other special-status amphibian, reptile, and mammal species. However, only a small quantity of potentially suitable habitat falls within the actual Project limits. As a result, it is unlikely, with the exception of American badger, that even if one of these species was present, that measures beyond avoidance and minimization of impacts beyond the Project limits would be required. Species-specific pre-construction surveys may be required to avoid direct impacts to American badger.

Migratory birds, including NCCP/HCP covered species, could nest throughout the Project limits. Direct impacts to migratory bird breeding habitat should be avoided during the
breeding season, typically defined as February 15 through August 31. If removal of nesting habitat is necessary during the breeding season, pre-construction nesting bird surveys would be required. If nesting birds were detected, appropriate no-construction buffers would be required to prevent take of the nest.

Build Alternatives (Alternatives 2 through 5) have the potential to directly impact nesting migratory bird species and other special-status plant and wildlife species. In order to avoid and/or minimize direct impacts, the following measures should be included in the Project:

- Avoid impacts to migratory bird breeding habitat during the breeding season, typically defined as February 15 through August 31.
- If nesting habitat removal is necessary during the breeding season, preconstruction nesting bird surveys would be required. If nesting birds are detected, appropriate no-construction buffers would be required to prevent take of the nest.
- Conduct American badger and burrowing owl pre-construction surveys,
- Implement BMPs to prevent construction debris, invasive species, and dust from entering waterways or adjacent preserve areas,
- Install Environmentally Sensitive Area fencing to clearly delineate work authorized limits,
- Reduce work areas to the extent feasible,
- Provide Worker Environmental Awareness Training

The BSA includes linear aquatic features that have the potential to be regulated by US Army Corps of Engineers and RWQCB as non-wetland Waters of the U.S, by CDFW as unvegetated streambed, and by California Coastal Commission (CCC) as wetlands. A Jurisdictional Delineation (JD) is required and will be conducted to support regulatory permitting, if needed. Additionally, CDFW and CCC may regulate special-status or riparian habitats where they occur within the Project limits. Compensatory mitigation is likely to be required if the Project results in the loss of aquatic features.

The Project is anticipated to be of limited scope and impact to biological resources, and is anticipated to have a "no effect' or "may affect, not likely to adversely affect" determination for impacts to federally listed species. Additional avoidance, minimization, and/or mitigation measures may be identified in the Natural Environmental Study (Minimal Impacts) (NES[MI]) and JD during the PA/ED phase.

### 5.4 Water Quality and Erosion

Construction work under the Build Alternatives (Alternatives 2 through 5) would disturb over one acre of soil and would require Stormwater Pollution Prevention Plan (SWPPP). BMPs identified in the SWPPP would be implemented to address potential impacts to water quality and soil erosion. Construction and maintenance BMPs are anticipated. Maintenance BMPs would include the installation of drain inlet stenciling on all inlet and catch basins. Construction BMP categories would include soil stabilization, sediment control, tracking control, wind erosion control, non-storm water management, waste management, and materials pollution control. Project specific BMPs would be determined
during the final design phase of the proposed Project. A Water Quality Technical Memorandum will be prepared during the PA/ED phase.

### 5.5 Air Quality

During construction of the proposed Project under the Build Alternatives (Alternative 2 through 5), short-term degradation of air quality may occur due to the release of particulate emissions (airborne dust) generated by excavation, grading, hauling, and other construction-related activities. Emissions from construction equipment are also expected and would include CO, NOX, volatile organic compounds (VOCs), directlyemitted particulate matter ( $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$ ), and toxic air contaminants such as diesel exhaust particulate matter. A construction emission analysis would be required to determine what mitigation, if any, would be required to meet the local South Coast Air Quality Management District (SCAQMD) California Environmental Quality Act (CEQA) thresholds.

Build Alternatives (Alternatives 2 through 5) are anticipated to require avoidance, minimization, and/or mitigation measures including any activities involving ground disturbance be required to follow the Caltrans Standard Specifications for Construction, the South Coast Air Quality Management District Rule 403 relating to controlling dust emissions and maintain engines to ensure good condition to limit ozone precursor emissions. Due to the inclusion of a reversible lane option under Alternative 5, the Project is also subject to regional conformity and must be modeled in the Regional Transportation Plan (RTP) and the FTIP. An Air Quality Assessment Report (AQAR) is recommended during the PA/ED phase.

### 5.6 Cultural Resources

The area within the Project limits under the Build Alternatives (Alternatives 2 through 5) may adversely affect archeological sites and historic resources. To adequately evaluate impacts of the proposed Project under Alternatives 2 through 5 on archaeological resources, a Caltrans format Archaeological Survey Report (ASR) is recommended. Depending on the results of the ASR and if the Project boundaries change to include any archaeological resources an Extended Phase I Survey may become necessary. Caltrans has recently evaluated the segment of SR-133/LCR between PM 0.0/7.8 for another project as ineligible for the NRHP/CRHR or as a CHL; SHPO concurred $7 / 24 / 18$. Due to the presence of the Laguna Canyon Historic District, that is considered locally eligible, a Historical Resource Evaluation Report (HRER) may also be necessary. Each of these studies would be appended to a Caltrans format Historic Property Survey Report (HPSR). Under Section 106 of the National Historic Preservation Act (NHPA) consultation will be necessary with local Indian Tribes. Caltrans will be the CEQA lead agency and will need to conduct consultation with California Native American groups, per Assembly Bill 52 (AB 52). Additional measures identified in HPSR, ASR, and HRER (if necessary) may be determined in the PA/ED phase.

### 5.7 Paleontological Resources

The proposed Project is underlain by multiple geologic units, most of which have a high potential to contain significant paleontological resources based on previously recorded fossil localities, field surveying, and literature searches. Impacts to paleontological resources are a possibility. A combined Paleontological Identification Report/Paleontological Evaluation Report (PIR/PER) will be prepared during the PA/ED phase, and if potential impacts to significant paleontological resources may occur based on proposed construction activities, a Paleontological Mitigation Plan (PMP) will be completed during the PS\&E phase to outline mitigation measures to reduce impacts. Measures to reduce impacts under the Build Alternatives (Alternatives 2 through 5) would include, but not be not limited to, the preparation of a paleontological mitigation plan and training for onsite personnel by a Principal Paleontologist and the presence of a qualified Paleontological Monitor onsite during construction activities. Should any paleontological resources be discovered during construction, requirements approved by Caltrans outlined in the PMP would be followed. Additional measures may be determined during the preparation of the PMP and would be adhered to.

### 5.8 Hazardous Waste/Materials

Under the Build Alternatives (Alternatives 2 through 5), no recognized environmental conditions (REC), based on the ASTM standard definition of RECs, have been identified for the proposed Project. However, the following environmental conditions may be encountered during Project construction activities:

- Aerially-Deposited Lead. Previously undisturbed soil areas and any unpaved areas within Caltrans ROW along the shoulders of SR-133 has the potential to contain aerially-deposited lead (ADL) soils.
- Paint and Thermoplastic Striping. Yellow paint used for lane striping and pavement marking along SR-133 may contain lead chromate.
- Polychlorinated Biphenyls. Utility pole- and pad-mounted electrical transformers within the Project limits may contain polychlorinated biphenyls (PCB).
- Creosote and Pentachlorophenol. Wooden utility poles within the Project limits may contain creosote and pentachlorophenol.

A full ISA is recommended for the PA/ED phase. Avoidance, minimization, and/or mitigation measures will be identified within the ISA prepared during the PA/ED phase. These measures are anticipated to include, but would not limited to, Preliminary Site Investigations (PSI) such as an ADL investigation in areas with undisturbed soil or unpaved shoulder areas, a PCB investigation associated with utility lines and electrical transformers, and a lead investigation for yellow paint used for lane striping or pavement marking. Additional measures may be identified within the ISA during the PA/ED phase.

## 6. Permits and Approvals

It is anticipated that the proposed Project will require the following permits and approvals identified in Table 2. Required Project Permits and Approvals.

Table 2. Required Project Permits and Approvals

| Required Permit/Approval | Approval Timeframe |
| :--- | :---: |
| California Statewide National Pollutant Discharge Elimination <br> System (NPDES) General Permit for Discharges of Storm Water <br> Associated with Construction Activity (Order No. 2009-0009-DWG, <br> NPDES No. CAS000002). | 3 to months |
| San Diego RWQCB: Section 401 Water Quality Certification | 8 to 12 months |
| U.S. Army Corps of Engineers: Section 404 Nationwide Permit | 3 to 6 months |
| California Department of Fish and Wildlife 1602 Streambed <br> Alteration Agreement | 3 to 6 months |
| California Coastal Commission/City of Laguna Beach: Coastal <br> Development Permit (State and Local Jurisdiction) | 3 to 6 months |
| State Water Resources Board: Construction General Permit | 3 to 6 months |
| State Historic Preservation Office Consultation | 4 to 5 months |
| De minimis finding from Orange County Parks and City of Laguna <br> Beach | 3 to 6 months |
| Approval of permanent partial acquisitions and/or easements | 3 to 6 months |

## 7. Level of Effort: Risks and Assumptions

The proposed Project contains multiple risks factors and assumptions. These risks factors and assumptions, discussed below, could add additional time, due to preparation and agency review and concurrence/approval, to the schedule and increase costs.

- If significant impacts are identified, it could elevate the environmental document from an IS/MND to an EIR, increasing the Project cost and schedule;
- Uncertainty in regulatory permitting timelines;
- Public controversy could delay the schedule;
- Unanticipated seasonal special status species surveys;
- Partial acquisitions will be required under all Build Alternatives (Alternatives 2 through 5). If difficulties arise during acquisitions, a delay of schedule may occur.


## 8. PEAR Technical Summaries

8.1 Land Use: Land uses within the Project limits are generally rural in character and include Permanent Open Space, Open Space, Residential/Hillside Protection, Public/Institutional, Light Industrial, Village Low Density and Medium Density, and Central Business District, per the City's General Plan Land Use Map (2009). The Project is also located within the Residential Hillside Protection Zone (R/HP) and

Village Community Zone (VC), per the City of Laguna Beach General Plan Zoning Map (2009) and is located within the CCC jurisdiction.

Table 1. Right-of-Way Impacts -Partial Acquisitions in Section 5.1.4 summarizes the ROW impacts for permanent partial acquisitions. The proposed Project under Alternatives 2 through 5 would require the partial acquisition of two parcels (APN 495-021-30 City Corporation Yard and APN 495-021-09 Laguna College of Art and Design). Alternatives 2, 3, and 5 would also require a partial acquisition of these two parcels; whereas, Alternative 4 would only require a permanent easement. Alternative 4 would require 16 additional permanent partial acquisitions and Alternative 5 would require 27 additional permanent partial acquisitions. TCEs are anticipated for the proposed Project for turn pockets, a local roadway intersection, private driveway reconstruction, and other proposed Project improvements. The partial acquisitions, permanent easements, and TCEs are for both privately and publicly owned property.

Although the land use designation of parcels requiring permanent partial acquisition would change to a transportation public ROW, the Build Alternatives (Alternatives 2 through 5) would not change the existing function and use of these properties. The surrounding lands would also continue to remain the same.
8.2 Growth: The proposed Project would not induce growth within the City. The proposed Project is intended to be make safety and operational improvements to the highway, not increase the capacity. It is recommended that growth impacts related to the proposed Project be documented in the environmental document during the PA/ED phase.
8.3 Farmlands/Timberlands: Based on the information from the Land Use Element of the City's General Plan (2012), there are no designated farmlands within the proposed Project limits. In addition, as designated by the California Department of Conservation no land has been classified as prime farmland, farmland of statewide importance, or unique farmland. No timberlands have been identified in the Project limits or in the vicinity of the proposed Project. Therefore, no impacts would occur to designated farmlands or timberlands as a result of the proposed Project and no further studies for this topic would be recommended during the PA/ED phase.
8.4 Community Impacts: The proposed Project proposes to relocate existing utility lines underground and to install traffic signalization at the intersection located at the Laguna College of Art and Design's main campus driveway. Temporary noise, dust, and traffic circulation and access issues to the community, in particular to nearby residential properties, businesses, schools, and recreational users, are anticipated during construction. However, these impacts are considered temporary, and would cease upon the completion of construction.

Additionally, as shown in Table 3. Consistency with Regional and Local Plans, the Build Alternatives (Alternatives 2 through 5) are consistent with existing regional and local plans. In addition, the Build Alternatives (Alternatives 2 through 5) are
consistent with applicable City General Plan goals and policies to provide a safe circulation system for all users while protecting and encouraging bicycle and pedestrian travel. Table 3. Consistency with Regional and Local Plans summarizes the Project's consistency with adopted regional and local plans.

Table 3. Consistency with Regional and Local Plans

| Goals and Policies | Project Consistency |
| :---: | :---: |
| Southern California Association of Governments - Regional Transportation Plan 2012$2035{ }^{1}$ |  |
| Challenge Area 7 - Local jurisdictions should incorporate signalization at problem non-signalized intersections. | Consistent |
| Challenge Area 8 - Local jurisdictions should consider pedestrian needs in all roadway and transit projects | Consistent |
| Challenge Area 13 - Local jurisdictions should fund and install dedicated bicycle facilities where appropriate and safe. | Consistent |
| County of Orange General Plan - Recreational Element ${ }^{\mathbf{2}}$ |  |
| Policy 1.3 - Regional riding and hiking trails shall, to the extent possible, be designed and constructed to enhance public safety by affording access to law enforcement, fire, emergency, public utility and maintenance vehicles. | Consistent |
| Policy 2.3 - Trail closures shall be kept to a minimum and, if a trail is closed, efforts should be made to have alternative trail routes available. | Consistent |
| City of Laguna Beach General Plan - Land Use Element ${ }^{3}$ |  |
| Policy 2.1-Maintain the diversity and uniqueness of individual neighborhoods. Development standards and design review guidelines shall minimize the scale and bulk of new construction and/or renovation and require development to be compatible with the surrounding residences. | Consistent |
| Policy 2.3 - Preserve and enhance the qualities that contribute to the character of the residential community, including quiet neighborhoods, pedestrian use of streets, and appropriate levels of illumination and nighttime activity and seek to mitigate the effects of high-volume thru-traffic. | Consistent |
| Policy 3.1 - Promote development that is compatible with the pedestrianoriented village character of the downtown (e.g., small lot sizes and height limitations). | Consistent |
| Policy 3.5-Promote safe and adequate pedestrian access to and within commercial areas. | Consistent |
| Policy 3.8 - Encourage pedestrian access and orientation in all commercial areas. | Consistent |
| Policy 4.3 - Maintain and enhance access to coastal resource areas, particularly the designated public beaches, by ensuring that access points are safe, attractive, and pedestrian friendly. | Consistent |
| Policy 6.9 - Provide public access to designated public areas wherever safe and legally and environmentally appropriate. | Consistent |
| Policy 7.2 - Maintain the General Plan designation of Permanent Open Space and the Zoning designations of Open Space/Conservation and Open Space/Passive as a method of protecting natural resources. | Consistent |
| Policy 8.1 - Encourage a pedestrian-oriented, non-motorized community by developing a system of bikeways and pedestrian paths and discouraging high-speed traffic along City streets. | Consistent |

Table 3. Consistency with Regional and Local Plans

| Goals and Policies | Project Consistency |
| :---: | :---: |
| Policy 8.2 - Maintain a pedestrian-oriented community while facilitating the movement of traffic in a safe and uncongested manner. | Consistent |
| Policy 8.3 - Provide walking and biking opportunities to link residential and commercial neighborhoods through improvements such as sidewalks, bicycle lanes and multi-use trails. | Consistent |
| Policy 8.5 - Require the construction of sidewalks and pathways and/or sidewalk widening on streets that carry significant pedestrian traffic. | Consistent |
| Policy 9.5 - Ensure that streetscapes are designed or modified to facilitate safe transit and bicycle and pedestrian movement. | Consistent |
| Policy 9.8 - Avoid the extension of community facilities, roads, and other infrastructures into environmentally sensitive areas when surplus capacities could facilitate or discourage extension of new development detrimental to those areas. Avoid the extension of roads and other infrastructure for the support of cellular/radio communication towers into environmentally sensitive areas and to protect public coastal views whenever feasible. | Consistent |
| City of Laguna Beach General Plan - Transportation, Circulation and Growth Management Element ${ }^{4}$ |  |
| Policy 1D - Discourage new roads and the extension or widening of existing roadways, since traffic almost always expands to fill available road capacity. | Consistent |
| Policy 2B - Discourage driveway access on Pacific Coast Highway and Laguna Canyon Road so interruptions to traffic flow are minimized. | Consistent |
| Policy 2H - Promote the safe and efficient movement of both local and through traffic, including the improvement of "bottleneck" intersections where feasible | Consistent |
| Policy 2I - Promote a local circulation system which serves the community and provides linkages to neighborhoods and regional transit facilities. | Consistent |
| Policy 2M - Avoid extending roads and utilities to identified Environmentally Sensitive Areas and unincorporated County lands. | Consistent |
| Policy 2P - Require proposals for major road improvements, alterations or major public works projects in Laguna Canyon to provide sufficient information on environmental impacts and on design and construction alternatives to enable the City to evaluate the proposal for conformance with all applicable general plan policies. Ensure that any such project is the least environmentally damaging alternatives and is approved only if sized, sited and designed in a manner that will not degrade environmentally sensitive areas, scenic resources, significant natural landforms, parks or recreation areas. | Consistent |
| Policy 6G - To enhance and increase public access, pursue funding for planning and development of a peripheral parking program for parking, increased access to the beaches and transit opportunities. Specifically, study the Pacific Coast Highway corridor, Laguna Canyon Road, El Moro school and the downtown area for parking and transit opportunities, including appropriate locations for parking structures. | Consistent |
| Policy 9C - Support and coordinate the development and maintenance of bikeways in conjunction with the county of Orange Master Plan of Countywide Bikeways to assure that local bicycle routes will be compatible with routes of neighboring jurisdictions. In particular, these bikeways include | Consistent |

Table 3. Consistency with Regional and Local Plans

| Goals and Policies | Project <br> Consistency |
| :--- | :--- |
| Route 67 through Laguna Laurel Regional Park, Route 71 along Laguna <br> Canyon Road, Route 75 along El Toro Road and Route 25 along Pacific <br> Coast Highway. |  |
| Policy 9E - Encourage the safe utilization of easements and/or rights-of-way <br> along flood control channels, public utility rights-of-way and street rights-of- <br> way wherever possible for use by bicyclists and/or hikers. | Consistent |
| Policy 9F - Encourage pedestrian access and orientation in the Central <br> Business District. | Consistent |
| Policy 10A - Improve and maintain the transportation system to further <br> enhance adequate emergency access to all developed areas. | Consistent |
| City of Laguna Beach General Plan - Transportation, Circulation and Growth <br> Management Element |  |
| Policy 1P - Inform utility companies of potential conflicts between the <br> location of their facilities and the currently identified high or extreme hazard <br> areas and encourage them to program for relocation or undergrounding of <br> potentially impacted facilities, especially along designated primary <br> emergency routes. | Consistent |
| Policy 1S - Continue to encourage the undergrounding of utilities in existing <br> developed areas of the City and require any new development to <br> underground utilities. | Consistent |
| Laguna Canyon Annexation Area Specific Plan ${ }^{6}$ |  |
| Goal B - Balance the need for street improvements against the objective to <br> protect the existing rural character of the Canyon annexation area. | Consistent |
| Downtown Specific Plan |  |

The proposed Project is located within Census Tracts 626.04, Block Group 2, and Census Tract 626.32, Block Group 1. Census data block group data from the 20122016 United States Census Bureau American Community Survey (ACS) 5-Year Estimates was used to gather demographic and economic information. Based on the census data, no environmental justice communities were identified.

The area within the Project limits consist of a predominately White population (72 percent). This is below the City's White population of 90 percent, but is higher than the County's White population of 63 percent. The area within the Project limits is not considered an environmental justice community because the non-white population and other non-white race groups within the area within the Project limits do not exceed 50 percent of the affected area. In addition, when analyzing the two census tracts (Census Tract 626.04, Block Group 2 and Census Tract 626.32, Block Group 1) that comprises of the area within the Project limits individually, both census tracts have a predominately White population ranging from 58 and 87 percent. Therefore, these census tracts are not considered an environmental justice community because the non-white population and other non-white race groups within these census tracts do not exceed 50 percent of the affected area.

The average median household income of $\$ 97,486$ for a household of 2.34 persons is well above the 2018 Health and Human Services (HHS) poverty threshold of $\$ 20,780$ for a household of three persons. As such, the area within the Project limits is not considered a low-income population. The median household income for each of the individual census tracts that comprises the area within the Project limits are also well above the 2018 HHS poverty threshold, ranging from $\$ 74,435$ to $\$ 120,536$ for a household of 2.26 to 2.41 persons, respectively. Therefore, these census tracts are not considered to be low-income populations.

## Real Property Acquisition

The proposed Project would improve the existing roadway and would not alter existing communities. It will improve existing traffic, pedestrian, and bicycle facilities along LCR, a major transportation corridor for adjacent communities. Partial acquisition of two parcels would be required under all Build Alternatives (Alternatives 2 through 5). These parcels are identified as APNs 495-021-30 (City Corporation Yard) and 495-021-09 (Laguna College of Art and Design). Alternatives 2,3 , and 5 would also require a partial acquisition of these two parcels; whereas, Alternative 4 would only require a permanent easement. Alternative 4 would require 16 additional permanent partial acquisitions and Alternative 5 would require 27 additional permanent partial acquisitions, as identified in Table 1. Right-of-Way Impacts -Partial Acquisitions.

Although no relocations are anticipated at this time, should a change in Project design occur during the PA/ED phase where relocation is found to be required, then preparation of a Relocation Impact Memorandum would be recommended. Relocations would be subject to the Federal Uniform Relocation Assistance and Real Property Acquisition Policies Act of 1970 and Title 49 Code of Federal Regulations (CFR), Part 24. Relocations and ROW acquisitions would be processed through the Caltrans' Relocation Assistance program, and costs associated with the property acquisitions and assistance would be included in the Project cost estimates.

Traffic and Transportation/Pedestrian and Bicycle Facilities
The Orange County Transportation Authority (OCTA) operates Bus Route 89 which provides transit service from inland areas to downtown Laguna Beach via El Toro Road and LCR - terminating at the downtown Laguna Beach Bus Station. Ten bus stops are located within the Project limits, as follows:

- Anneliese's School (in the NB direction of LCR)
- Willow Canyon Staging Area/Laguna Coast Wilderness Park, located just south of El Toro Road in the SB direction of LCR)
- Vicinity of Stans Lane and Phillips Street, located just north of Sun Valley Drive (in the NB and SB directions of LCR)
- Vicinity of Stan Oaks Drive (in NB and SB directions of LCR)
- Laguna Canyon of Art \& Design Main Campus (in NB and SB directions of LCR)
- Vicinity of Canyon Acres Drive (in NB and SB directions of LCR)

The City also operates a trolley bus service during the summer months to help relieve the traffic demand associated with beachgoers and other visitors heading to Laguna Beach for special events. This trolley service provides a shuttle between the City Maintenance Yard/Municipal Parking Lot (ACT V Parking Lot), which is heavily used as a park-and-ride lot, and other points downtown. In addition, a weekend Summer Breeze service (OC Bus Route 689) operates during the peak summer months providing bus service from a parking lot near the intersection of SR-133/I-405 to the downtown Laguna Beach Bus Station with intermediate stops at key destinations along LCR. During construction of the proposed Project, there may be potential impacts to bus and trolley service times and routes.

The existing roadway within the Project limits lacks pedestrian paths or sidewalks, or a designated bikeway, forcing pedestrians and bicyclists to use the limited shoulders to gain access to the various businesses, schools, recreational areas and trails, and transit stops along LCR. The proposed Project would improve pedestrian and bicycle mobility and safety and encourage the use of active transportation along the corridor by adding Class I and Class II bicycle lane(s), pedestrian pathways, and sidewalks with ADA access; improving access to transit facilities; and improving shoulders along the corridor.

## Parking

City of Laguna Beach Maintenance Facility Parking Lot 16 (ACT V Lot)
Temporary impacts are anticipated at the City's Maintenance Facility Parking Lot 16. The Project anticipates to utilize the City's Parking Lot 16 as a potential staging area (identified as Staging Area 1 on Figure 2. Project Limits in Attachment A) during construction. The use of the parking lot as a staging area is considered a temporary impact and will cease upon completion of construction. Additionally, after construction, the parking lot will be returned to its existing condition. Access to the City's Maintenance Facility Parking Lot 16 will remain accessible throughout
construction. No temporary or permanent loss of parking spaces are anticipated as a result of the Project.

## Laguna College of Art \& Design Main Campus

Temporary impacts are anticipated at the Laguna College of Art \& Design Main Campus with regards to the entrance to the parking lot off of LCR. Access to the parking lot will remain accessible throughout construction. No temporary or permanent loss of parking spaces are anticipated as a result of the Project.

## Laguna Coast Wilderness Park

Temporary impacts will occur to the existing parking lot at Laguna Coast Wilderness Park specifically in the areas of entrance to the Big Bend Staging Area and Willow Staging Area. A TCE is required in the existing driveways of the staging areas. However, access to these two driveways will remain open throughout construction to allow for full use of the parking lot. No temporary or permanent loss of parking spaces are anticipated as a result of the Project.

Although no impacts to parking spaces are anticipated at the City's Maintenance Facility Parking Lot 16, Laguna College of Art \& Design Main Campus, and Laguna Coast Wilderness Park, permanent and temporary impacts to City-permitted on-street parking may occur along LCR within the Project limits. A parking study will be conducted during the PA/ED phase as part of the Traffic Study to further analyze these impacts, and to provide measures to reduce and minimize these impacts.

A CIA is recommended to be prepared during the PA/ED phase to further analyze the impacts discussed above, and to provide measures to reduce and minimize these environmental impacts. A Relocation Impact Memorandum is only recommended if during the PA/ED phase there are Project design changes where relocation is found to be required.

## Section 4(f) Resources

Funding for the proposed Project is being sought from federal, state, and local sources. If the Project involves the use of federal funds, then the Project would be subject to Section 4(f) evaluation. There are parks and a recreational facility located within the Project limits, including the Laguna Coast Wilderness Park, Laguna Beach Dog Park, and Laguna Beach Batting Cages. The Build Alternatives (Alternatives 2 through 5) would require a TCE which would result in the temporary occupancy of the Laguna Coast Wilderness Park property, Laguna Beach Dog Park property, and Laguna Beach Batting Cages property that are located directly adjacent to the roadway improvements. In addition, Alternative 5 would also require a partial acquisition of the Laguna Beach Batting Cages. Orange County Parks is the OWJ of the Laguna Coast Wilderness Park, and the City is the OWJ of the Laguna Beach Dog Park and the Laguna Beach Batting Cages. The existing use of both parks and the batting cages will remain unchanged and access to the parking area would not be impacted during construction. Areas affected by the TCEs will be restored upon completion of construction. The Project's temporary impacts under the Build Alternatives (Alternatives 2 through 5) to both parks and the batting cages, and the permanent impacts to the parking area of the batting cages under Alternative 5, would not affect the existing activities, features, or attributes of these Section 4(f) resources. Therefore, the temporary occupancy of these properties (depending on the Build Alternative) are anticipated to result in a de minimis finding. A Section 4(f) Evaluation will also be prepared during the PA/ED phase to evaluate the requirements of Section 4(f) and to document the use finding, and coordination and concurrence from Orange County Parks and the City.
8.5 Visual/Aesthetics: The proposed Project under the Build Alternatives (Alternatives 2 through 5) would not include features that will visually degrade the view of LCR or views from LCR to neighboring businesses and hillsides. The Project would underground the overhead transmission lines within the Project limits along LCR. Undergrounding the transmission lines would remove vertical intrusions allowing less obstructions to scenic hillside resources from LCR within the Project limits. Thus, prominent ridgelines will not be impacted as a result of the proposed Project. If impacts were to occur, avoidance, minimization, and/or mitigation measures would be implemented to ensure the integrity of these features and remain consistent with the City's General Plan and the City's LCP. A VIA Technical Memorandum is recommended to be prepared during the PA/ED phase.
8.6 Cultural Resources: On April 18, 2018, a records search at the South Central Coastal Information Center, a part of the California Historical Resources Informational System, located at California State University Fullerton was conducted. The literature search revealed two historic cultural resources within the proposed Project limits:

30-177470, Historical route of LCR constructed prior to 1896; Caltrans has recently evaluated the segment of SR-133/LCR between PM 0.0/7.8 for another project as ineligible for the NRHP/CRHR or as a CHL. SHPO concurred on July 24, 2018.

30-177656, Laguna Canyon Historic District comprised of pre-1940s residential homes including homes located along LCR and in the Canyon Acres neighborhood adjacent to the LCR located at the southern end of the proposed Project. This resource is listed in the Historic Properties Data File (HPDF) and the City's local Historic Resources Inventory (2014) as not eligible for the NRHP/CRHR but determined to be a contributor to a district that is eligible for local listing or designation (NRHP Status Code: 5D2).

Additionally, twelve prehistoric and six historic cultural resources are recorded within $1 / 4$ mile of the proposed Project limits. One of these resources, 30-000285, is a prehistoric burial consisting of a human cranium that was exposed by a road grader in 1935. This resource is thought to be associated with the nearby Hogan Site, 30-000286, a nearby rock shelter containing two manos and a broken awl, as well as shell midden.

There have been approximately forty previous cultural resources studies conducted within $1 / 4$ mile of the proposed Project limits. Of these, twenty-seven are located within the Project limits or a portion thereof. Fifteen of the studies within $1 / 4$ mile of the Project limits had large study areas greater than ten acres; twenty-one had study areas of less than ten acres; and four were linear surveys. The entire Project limits has been previously surveyed for cultural resources.

A reconnaissance-level windshield survey was conducted on April 23, 2018. The survey confirmed that the majority of the immediate Project limits can be categorized as a built environment consisting of the paved highway SR-133/LCR. Laguna Coast Wilderness Park runs along the west side of Highway SR-133/LCR. This area is primarily undeveloped; however, the main recreational portion of the park it is not within the Project limits. A TCE is estimated to be required for the construction of the proposed road and adjacent sidewalks along LCR, and would be located on the outer most edge of the park's property that is directly adjacent to LCR.

The east side of SR-133/LCR is primarily developed with commercial businesses and residential properties. Ground visibility is poor in most areas of the Project due to the built environment, developed shoulders, and dense grasses and vegetation. Nearly all visible soils adjacent to LCR within the Project limits or the existing ROW appear disturbed due to road construction or other modern disturbances. The exception is an approximately 1,500 -square-foot area of land on the east side of LCR, east of the Laguna College of Art \& Design, which is indicated as being within the Project limits on the PSR/PDS Project description maps. This land is signed as a habitat restoration area, and is overgrown with vegetation and appears undisturbed. There are also several small slivers of land within the existing ROW on the west side of LCR near the southern Project limits boundary that appear undisturbed.

The records search identified prehistoric and historic archaeological resources within 0.25 miles of the proposed Project limits, including the presence of prehistoric
human remains. These sites are not within the Project limits. There is a historic residential district immediately adjacent to the Project which has been determined not eligible for the NRHP/CRHR but is considered locally significant and may be impacted by the Project (30-177656). Caltrans has recently evaluated the segment of SR-133/LCR between PM 0.0/7.8 for another project as ineligible for the NRHP/CRHR or as a CHL. SHPO concurred on July 24, 2018.

Additionally, the NAHC indicated that the area is sensitive for cultural resources as did several Native American groups. Development of the area has likely disturbed and/or obscured prehistoric and historic archaeological resources, making it difficult to accurately predict the potential for impacting archaeological resources within the majority of the proposed Project limits. However, the survey identified several areas within the proposed Project limits and/or existing ROW which may not have been previously disturbed.

The potential for the Project under the Build Alternatives (Alternatives 2 through 5) to impact previously undisturbed soils, along with the presence of human remains in close proximity to the proposed Project limits, indicates a high sensitivity for cultural resources when working in previously undisturbed sediments. Therefore, it is recommended that an ASR, HRER, APE Map be prepared and appended to an HPSR for the PA/ED phase.
8.7 Hydrology and Floodplain: The proposed Project is within the Laguna Canyon Channel Watershed within the San Juan Hydrologic Unit (901.12) within the San Diego RWQCB jurisdiction. According to the Safety Element of the City's General Plan (June 1995) the entire Project is located within a 100-year flood zone. Further, based on the information from the Federal Emergency Management Agency (FEMA) Map Nos. 06059C0417J and 06059C0409J, the proposed Project is located within FEMA flood designations "AE" and identified as a Floodway Area within Zone AE. Areas located within "Zone AE" have a 1 percent probability of flooding every year, or within a 100-year floodplain. "Floodway Areas in Zone AE indicates that the floodway is the channel of a stream and includes any adjacent floodplain areas that must be kept free of encroachment so that the 1 percent annual chance flood can be carried without substantial increases in flood heights.

Although these designations are identified as high-risk flood areas, the projected increase in impervious area and disturbed soil area as a result of the proposed Project under the Build Alternatives (Alternatives 2 through 5) would not be sufficient enough to trigger a Conditional Letter of Map Revision (CLOMR) or Letter of Map Revision (LOMR). In addition, the proposed Project under the Build Alternatives (Alternatives 2 through 5) is located within the Coastal Zone and as such, will need to address water quality issues not only related to City and Caltrans, but Coastal Zone standards, as stipulated in the CDP.

Therefore, a Location Hydrologic Study (LHS) is recommended to be prepared for the Project during the PA/ED phase. This LHS would evaluate potential impacts
related to hydrology and floodplain and provide the appropriate avoidance, minimization, and/or mitigation measures.
8.8 Water Quality and Storm Water Runoff: Caltrans' MS4 Permit, NPDES No. CAS000003, State Water Resources Control Board (SWRCB) Order No. 2012-0011-DWQ (adopted on September 19, 2012, and effective on July 1, 2013), as amended by Order No. 2014-0006-EXEC (effective January 17, 2014), Order No. 2014-0077-DWQ (effective May 20, 2014) and Order No. 2015-0036-EXEC (conformed and effective April 7, 2015) contains three basic requirements:

1. Caltrans must comply with the requirements of the CGP (see below);
2. Caltrans must implement a year-round program in all parts of the State to effectively control stormwater and non-stormwater discharges; and
3. Caltrans stormwater discharges must meet water quality standards through implementation of permanent and temporary (construction) BMPs to the Maximum Extent Practicable, and other measures deemed necessary by the SWRCB and/or other agency having authority reviewing the stormwater component of the project.

To comply with the permit, Caltrans developed the Statewide Storm Water Management Plan (SWMP) to address stormwater pollution controls related to highway planning, design, construction, and maintenance activities throughout California. The SWMP assigns responsibilities within Caltrans for implementing stormwater management procedures and practices as well as training, public education and participation, monitoring and research, program evaluation, and reporting activities. The SWMP describes the minimum procedures and practices Caltrans uses to reduce pollutants in stormwater and non-stormwater discharges. It outlines procedures and responsibilities for protecting water quality, including the selection and implementation of BMPs. The proposed Project will be programmed to follow the guidelines and procedures outlined in the latest Storm Water Management Plan (SWMP) to address storm water runoff. The Project will also comply with the Construction General Permit (NPDES No. CAS000002, SWRCB Order No. 2009-0009-DWQ, adopted on November 16, 2010) became effective on February 14, 2011 and was amended by Order No. 2010-0014-DWQ and Order No. 2012-0006-DWQ (effecting July 17, 2012) which regulates storm water discharges from construction sites which result in a Disturbed Soil Area (DSA) of one acre or greater, and/or are smaller sites that are part of a larger common plan of development.

The anticipated storm water project risk level is Level 2. Implementation of treatment BMPs are recommended to treat the Project targeted design pollutants. It is anticipated that post-project state ROW will provide adequate area for BMPs. This will be confirmed during the PA/ED and PS\&E phases. During the PA/ED phase, water quality impacts will be analyzed in detail within the water quality report. The water quality report will discuss the Caltrans BMP requirements, including treatment BMPs, as well as compliance with applicable laws and permits. It is assumed, during PS\&E and outlined during PA/ED within the water quality report,
the construction contractor will prepare and implement a SWPPP to address construction site BMPs during construction.

The Project is located within the Aliso Creek-Frontal-Gulf of Santa Catalina watershed and Salt Creek-Frontal Gulf of Santa Catalina sub-watershed. The Project is located within the San Juan Hydrologic Unit (HU) [901.00], the Laguna Hydrologic Area (HA) [901.10], and the Laguna Beach Hydrologic Sub-Area (HSA) [901.12] under the San Diego Regional Water Quality Control Board (San Diego RWQCB) jurisdiction. The receiving water body within the Project limits is Laguna Canyon Channel. Based on the Final 2014/2016 Califocraial Integrated Report (Clean Water Act Section 303(d) List / 305(b) Report) approved by the SWRCB and United States Environmental Protection Agency (USEPA), Laguna Canyon Channel is not listed on the 303(d) list for Total Maximum Daily Load requirements. There are no 303(d) listed waters within the Project limits. Laguna Canyon Channel ultimately drains to Pacific Ocean. A small portion of the Pacific Ocean near the Laguna Canyon Channel outlet to the Pacific Ocean has been identified on the 303(d) list for indicator bacteria.

Beneficial surface water uses for Laguna Canyon Channel as identified within the San Diego RWQCB Basin Plan are:

- Municipal and Domestic Supply (MUN) waters are used for community, military, municipal, or individual water supply systems. These uses may include, but are not limited to, drinking water supply. Laguna Canyon Channel has been excepted from the MUN beneficial use.
- Agricultural Supply (AGR) waters are used for farming, horticulture or ranching. These uses may include, but are not limited to, irrigation, stock watering, and support of vegetation for range grazing.
- Non-contact Water Recreation (REC2: Secondary Contact Recreation) waters are used for recreational activities involving proximity to water, but not normally involving body contact with water where ingestion of water would be reasonably possible. These uses may include, but are not limited to, picnicking, sunbathing, hiking, beachcombing, camping, boating, tidepool and marine life study, hunting, sightseeing, and aesthetic enjoyment in conjunction with the above activities.
- Warm Freshwater Habitat (WARM) uses of water that support warm water ecosystems including, but not limited to, preservation or enhancement of aquatic habitats, vegetation, fish or wildlife, including invertebrates.
- Wildlife Habitat (WILD) waters support wildlife habitats that may include, but are not limited to, the preservation and enhancement of vegetation and prey species used by waterfowl and other wildlife.

Laguna Canyon Channel also has the potential beneficial surface water use of:

- Water Contact Recreation (REC1: Primary Contact Recreation) waters are used for recreational activities involving body contact with water where ingestion of water is reasonably possible. These uses may include, but are
not limited to, swimming, wading, water-skiing, skin and scuba diving, surfing, whitewater activities, fishing, and use of natural hot springs.

The San Diego RWQCB Basin Plan has designated the following beneficial uses for groundwater in the Laguna Beach (HSA 901.12) as:

- Municipal and Domestic Supply (MUN) waters are used for community, military, municipal, or individual water supply systems. These uses may include, but are not limited to, drinking water supply. Laguna Canyon Channel is excepted from the MUN beneficial use.
- Agricultural Supply (AGR) waters are used for farming, horticulture or ranching. These uses may include, but are not limited to, irrigation, stock watering, and support of vegetation for range grazing.

The DSA for the Project is anticipated to be about 7 acres which includes areas for construction, access, and staging. Groundwater is estimated at approximately 7 - ft . below ground surface (bgs). Test borings will be performed in later phases of the Project to confirm depth to groundwater. Potential temporary impacts to water quality that can be anticipated during construction include sediments caused by the temporary access of construction equipment, excavation and grading for the new roadway, vegetation removal, concrete waste from the construction, trash from workers and construction waste, petroleum products from construction equipment and/or vehicles, sanitary wastes from portable toilets and any other chemicals used for construction such as coolants used for equipment and/or concrete curing compounds.

Since the Project causes a DSA greater than 1.0 acre, the Project would need to comply with the NPDES Construction General Permit. The Project would be required to prepare and implement a Storm Water Pollution Prevention Plan (SWPPP). The SWPPP would identify temporary BMPs to address the potential temporary impacts to water quality. Project specific BMP measures will be specified and quantified during the final design. Design Pollution Prevention BMPs will be incorporated into the Project where appropriate to minimize impacts to water quality by preventing downstream erosion and stabilizing disturbed soil areas.

The Project is anticipated to result in a net impervious surface area less than the existing condition if the Alternatives are selected that result in a Class I bikeway and pedestrian walkway. The Class I bikeway and pedestrian walkway would be constructed utilizing impervious surfaces allowing water infiltration in those areas. This would lessen the net impervious surfaces to a negative number. As such, the Project would not be required to implement permanent BMPs for water quality. The Project is anticipated to result in a net negative impervious surface reducing the amount of storm water and runoff from the Project limits. The existing stream thresholds would not be exceeded as a result of the Project.

The Project will require a Section 401 Water Quality Certification, a Section 404 Nationwide Permit, a Construction General Permit, and a CDP. A Water Quality Technical Memorandum is recommended for the PA/ED phase.
8.9 Geology, Soils, Seismic and Topography: The proposed Project is located in Southern California, a seismically active region with numerous faults in the area. Seismic activity is common throughout Southern California. According to the Safety Element of the City's General Plan, the proposed Project is located within a geomorphic subarea, Major Canyons. The Newport-Inglewood fault is the closest dominant fault located three miles to the west. These faults have the potential to cause moderate to severe earthquakes. According to the City's GIS database ${ }^{1}$, the Project limits are susceptible to liquefaction, a phenomenon caused when ground shaking causes the earth or soil to behave as a liquid. Impacts to geology, soils, seismic and topography will be discussed further in the environmental document during the PA/ED phase.
8.10 Paleontology: The proposed Project is located in the edge of the Peninsular Ranges geomorphic province. The Peninsular Ranges province is distinguished by northwest trending mountain ranges and valleys following faults branching from the San Andreas Fault. The Peninsular Ranges are bound to the east by the Colorado Desert and extend north locally to the Santa Monica Mountains (Yerkes and Campbell, 2005; Hillhouse, 2010), west into the submarine continental shelf, and south to the California state line.

Locally, the area within the Project limits is located in the San Joaquin Hills which is part of the Coastal Province of Orange County. The Coastal Province also includes Capistrano Hills, mesa areas, and coastal deposits on the western border of the county (Babilonia, et al., 2013). Laguna Canyon represents two disparate episodes of geologic history: the canyon walls are composed of sedimentary deposits from various marine environments in the Miocene Epoch ( 23 to 5.3 million years ago), while the canyon was cut into the San Joaquin Hills, and the sediments of the canyon floor deposited, during a low stand of global sea level during the Pleistocene Epoch ( 2.5 million years ago to 11,700 years ago).

A combined vehicular ("windshield") and pedestrian field survey of the Project limits was conducted on April 23, 2018, to verify the geology summarized in published reports and geological maps and to document any unrecorded paleontological localities. As a result, a determination can be made for the existence of paleontological material prior to the beginning of ground-disturbing activities, and areas can be located within the Project area that might contain paleontological resources.

## 1

http://gisweb.lagunabeachcity.net/Html5Viewer/index.html?configBase=http://gisweb.lagunabeachcity.net/ Geocortex/Essentials/REST/sites/GISMap3/viewers/HTML5_22/virtualdirectory/Resources/Config/Default . Accessed May 25, 2018.

The proposed Project is underlain by multiple geological units, most of which have a high potential to contain significant paleontological resources based on known fossil collecting localities, field surveying, and information from published paleontological and geological literature. The geologic units with a high potential are the young axial-channel deposits, Topanga Group, and Vaqueros Formation. These findings apply to the Build Alternatives (Alternatives 2 through 5). In order to minimize impacts to potentially fossiliferous deposits, a combined PIR/PER, following the Caltrans SER, should be prepared by a Principal Paleontologist for the PA/ED phase. If a potential to impact significant paleontological resources is determined in the PIR/PER, a PMP is required during the $83 /$ rstphase that outlines paleontological mitigation to reduce impacts during construction.
8.11 Hazardous Waste/Materials: The Project has the potential to encounter hazardous waste and materials during construction activities. Four environmental conditions were identified that would warrant PSIs during PA/ED to determine proper handling and disposal requirements. The four environmental conditions pertain to ADL, paint and thermoplastic striping (PTS), PCBs, and creosote and pentachlorophenol. PSIs are recommended during PA/ED to sample for the presence of ADL, PTS, and PCBs.

In addition to the PSIs identified above, a full ISA for all ROW acquisition properties would be prepared during PA/ED that would comply with ASTM E1527-21 to meet "innocent landowner" provisions under the Comprehensive Environmental Response, Compensation and Liability Act of 1980 (CERCLA), which establish a defense for the purchase of real property. The full ISA would include an environmental database search, review of historical land use records, field reconnaissance, interviews with knowledgeable individuals, and agency records review.

The Project would also be required to comply with the California Statewide NPDES General Permit for Discharges of Storm Water Associated with Construction Activity (Order No. 2009-0009-DWG, NPDES No. CAS000002). NPDES permit compliance would entail preparation and implementation of a SWPPP, which would include BMPs to address potential impacts related to the use and potential discharge of construction-related hazardous waste and materials such as oil, grease, paint, solvents, and sediment. There is also a potential earth-moving activity during construction may uncover unknown underground fuel storage tanks or contaminated soil and groundwater.

In addition, it is recommended that a full ISA be prepared during the PA/ED phase to identify pertinent plans that would be prepared prior to construction to protect worker health and safety and the environment in the event known and unknown hazards are encountered during construction. These plans may include a Construction Health and Safety Plan, Construction Contaminant Management Plan, and Construction Contingency Plan.
8.12 Air Quality: The proposed Project is located in Orange County, an area within the South Coast Air Basin (SCAB), which includes Orange County and the non-desert portions of Los Angeles, Riverside, and San Bernardino Counties. Air quality regulation in the SCAB is administered by the SCAQMD, a regional agency created for the Basin. The U.S. EPA has classified the SCAB as attainment/maintenance for the $\mathrm{CO}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ federal standards and nonattainment for the $\mathrm{O}_{3}$ and PM 2.5 federal standards. Under the California Clean Air Act (CCAA), the Orange County portion of the SCAB is designated as a nonattainment area for the $\mathrm{O}_{3}, \mathrm{PM}_{2.5}$, and $\mathrm{PM}_{10}$ State standards.

A site survey of the Project limits was conducted using aerial mapping and site photographs. Sensitive land uses, including residences, restaurants, college and school buildings, a marine mammal center, and a boys and girls club, were identified along LCR.

During construction, short-term degradation of air quality may occur due to the release of particulate emissions (airborne dust) generated by excavation, grading, hauling, and other construction-related activities. Emissions from construction equipment are also expected and would include CO, NOx, VOCs, directly-emitted particulate matter ( $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$ ), and toxic air contaminants such as diesel exhaust particulate matter. A construction emission analysis would be required to determine what mitigation, if any, would be required to meet the local SCAQMD CEQA thresholds. Due to the inclusion of a reversible lane option under Alternative 5, the Project is also subject to regional conformity and must be modeled in the Regional Transportation Plan (RTP) and the FTIP. An Air Quality Assessment Report (AQAR) is recommended for the proposed Project during the PA/ED phase. Coordination with the Transportation Conformity Working Group (TCWG) is necessary to assess conformity for particulate matter and determine if the proposed Project is a "Project of Air Quality Concern."
8.13 Noise and Vibration: During construction, heavy equipment, haul trucks, and employee commutes could generate high noise and vibration levels that would affect the sensitive land uses described above. A construction noise impact analysis would be required to determine what mitigation, if any, would be required to meet the local and State standards.

Although the Project under Build Alternatives 2 through 4, would not construct a highway on a new location, physically alter an existing highway either horizontally or vertically, propose the addition of a through-traffic lane, auxiliary lane, or restriping existing pavement for the purpose of adding a through traffic lane or auxiliary lane, Build Alternative 5 would propose the additional traffic lane (although only at peak hour conditions along LCR). As a result of Alternative 5, the proposed Project would be classified as a Type I project under Title 23, Part 772, Code of Federal Regulations and thus, be subject to long-term operational noise analysis.

Therefore, a Noise Study Report (NSR) is recommended to address short-term construction impacts, and long-term operation impacts related to noise with the proposed Project under the Build Alternatives (Alternatives 2 through 5).
8.14 Energy and Climate Change: The proposed Project under the Build Alternatives (Alternatives 2 through 5) would underground utilities. It is not anticipated that construction of the Build Alternatives (Alternatives 2 through 5) would alter the energy consumption in the City. In addition, the proposed Project would not increase the number of through lanes on LCR under Alternatives 2 through 4 and only proposes a reversible through travel lane in one direction along LCR during peak hours. Therefore unlikely to have an effect on regional traffic volumes. The proposed Project's effect on regional criteria pollutant greenhouse gas emissions and mobile source air toxics (MSAT) can be evaluated qualitatively. Energy impacts will be evaluated further within the environmental document during the PA/ED phase.
8.15 Biological Environment: Available literature resources, including the California Department of Fish and Wildlife's California Natural Diversity Database RareFind 5 program (Online CDFW 2018), California Native Plant Society’s (CNPS) Inventory of Rare and Endangered Plants of California (Online Edition, v. 8.2; CNPS 2018), Consortium of California Herbaria (Jepson Flora Project 2018), and USFWS online Information for Planning and Consultation Environmental Conservation Online System were reviewed to identify special-status plant and wildlife species and designated Critical Habitat with the potential to occur in the vicinity of the Project limits. Searches of the California Natural Diversity Database and CNPS databases were conducted for the six U.S. Geological Survey 7.5' quadrangles surrounding the Project, which include Newport Beach, Tustin, El Toro, Laguna Beach, San Juan Capistrano, and Dana Point, California. Appendix B includes the USFWS Species List, California Natural Diversity Database, and CNPS record search results.

Additional resources used to characterize existing site conditions included: U.S. Geologic Survey topographic maps at a minimum 1:24,000 scale, USFWS National Wetland Inventory dataset, Natural Resource Conservation Service Soil Mapping, aerial imagery available on Google Earth, and a field visit to conduct vegetation mapping and a habitat assessment for special-status species with potential to occur in the vicinity of the proposed Project. The consultant biologist also identified all aquatic features with the potential to be regulated by the US Army Corps of Engineers and RWQCB pursuant to Sections 401 and 404 of the Clean Water Act, respectively, and by CDFW pursuant to Section 1600 of California Fish and Game Code. This assessment did not include a delineation of jurisdictional boundaries or wetland determination. Vegetation units were defined based on methodology defined in the online Manual of California Vegetation (CNPS 2018).

Habitats of high concern, as determined by the Open Space - Conservation Element of the City's General Plan, would be impacted as a result of the proposed Build Alternatives, specifically in the proposed location for Staging Area 2. In
addition, the BSA supports five special-status communities: are covered and fully mitigated through participation in the NCCP/HCP. Therefore, Project approval could be affected by the cost of compensatory mitigation for direct impacts to non-covered habitats.

No federally or state-listed plant species are expected within the BSA, as detailed below. Based on the records search, eight federally and/or state-listed plant species were evaluated for the potential to occur within the BSA. These include:

- Thread-leaved brodiaea (Brodiaea filifolia) - Sage scrub and grassland where suitable mesic or clay soils occur (between Castle Rock Road and 3275 Laguna Canyon Rd) have a long history of disturbance. Not Expected.
- Salt marsh bird's beak (Chloropyron maritimum) - no coastal marsh or coastal dune habitat within the BSA. Not Expected.
- Slender horned spine-flower (Dodecahema leptoceras) - BSA is outside of known elevation range for the species. Not Expected.
- Laguna Beach dudleya (Dudleya stolonifera) - BSA does not include northfacing San Onofre or Miocene sandstone rock-outcrops. Not Expected.
- San Diego button celery (Eryngium aristulatum var. parishii) - BSA does not include the necessary vernal pool or mesic sage scrub or grassland habitat. Not Expected.
- Gambell's water cress (Nasturtium gambelii) - BSA does not include necessary marsh habitat. Not Expected.
- California Orcutt's grass (Orcuttia californica) - BSA does not include necessary vernal pool habitat. Not Expected.
- Big-leaved crown beard (Verbesina dissita) - BSA does not include suitable San Onofre brecca substrate or steep, rocky north-west facing slopes.

Based on the records search results, known species' range, and presence of California Sagebrush Scrub and California Buckwheat Scrub within and adjacent to the BSA, the federally threatened CAGN has the potential to occur within or immediately adjacent to the proposed Project limits. Similarly, based on the records search results, known species' range, and presence of Black Willow Thickets and Arroyo Willow Thickets within and adjacent to the BSA, the federally and stateendangered LBVI and SWFL have the potential to occur within or immediately adjacent to the BSA. No critical habitat occurs within the BSA. No other federally or state-listed wildlife species are expected to occur within or adjacent to the BSA, as detailed below.

Based on the records search results, federally and/or state-listed wildlife species that were evaluated for their potential for occurrence within the BSA, but that are not expected to occur include:

- San Diego fairy shrimp (Branchinecta sandiegonensis) - The BSA does not include suitable seasonal pond habitat
- Quino checkerspot butterfly (Euphydryas editha quino) - The BSA is outside of the known range for this species
- Vernal pool fairy shrimp (Branchinecta lynchi) - The BSA does not include suitable seasonal pond habitat
- Tidewater goby (Eucyclogobius newberryi) - The BSA does not support suitable brackish estuarine habitat
- Arroyo toad (Anaxyrus californicus) - The BSA does not include slow moving streams with shallow pools, nearby sandbars and adjacent undeveloped stream terraces.
- Tricolored blackbird (Agelaius tricolor) - The BSA does not include emergent marsh for breeding
- Western snowy plover (Charadrius nivosus nivosus) - The BSA does not include required beach, sand spit, or salt flat nesting habitat
- Western yellow-billed cuckoo (Coccyzus americanus occidentalis) - The riparian corridor associated with Laguna Canyon Creek does not meet the minimum width or acreage requirements for breeding
- Ridgway's rail (Rallus obsoletus) - The BSA does not include required salt marsh and mudflat habitat
- Bank swallow (Riparia riparia) - The BSA does not include the necessary riparian areas with sandy, vertical bluffs or riverbanks.
- California least tern (Sterna antillarum browni) - The BSA does not include the necessary beach and estuarine habitat
- Pacific pocket mouse (Perognathus longimembris pacificus) - The BSA does not include the necessary fine, sand substrate in sage scrub or grassland habitat

Build Alternatives (Alternatives 2 through 5) may directly impact all three-listed species through habitat removal and may indirectly impact all three-listed species through temporary disturbance from construction noise, dust, or lighting during the breeding season. No direct impacts to these species are anticipated after implementation of avoidance and minimization measures. The proposed Project activities are covered by the NCCP/HCP.

Based on the elevation range of the BSA (80-ft. above mean sea level at the southwest end of the BSA to 240-ft. above mean sea level at the northeast end of the BSA), soils in the undeveloped portions of the BSA (primarily Capistrano sandy loam with a small amount of Chino silty clay loam in the vicinity of Castle Rock road and small amounts of Anaheim loam, Cienaba-Rock Outcrop Complex and RockOutcrop Cieneba Complex protruding into the lateral margins of the BSA upslope from the road), known plant species' ranges, and the presence of California Sagebrush Scrub and California Buckwheat Scrub in the BSA, the following 10 special-status plant species, none of which are federally or state-listed, have the potential to occur in the BSA:

- South Coast saltscale (Atriplex pacifica);
- Catalina mariposa lily (Calochortus catalinae);
- Lewis' evening-primrose (Camissoniopsis lewisii);
- Cliff spurge (Euphorbia misera);
- Mesa horkelia (Horkelia cuneata var. puberula);
- Decumbent goldenbush (Isocoma menziesii var. decumbens);
- Allen's pentachaeta (Pentachaeta aurea);
- South coast branching phacelia (Phacelia ramosissima var. austrolitoralis);
- White rabbit-tobacco(Pseudognaphalium leucocephalum); and
- Nuttall's scrub oak (Quercus dumosa)
- Catalina mariposa lily, Lewis' evening-primrose, mesa horkelia, white rabbittobacco, and chaparral ragwort may also occur in Coast Live Oak Woodland (Quercus agrifolia Alliance). Catalina mariposa lily, Lewis' evening-primrose, and Allen's pentachaeta may occur in Mediterranean California Naturalized Annual and Perennial Grassland Group (primarily Bromus diandrus Alliance). White-rabbit tobacco may also occur in riparian woodland (Black Willow Thickets and Arroyo Willow Thickets).

Of the 10 special-status species with the potential to occur in the BSA, only Catalina mariposa lily is covered by the NCCP/HCP. Since most of the Project area is developed, only a small amount of potentially suitable habitat for these species (generally less than 0.25 acre of any single native vegetation community) falls within the actual Project limits and these areas occur in narrow disturbed strips (generally less than 0.1 acre in size) no more than 30 -ft. of the edge of LCR pavement. The small areas of native habitat that would be directly impacted by the Project are not large enough to support significant local populations of these species that, if lost, would contribute to their listing on the state or federal endangered species lists. No compensatory mitigation would be anticipated for potential impacts to special-status plant species even if these species were present and focused surveys are not necessary.

Other special-status wildlife species with the potential to occur within the BSA and covered by the NCCP/HCP include arboreal salamander (Aneides lugubris), blackbellied slender salamander (Batrachoseps nigriventris), coastal whiptail (Cnemidophorus tigris), red-diamond rattlesnake (Crotalus ruber), San Bernardino ringneck snake (Diadophis punctatus modestus), coast horned lizard (Phrynosoma coronatum), Coronado skink (Plestiodon skiltonianus interparietalis), sharpshinned hawk (Accipiter striatus), southern California rufous-crowned sparrow (Aimophila ruficeps), golden eagle (Aquila chrysaetos), rough-legged hawk (Buteo lagopus), red-shouldered hawk (Buteo lineatus), coastal cactus wren (Campylorhynchus brunneicapillus), northern harrier (Circus hudsonius), prairie falcon (Falco mexicanus), peregrine falcon (Falco peregrinus) and San Diego desert woodrat (Neotoma lepida intermidia).

Non-covered special-species wildlife species with the potential to occur within the BSA include California glossy snake (Arizona elegans), coast patch-nosed snake (Salvadora hexalepis), grasshopper sparrow (Ammodramus savannarum), longeared owl (Asio otus), burrowing owl, white-tailed kite (Elanus leucurus), yellowbreasted chat (Icteria virens), yellow warbler (Setophaga petechial), pallid bat (Antrozous pallidus), Dulzura pocket mouse (Perognathus californicus femoralis),
northwestern San Diego pocket mouse (Chaetodipus fallax), western mastiff bat (Eumops perotis), western red bat (Lasiurus blossevillii) and American badger. For these other special-status wildlife species, including those covered by the NCCP/HCP, only a small amount of potentially suitable habitat (generally less than 0.25 acre of any single native vegetation community) would be directly impacted by the Project and these areas occur in narrow disturbed strips (generally less than 0.1 acre in size) and no more than $30-\mathrm{ft}$. of the edge of LCR pavement. Compensatory mitigation would not be anticipated for potential impacts to these special-status wildlife species even if these species were present and focused surveys are not necessary. Species-specific pre-construdibgustrłeyspar2American badger and burrowing owl and measures for avoidance of direct impacts may be required should these species be present.

Migratory birds, including all of the special-status bird species described above, could nest throughout the Project limits. Direct impacts to migratory bird breeding habitat should be avoided during the breeding season, typically defined as February 15 through August 31. If nesting habitat removal is necessary during the breeding season, pre-construction nesting bird surveys would be required. If nesting birds were detected, appropriate no-construction buffers would be required to prevent take of the nest.

Although the Project occurs within primarily developed habitat, it abuts native habitat. Several invasive plant species with either Limited or Moderate ratings from the California Invasive Plant Council ${ }^{2}$ were identified during the site visit including Brazilian pepper tree (Schinus terebinthifolius, Moderate), Peruvian pepper tree (Schinus molle, Limited), ripgut brome (Bromus diandrus, Moderate) and wild oats (Avena fatua, Moderate).

The BSA includes linear aquatic features that have the potential to be regulated by USFWS and RWQCB as non-wetland Waters of the U.S., by CDFW as unvegetated streambed, and by the CCC as wetlands. Additionally, CDFW and CCC may regulate Arroyo Willow Thickets and Black Willow Thickets where they occur within the BSA.

The Project is anticipated to be of limited scope and impact to biological resources and is anticipated to have a "no effect' or "may affect, not likely to adversely affect" determination for impacts to federally listed species. To further evaluate Project

[^13]impacts to biological resources and linear aquatic features, a NESMI and JD are recommended to be prepared during the PA/ED Phase.
8.16 Cumulative Impacts: Project related cumulative impacts would occur under all Build Alternatives (Alternatives 2 through 5). The cumulative impacts are not anticipated to be considered significant under CEQA or adverse under NEPA. The impacts may be seen as adverse or significant when viewed with other projects along SR-133. Three Caltrans projects have been identified within a half mile of the proposed Project, State Route 133 Safety Project PM 3.1/3.6, State Route 133 Canyon Acres Drive Safety Project PM 0.86/1.2 (SR-133 Canyon Acres Safety Project), and SR-133 Shoulder Widening Project. The SR-133 Safety Project and SR-133 Canyon Acres Safety Project are currently in the design phase. SR-133 Shoulder Widening Project is currently in the design Phase. The environmental document prepared during the PA/ED phase will analyze the cumulative impacts.
8.17 Context Sensitive Solutions: Context Sensitive Solutions (CSS) was developed by the FHWA and is used by Caltrans as its approach to include all stakeholders to design, plan, construct, maintain, and operate its transportation system. CSS may be included within aesthetic, historic, and community elements within the proposed Project. Further design during the PA/ED phase would include public outreach so the community can provide input for the proposed Project. Some of these solutions may be incorporated as design features or as avoidance, minimization, and/or mitigation measures during the PA/ED phase.

## 9. Summary Statement for PID

To identify environmental constraints, cost and potential mitigation needed, a Preliminary Environmental Analysis Report (PEAR) was prepared. As part of this effort, minimal field reviews, such as windshield surveys, were performed. Further in-depth analysis has been deferred to the PA/ED phase.

The anticipated document for compliance with CEQA and NEPA is an Initial Study/Environmental Assessment (IS/EA). Caltrans will be the lead agency under CEQA and NEPA. The IS/EA timeline could require up to 24 months to prepare from the start of the environmental studies to the approval of the environmental document.

Potential constraints and special considerations include:

- Under Build Alternatives (Alternatives 2 through 5), traffic circulation and access to businesses and residences along LCR may be impacted temporarily during construction of the proposed Project. A CIA is recommended to evaluate these potential community impacts.
- Under Build Alternatives (Alternatives 2 through 5), the proposed Project would require a TCE and work within an Orange County park, Laguna Coast Wilderness Park. Any impacts to the facility would need to be evaluated under Section 4(f) and
would require compliance with Section 4(f) of the Department of Transportation Act.
- The proposed Project, under the Bulid Alternatives, would require a NES(MI) and a JD to evaluate impacts on biological resources and identify any necessary avoidance, minimization, or mitigation measures. The proposed Project limits is primarily developed, roadway, but would require focused surveys for Least Bell's Vireo and Southern Willow Flycatcher and a Burrowing Owl Habitat Assessment/Breeding Season Survey.
- The proposed Project, under the Build Atlernatives, will require a Water Quality Technical Memorandum to address water quality issues in the area. A SWPPP would also be required because the proposed Project will disturb more than one acre of soil. BMPs will be identified within both the Water Quality Technical Memorandum and SWPPP to address water quality, sediment, and erosion control during construction.
- The proposed Project is within a 100-year flood plain. A Location Hydraulic Study is recommended.
- The proposed Project, under the Build Alternatives, would require an ASR to identify any archaeological resources within the Project area. If the Project limits were to change and include any archaeological resources, an Extended Phase 1 survey may be required. The portion of LCR within the project limits was determined not eligible for the NRHP/CRHR by the SHPO on $7 / 24 / 18$, and the Laguna Canyon Historic District is locally eligible. An HRER may be required to evaluate the built environment or any historical resources in the APE. The ASR and HRER would be appended to the HPSR. Consultation with Native Americans will be required under Section 106 of the NHPA with Caltrans as the lead agency for NEPA, and for AB52 as the lead agency for CEQA.
- The proposed Project, under the Build Alternatives, will require excavations exceeding $6-\mathrm{ft}$. below ground surface, and potentially impact paleontological resources. A combined PIR/PER is required during PA/ED, and a PMP will be prepared during PS\&E to outline a mitigation program during construction if it is determined that potentially significant paleontological resources may be impacted.
- The proposed Project, under the Build Alternatives, will require an ISA to address any hazardous waste concerns within the area, as well as potential impacts to water quality.
- The proposed Project, under the Build Alternatives, will require an AQAR to address air quality concerns within the Project limits due to a new signalized intersection. The AQAR would address PM and CO hot-spot analyses for local
transportation conformity. The Project would also require coordination with the Transportation Conformity Working Group to assess conformity for particulate matter and determine if the proposed Project is a "Project of Air Quality Concern." In addition, a quantitative analysis of greenhouse gas emissions will be required.
- The proposed Project, under the Build Alternatives, will require a short-term and long-term noise and vibration analysis. With the inclusion of a reversible lane under Alternative 5, the proposed Project would be classified as a Type I project under Title 23, Part 772, Code of Federal Regulations, and thus, be subject to long-term operational noise analysis, as well. Therefore, a NSR would be required.
- The proposed Project would require the following permits: Coastal Development Permit, a Section 401 Water Quality Certification, a Section 404 Nationwide Permit, and a California Fish and Game 1602 Streambed Alteration Agreement.


## 10. Disclaimer

This Preliminary Environmental Analysis Report (PEAR) provides information to support programming of the proposed project. It is not an environmental determination or document. Preliminary analysis, determinations, and estimates of mitigation costs are based on the project description provided in the PID. The estimates and conclusions in the PEAR are approximate and are based on cursory analyses of probable effects. A reevaluation of the PEAR will be needed for changes in project scope or alternatives, or in environmental laws, regulations, or guidelines.

## 11. List of Preparers

| Cultural Resources specialist: Ben Volta | Date: $5 / 27 / 2022$ |
| :--- | :--- |
| Biologist: Sarah Barrera | Date: $5 / 27 / 2022$ |
| Community Impacts specialist: Uyenlan Vu | Date: $5 / 27 / 2022$ |
| Noise and Vibration specialist: Angie Kung | Date: $5 / 27 / 2022$ |
| Air Quality specialist: Angie Kung | Date: $5 / 27 / 2022$ |
| Paleontology specialist/liaison: Curt Duke | Date: $5 / 27 / 2022$ |
| Water Quality specialist: Natalie Brim | Date: $5 / 27 / 2022$ |
| Hydrology and Floodplain specialist: Natalie Brim | Date: $5 / 27 / 2022$ |
| Hazardous Waste/Materials specialist: Uyenlan Vu | Date: $5 / 27 / 2022$ |
| Visual/Aesthetics specialist: Natalie Brim | Date: $5 / 27 / 2022$ |
| Energy and Climate Change specialist: Angie Kung | Date: $5 / 27 / 2022$ |
| Other: | Date: $5 / 27 / 2022$ |
| PEAR Preparer: Angie Kung, Environmental Section Manager | Date: $5 / 27 / 2022$ |

## 12. Review and Approval

I confirm that environmental cost, scope, and schedule have been satisfactorily completed and that the PEAR meets all Caltrans requirements. Also, if the project is scoped as a routine EA, complex EA, or EIS, I verify that the HQ DEA Coordinator has concurred in the Class of Action.
$\qquad$
Environmental Branch Chief


Project Manager

Aug 18, 2022
Date

August 29, 2022
Date

## ATTACHMENTS:

Attachment A: Figures
Attachment B: PEAR Environmental Studies Checklist
Attachment C: Mitigation and Compliance Cost Estimate (MCCE) (not required for PSR-PDS)
Attachment D: Schedule (Gantt Chart)
Attachment E: Caltrans staff should use the "Bottom Up Tool." External partners should contact their local Caltrans district office for direction.

Attachment A: Figures


12-ORA-133 PM 0.96/3.42
EA 0Q670

Laguna Canyon Road PSR/PDS
Figure 1. Regional Location



Figure 2. Project Limits


Figure 2. Project Limits


Figure 2. Project Limits


Figure 2. Project Limits

Attachment B: PEAR Environmental Studies Checklist

Attachment B：PEAR Environmental Studies Checklist

| Environmental Studies for PA\＆ED Checklist |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  | Not anticipated | Memo to file | Report required | $\begin{aligned} & \text { Risk* }^{*} \\ & \text { L M H } \end{aligned}$ | Comments |
| Land Use | $\square$ | $\square$ | 区 | $\underline{L}$ | New ROW required （potential conversion of existing land uses to transportation）． Included in CIA． |
| Growth | 区 | $\square$ | $\square$ | $\underline{L}$ | Project related impacts not anticipated． Discussed in ED． |
| Farmlands／Timberlands | 区 | $\square$ | $\square$ | $\underline{L}$ |  |
| Community Impacts | $\square$ | $\square$ | 区 | M | CIA，include parking survey |
| Community Character and Cohesion | $\square$ | $\square$ | 区 | $\underline{L}$ | Included in CIA <br> Technical Memorandum |
| Relocations | 区 | $\square$ | $\square$ | $\underline{L}$ | Relocation Impact Memorandum，only if there are Project design changes during PA／ED where relocations are found to be required． |
| Environmental Justice |  |  | 区 | $\underline{L}$ | Included in CIA． |
| Utilities／Emergency Services |  |  | 区 | M | Included in CIA． |
| Visual／Aesthetics |  | $\square$ | 区 | $\underline{L}$ | VIA Technical Memorandum． |
| Cultural Resources： |  |  | 区 | M | HPSR，ASR，HRER． |
| Archaeological Survey Report |  |  | 区 | M |  |
| Historic Resources Evaluation Report |  |  | Х | M |  |
| Historic Property Survey Report |  |  | 区 | M |  |
| Historic Resource Compliance Report | 区 |  |  | M | Included in HPSR． |
| Section 106 ／PRC 5024 \＆ 5024.5 |  |  | 区 | M | Included in HPSR． |
| Native American Coordination |  |  | 区 | M | Included in HPSR． |
| Finding of Effect | 区 |  |  | $\underline{L}$ |  |
| Data Recovery Plan | 区 | $\square$ | $\square$ | $\underline{L}$ |  |
| Memorandum of Agreement | 】 |  | $\square$ | $\underline{L}$ |  |
| Other： | 区 |  |  | $\underline{L}$ |  |
| Hydrology and Floodplain |  |  | 区 | $\underline{L}$ | Discussed in LHS． |
| Water Quality and Stormwater Runoff | $\square$ | $\square$ | 区 | $\underline{L}$ | Water Quality Technical Memorandum． |
| Geology，Soils，Seismic and Topography | 区 | $\square$ | $\square$ | $\underline{L}$ | Discussed in ED． |
| Paleontology |  |  | 区 | H |  |
| PER |  |  | 区 | H |  |
| PMP | $\square$ | $\square$ | 区 | H | Recommended during PS\＆E． |


| Environmental Studies for PA\＆ED Checklist |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Not anticipated | Memo to file | Report required | $\begin{aligned} & \text { Risk }^{*} \\ & \text { L M H } \end{aligned}$ | Comments |
| Hazardous Waste／Materials： | $\square$ | $\square$ | 区 | M |  |
| ISA（Additional） | $\square$ |  | 区 | M |  |
| PSI |  |  | 区 | M |  |
| Other： | $\square$ | ， | － |  |  |
| Air Quality | $\square$ | $\square$ | 区 | $\underline{L}$ | Air Quality Assessment Report． |
| Noise and Vibration | $\square$ |  | 区 | $\underline{L}$ | Noise Study Report． |
| Energy and Climate Change | 区 |  |  | $\underline{L}$ | Discussed in ED． |
| Biological Environment |  |  | 区 | M |  |
| Natural Environment Study |  |  | 区 | M | NES（MI）． |
| Section 7： | 区 |  |  | $\underline{L}$ |  |
| Formal | 区 |  |  | $\underline{L}$ |  |
| Informal | 区 |  |  | $\underline{L}$ |  |
| No effect | 区 |  |  | $\underline{L}$ |  |
| Section 10 | 区 |  |  | $\underline{L}$ |  |
| USFWS Consultation | 区 |  | $\square$ | $\underline{L}$ |  |
| NMFS Consultation | 区 |  | $\square$ | $\underline{L}$ |  |
| Species of Concern（CNPS，USFS， BLM，S，F） | $\square$ | $\square$ | 区 | $\underline{M}$ |  |
| Wetlands \＆Other Waters／Delineation | $\square$ |  | 区 | M | JD． |
| 404（b）（1）Alternatives Analysis | 区 |  |  | $\underline{L}$ |  |
| Invasive Species |  |  | 区 | M | Included in NES（MI）． |
| Wild \＆Scenic River Consistency | 区 |  | $\square$ | $\underline{\underline{L}}$ |  |
| Coastal Management Plan |  |  | 区 | M | Included in NES（MI）． |
| HMMP | $\square$ |  | 区 | M | Included in NES（MI）． |
| DFG Consistency Determination | 区 |  |  | $\underline{L}$ |  |
| 2081 | 区 |  |  | $\underline{L}$ |  |
| Other： | 区 |  |  | $\underline{L}$ |  |
| Cumulative Impacts | 区 |  |  | $\underline{L}$ | Discussed in ED． |
| Context Sensitive Solutions | 区 |  |  | $\underline{L}$ | Discussed in ED． |
| Section 4（f）Evaluation | $\square$ | $\square$ | 区 | $\underline{M}$ | Section 4（f） Evaluation． |
| Permits： |  |  |  |  |  |
| 401 Certification Coordination |  |  | 区 | M |  |
| 404 Permit Coordination，IP，NWP，or LOP | $\square$ | － | 区 | M |  |
| 1602 Agreement Coordination |  |  | ถ | M |  |
| Local Coastal Development Permit Coordination | $\square$ | $\square$ | 区 | M |  |
| State Coastal Development Permit Coordination | $\square$ | $\square$ | 区 | M |  |
| NPDES Coordination | $\square$ |  | 区 | $\underline{L}$ |  |
| US Coast Guard（Section 10） | 区 |  |  | $\underline{L}$ |  |
| TRPA | 区 | $\square$ | ］ | $\underline{L}$ |  |
| BCDC | 区 | $\square$ | $\square$ | $\underline{L}$ |  |

Attachment C: Mitigation and Compliance Cost Estimate (MCCE) (not required for PSR-PDS)

Attachment D: Schedule (Gantt Chart)

Laguna Canyon Road - Schedule

|  |  |  |  | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project Milestones | Mile stone |  | Duration (Months) |  |  |  |  |  |  |  |  |  |
| PSR/PDS Approval | M010 | Jul-22 |  |  |  |  |  |  |  |  |  |  |
| Program Project | M015 | Jul-23 | 12 |  |  |  |  |  |  |  |  |  |
| Project Report/Env. <br> Document Approval | M200 | Jul-25 | 24 |  |  |  |  |  |  |  |  |  |
| Complete PS\&E | M377 | Jan-27 | 18 |  |  |  |  |  |  |  |  |  |
| Right-of-way Certification | M410 | Apr-27 | 3 |  |  |  |  |  |  |  |  |  |
| Obtain Coastal Development Permit |  | Jul-27 | 12 |  |  |  |  |  |  |  |  |  |
| Ready-to-list | M460 | Oct-27 | 3 |  |  |  |  |  |  |  |  |  |
| Advertise/Bid/Award Contract | M495 | Feb-28 | 4 |  |  |  |  |  |  |  |  |  |
| Construction Contract Complete | M800 | Feb-30 | 24 |  |  |  |  |  |  |  |  |  |
| Base year | 2022 |  |  |  |  |  |  |  |  |  |  |  |
| Opening Year | 2030 |  |  |  |  |  |  |  |  |  |  |  |
| Horizon Year | 2050 |  |  |  |  |  |  |  |  |  |  |  |

Attachment E: Caltrans staff should use the "Bottom Up Tool." External partners should contact their local Caltrans district office for direction.






## ATTACHMENT J

INITIAL SITE ASSESSMENT (ISA) CHECKLIST

Initial Site Assessment (ISA) Checklist

## Project Information

District 12 County $\quad$ OC Route 133 Kilometer Post_PM 0.9/PM 3.4 EA (Post Mile)
Description The City of Laguna Beach (City), in cooperation with the California Department of Transportation (Caltrans), is proposing to improve a 2.5 mile corridor of the State Route 133 (SR-133) in the City of Laguna Beach, California. SR-133, also known as Laguna Canyon Road (LCR), extends from approximately Canyon Acres Drive (PM 0.9) to El Toro Road (PM 3.4) in Orange County, California (Project). The proposed roadway improvements include bicycle lanes, pedestrian pathways, improving access to transit facilities, and compliant lane widths and shoulders. Due to limited space within the existing right-of-way, the undergrounding of existing transmission and distribution lines owned by Southern California Edison would be required to accommodate the proposed improvements.

Is the project on the HW Study Minimal-Risk Projects List (HW1)?
No
Project Manager _ Lorica Subida, Caltrans
Project Engineer Raouf Fam, Caltrans
phone \#
phone \# (657) 328-6269

## Project Screening

Attach the project location map to this checklist to show location of all known and/or potential HW sites identified. (Refer to the ISA for project and site-specific location maps.)

1. Project Features: New R/W? __Yes_Excavation? Yes_Railroad Involvement? No No

Structure demolition/modification?_ No Subsurface utility relocation? Yes
2. Project Setting Rural area with primarily light-industrial, commercial and residential development, along with transportation and utility facilities.

Rural or Urban Rural

Current land uses State, County, City, and private right-of-way.

Adjacent land uses Light-industrial, commercial, residential, and recreational.
(industrial, light industry, commercial, agricultural, residential, etc.)
3. Check federal, State, and local environmental and health regulatory agency records as necessary to see if any known hazardous waste site is in or near the project area. If a known site is identified, show its location on the attached map and attach additional sheets, as needed, to provide pertinent information for the proposed project. (Refer to the ISA Memorandum for site-specific information.)
4. Conduct Field Inspection. Date 5/23/2018 Refer to the ISA Memorandum to locate potential or known HW sites.

STORAGE STRUCTURES / PIPELINES:

| Underground tanks | Yes | Surface tanks | Yes |
| :---: | :---: | :---: | :---: |
| Sumps | None found | Ponds | None found |
| Drums | Yes | Basins | None found |
| Transformers | Yes | Landfill | Yes |

Other $\qquad$

# Initial Site Assessment (ISA) Checklist (continued) 

CONTAMINATION: (spills, leaks, illegal dumping, etc.)

| Surface staining | Yes (minor) | Oil sheen | None found |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |
| Odors | None found | Vegetation damage | None found |

Other _ De minimis pavement oil staining at Laguna Beach Unified School District Maintenance Yard.
HAZARDOUS MATERIALS: (asbestos, lead, etc.)

| Buildings | Unknown |  | Spray-on fireproofing | Unknown |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |
| Pipe wrap | Unknown | Friable tile | Unknown |  |
|  |  |  |  |  |
| Acoustical plaster | Unknown |  | Serpentine |  |

Paint
Unknown
Other Potential for aerially-deposited lead (ADL) in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133, lead chromate in yellow traffic striping and pavement marking materials along SR-133, polychlorinated biphenyls (PCB) in utility pole- and padmounted electrical transformers, and creosote and pentachlorophenol in wooden utility poles.
5. Additional record search, as necessary, of subsequent land uses that could have resulted in a hazardous waste site. (Refer to the ISA Memorandum for site-specific information.)
6. Other comments and/or observations:

## ISA Determination

Does the project have any potential hazardous waste involvement? Yes If there is known or potential hazardous waste involvement, is additional ISA work needed before task orders can be prepared for the Preliminary Site Investigation? _No If "YES," explain; then give an estimate of additional time required:

During PA/ED, a full ISA for all right-of-way acquisition properties is recommended to comply with ASTM E1527-21 to meet "innocent landowner" provisions under the Comprehensive Environmental Response, Compensation and Liability Act of 1980 (CERCLA), which establish a defense for the purchase of real property. In addition, Preliminary Site Investigations (PSI) are also recommended to be conducted during PA/ED for the following:

- ADL in previously undisturbed soil areas or unpaved areas within Caltrans right-of-way along the shoulders of SR-133
- Lead chromate in yellow traffic striping and pavement materials along SR-133
- PCB in utility pole- and pad-mounted electrical transformers and in soil surrounding the transformers
- Creosote and pentachlorophenol in wooden utility poles and in soil surrounding the poles

The full ISA can be prepared simultaneously when the PSIs are conducted during PA/ED.

A brief memo should be prepared to transmit the ISA conclusions to the Project Manager and Project Engineer.


Date 5/23/2022

## ATTACHMENT K

## RISK REGISTER

| EVEL - - RISK REGIITER |  |  |  |  |  | Project Name: | SR-133 PSRRPDS |  | $\begin{array}{\|l\|} \hline \text { DisT-EA } \\ \hline \text { Probabaility } \end{array}$ | $\begin{array}{\|l\|l\|} \hline 12.006870 \\ \hline \text { CostImpact } \end{array}$ |  |  |  |  | Risk Response |  | Risk owner |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | skl Identification |  |  |  |  |  |  |  |  | Upataed |  |
| Status | 10\% | Type | Category | (inte |  |  | Risk Statement | Current statusassumptions |  |  | Rore | Sk Assessm | Time Score | Rationale |  | Strateg |  | Response Actions |
| Active | 1 | Threat | Envionmental | 10132017 | Both | Local community stakeholder groups pose objections to the Project |  |  | 4-High | ${ }^{8 . \text { High }}$ | ${ }^{32}$ | ${ }^{8 . \text { Hiligh }}$ | ${ }^{32}$ | Some opposition has been heard from local community heard from groups. | Miligate | The City of Laguna Beach and Caltrans to maintain a proactive public outreach effort by providing up-to-date meetings, City Council meetings, and other community outreach opportunities | $\underset{\substack{\text { city } \\ \text { Beach launa }}}{\text { che }}$ |  |
| Active | 2 | Threat | Envionmental | 10132017 | Schedule | Challenge to Environmental Document |  | Mitigated during PA\&ED Phase. <br> Triggered during public review. | 3-Moderate | ${ }^{8 . \text { High }}$ | ${ }^{24}$ | ${ }^{8 . \text { High }}$ | ${ }^{24}$ |  | Mitigate | $\begin{aligned} & \text { Maintain good communications with } \\ & \text { community during PA\&ED phase to } \\ & \text { ensure concerns and impacts are } \\ & \text { addressed in ED. } \end{aligned}$ | Evirommenal |  |
| Active | 3 | Threat | PM | 10132017 | Schedule | Delay or withdrawal of <br> funding | f funding for the project is not available, project may be delayed or cancelled. |  | 3-Moderate | 4-Mo | ${ }^{12}$ | 4-Mod | 12 |  | Mitate | Produce Project Intitation Documen Progiond and include Proiect in local and regramming documents. Pursue wide range of funding opportunities from local, State, and Federal sources. | City of Laguna | 42771202 |
| Active | 4 | Threat | Design | 10132017 | Schedule | Project Costis too high |  |  | 3-Moderate | 4-Moderate | ${ }^{12}$ | ${ }^{8 . H \text { High }}$ | 24 | Too high of an estimated cost could cause delay in being able to program the project. | Mitigate | Develop accurate cost estimates for the project early and update cost estimate periodically | pot |  |
| Active | 5 | Threat | Row | 10132017 | Schedule | Additional RW | Due to the complex nature of the project, additional right of way, permanent easements may be required to complete the work as cost to the project. |  | 3-Moderate | 4-Moderate | ${ }^{12}$ | 4-Moderat | 12 |  | Mitigate | Early detection of right of way needs is key. Justification of right of way needs Caltrans and SCE to locate undergrounded utilities within existing State right-of-way | pot | 51122022 |
| Active | 6 | Threat | row | 10132017 | Both | Residential Encroachments into Existing ROW | At various locations, existing residential improvements encroach into existing State R/W. | Mitigated during PAED Phase. | 3-Moderate | 4-Moderate | ${ }^{12}$ | 4-Moderate | 12 |  | Mitigate | Advare right-of-way documentation in PA/ED phase. Initiate early communication with property owners | pot | 51122022 |
| Active | 7 | Threat | Row | 10/32017 | Schedule | Proposed pedestrian path requires $R / W$ |  | May be resolved with design and PDT concurrence. | 2-Low | 4-Moderate | 8 | 4-Moderate | 8 | Evaluate mitigation options in PA/ED phase. | Mitgate | Review locations early in the PA/ED phase to determine environmenta concerns and mitigation options. | pot |  |
| Active | 8 | Threat | PM | 10/32017 | Schedule | Agency Permis |  | Mitigated during PAED Phase. | 2-Low | 4-Moderate | 8 | ${ }^{8 . \text { High }}$ | 16 | This has been an issue on both budget and scheduls | Mitigat | Meet early and often with resource agencies to ensure that their concerns are addressed. | PDT |  |
| Active | 9 | Threat | Envionmental | 10/32017 | Schedule | Envirommental Impacts | As part of the PEAR it is discovered that significant impacts may cause delays or higher than expected mitigation costs. |  | 2-Low | ${ }^{8}$-High | ${ }^{16}$ | 4-Moderate | 8 |  | Mitigat |  | pot | 427712022 |
| Active | 10 | Threat | PM | 10/32017 | Schedule | SCE Coordination for undergrounding |  |  | 3-Moderate | ${ }^{8 . \text { High }}$ | ${ }^{24}$ | ${ }^{8 . \text { High }}$ | ${ }^{24}$ |  | Mitigate | Engage SCE throughout design process to solicit input and co in order to minimize impacts. | PDT |  |
| Active | 11 | Threat | Design | 10/32017 | Schedule | Costal Zone Requirement |  |  | 2-Low | ${ }^{8 . \text { High }}$ | ${ }^{16}$ | ${ }^{8}$.righ | 16 |  | Mitate | Understand additional requirements of Coastal Zone development; especially water quality requirements and quring construction. | pot |  |
| Active | 12 | Threat | Envionmental | 512712022 | cost | Costs to mitigate impacts to CDFW and OC Flood may be high | (mpacts not apparentin preliminay |  | 2-Low | ${ }^{8}$-righ | ${ }^{16}$ | 4-Moderate | 8 |  | Mitate | Environmental review will be provided during PA/ED. Design will consider avoiding impacts | pot |  |
| Active | 13 | Threat | Row | 512712022 | Both | Property accuisition | Objections to loss of property rigths may lead to Resolution of Necessity (RON) (RON) |  | 2-Low | 4-Moderate | ${ }^{8}$ | 4-Modeate | 8 | $\begin{aligned} & \text { Acquisitions are all partial and } \\ & \text { most are slither area where } \\ & \text { current use is minimal } \end{aligned}$ | Mitigat | Public outreach | PDT |  |
| Active | 13 | Threat | Envionmental | 512712022 | cost | Additional Stakeholder outreach | Additional Reporting and participation in local information distribution may increase Proj Development Costs developmenicosts |  | 3-Moderate | 4-Moderate | ${ }^{12}$ | 4-Modeate | 12 | Costsinguled in essimate or or public paticipation | Mitgate | Invesigate waterine provide | Design Pot |  |
| Active | 14 | Threat | Design | 512712022 | Both | Waterline adjacent to roadway | Waterline is fragile; it may need to be designed around |  | 3 -Moderate | 4-Moderate | ${ }^{12}$ | 4-N | 12 | $\begin{aligned} & \text { Costs included in estimate to } \\ & \text { include this potential } \\ & \text { relocation } \end{aligned}$ | Mitiate | Investigate waterline; provid innovative designs | Design PDT |  |


[^0]:    Source: Caltrans District 12 TASAS Table B (January1, 2016 to December 31, 2020)
    Notes: ${ }^{1}$ the accident rate is the number of accidents per million vehicle-miles ( $\mathrm{a} / \mathrm{mvm}$ )
    Bold indicates total actual accident rate that is higher than the statewide average accident rate for similar facilities

[^1]:    *Applies to all SWPPPs and those WPCPs with sediment control or soil stabilization BMPs.
    **Applies to both SWPPPs and WPCP projects.
    *** Applies only to project with SWPPPs.

[^2]:    Subtotal Stage Construction and Traffic Handling
    $\$$

[^3]:    Note: Items G \& H applied to items A + B

[^4]:    ${ }^{2}$ When estimate has Utility Relocation $\quad{ }^{3}$ When R/W Acquisition is required

[^5]:    Subtotal Stage Construction and Traffic Handling \$

[^6]:    ${ }^{2}$ When estimate has Utility Relocation $\quad{ }^{3}$ When R/W Acquisition is required

[^7]:    Subtotal Stage Construction and Traffic Handling \$

[^8]:    ${ }^{2}$ When estimate has Utility Relocation $\quad{ }^{3}$ When R/W Acquisition is required

[^9]:    Subtotal Stage Construction and Traffic Handling \$

[^10]:    ${ }^{2}$ When estimate has Utility Relocation $\quad{ }^{3}$ When R/W Acquisition is required

[^11]:    Source: Caltrans District 12 TASAS Selective Accident Retrieval (TSAR) (January 2016 to December 2020)
    Bold Red indicates most occurring accident
    Bold indicates second most occurring accident

[^12]:    *Proposed funding to be determined. Purpose of PSR is to obtain funding and potential funding sources.
    **R/W Support costs include costs for engineering, appraisals, etc.
    ROW cost estimate is assumed to be probable to optimistic.

[^13]:    ${ }^{2}$ Moderate - These species have substantial and apparent—but generally not severe—ecological impacts on physical processes, plant and animal communities, and vegetation structure. Their reproductive biology and other attributes are conducive to moderate to high rates of dispersal, though establishment is generally dependent upon ecological disturbance. Ecological amplitude and distribution may range from limited to widespread.

    Limited - These species are invasive but their ecological impacts are minor on a statewide level or there was not enough information to justify a higher score. Their reproductive biology and other attributes result in low to moderate rates of invasiveness. Ecological amplitude and distribution are generally limited, but these species may be locally persistent and problematic.

